

HELSMAC- Cambridge, UK

---

## A FEW ASPECTS OF THE CURRENT UNDERSTANDING OF DPF MATERIALS THERMAL AND MECHANICAL PROPERTIES

Giovanni Bruno

BAM-8.5 „Micro NdT“, Berlin, Germany

Alexander M. Efremov, Andrey N. Levandovskyi

Corning Incorporated, St.Petersburg, Russia

Mark L.Kachanov

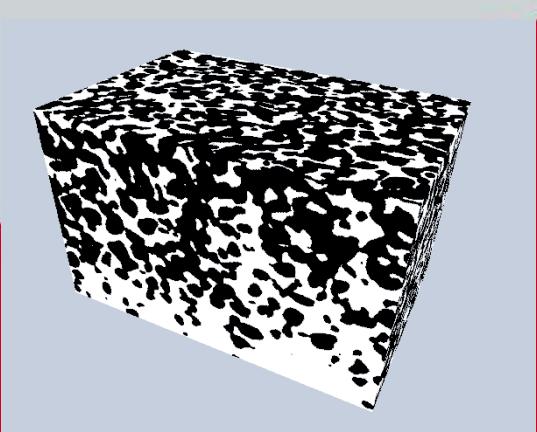
Tufts University, Medford, MA, USA

Sven Vogel, Bjørn Clausen

Lujan Center, LANL, Los Alamos, NM, USA

Darren J.Hughes

Warwick University, Coventry, UK



# BAM guideline and mission



Safety in technology and chemistry

---

Pursuing our mission as a Federal institute for materials technology and chemical engineering, we ensure ongoing safety in technology and chemistry through

- research and development
- testing, analysis, approval and certification
- consultation, information and advice

within our objective of promoting German (and EU) industrial development.



# Porous Ceramics in Industry

## Applications as

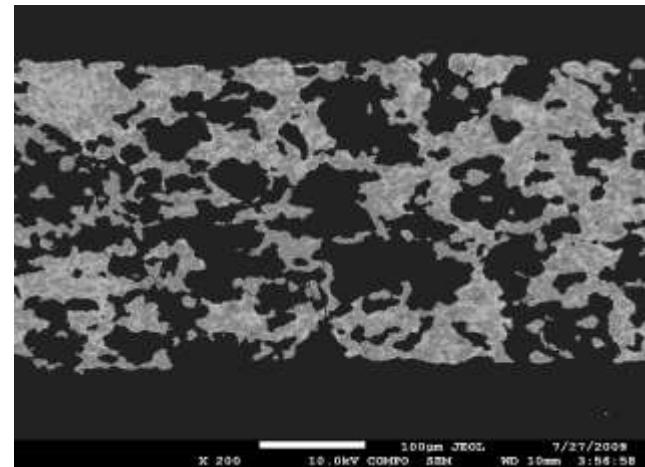
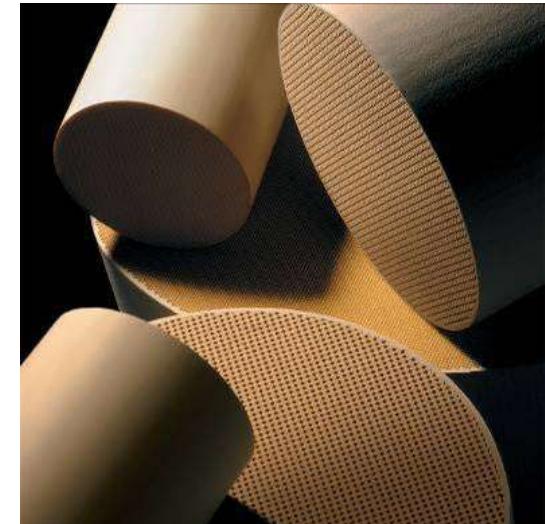
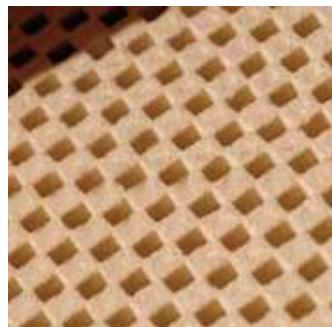
- Filters (mobile/ stationary)
- Membranes
- Substrates for catalysts

## Typical materials

- Cordierite
- Silicon Carbide
- Aluminum Titanate
- $\beta$ -Eucryptite

## Typical Characteristics

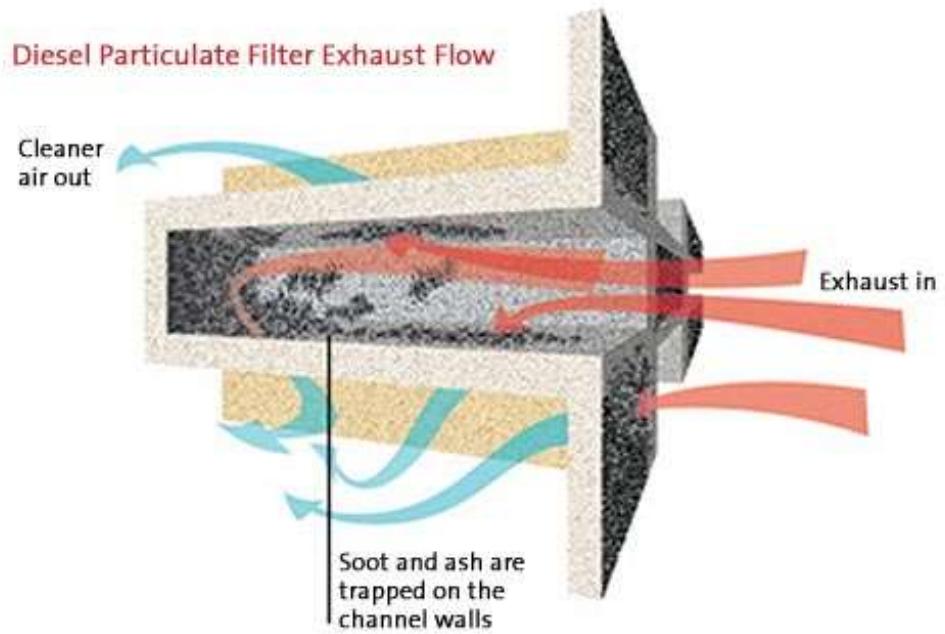
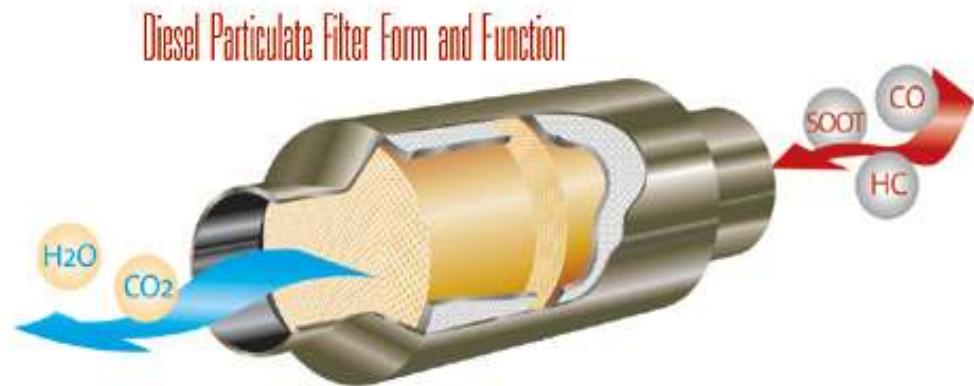
- Low thermal expansion (not all)
- Microcracking (not all)
- High permeability
- High **thermal shock resistance**
- Strain tolerance



# Porous Ceramic Filters

## Main attributes

- Filtration efficiency
- Pressure drop
- Resistance to crack initiation
- Operation at high temperatures



# Facts

---

Microstructure

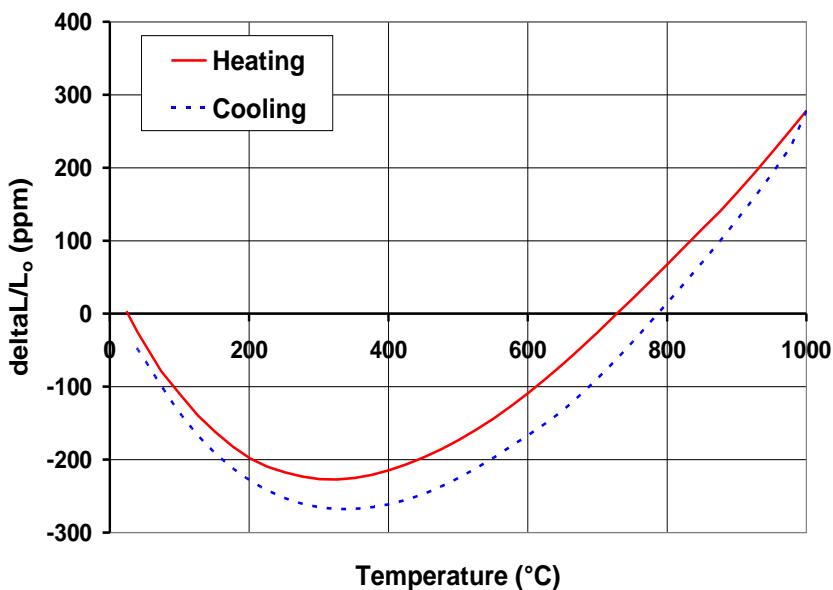
Mechanical behavior

Thermal behavior

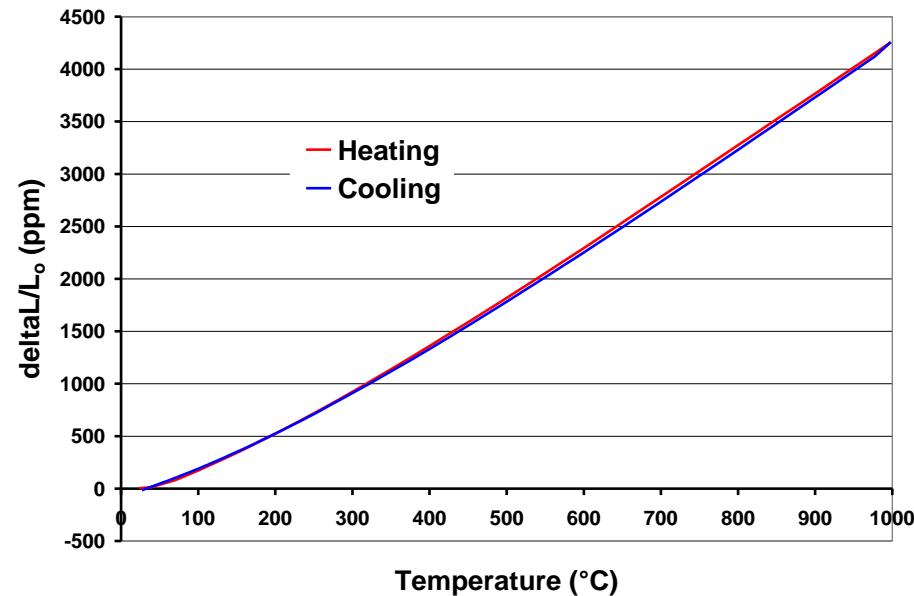
# DPF Ceramics:

## Microstructure and Thermal Properties

### Thermal expansion



Cordierite

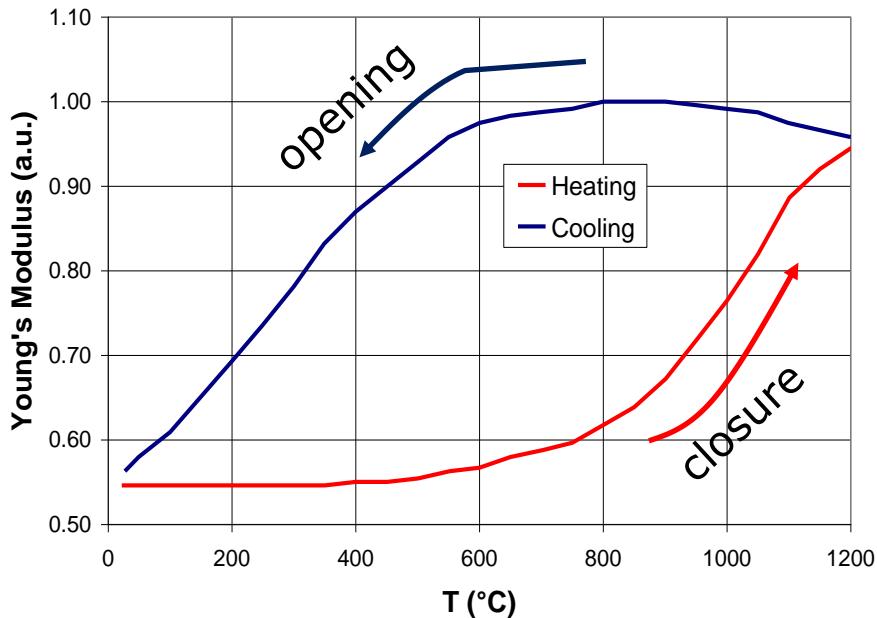


Silicon Carbide

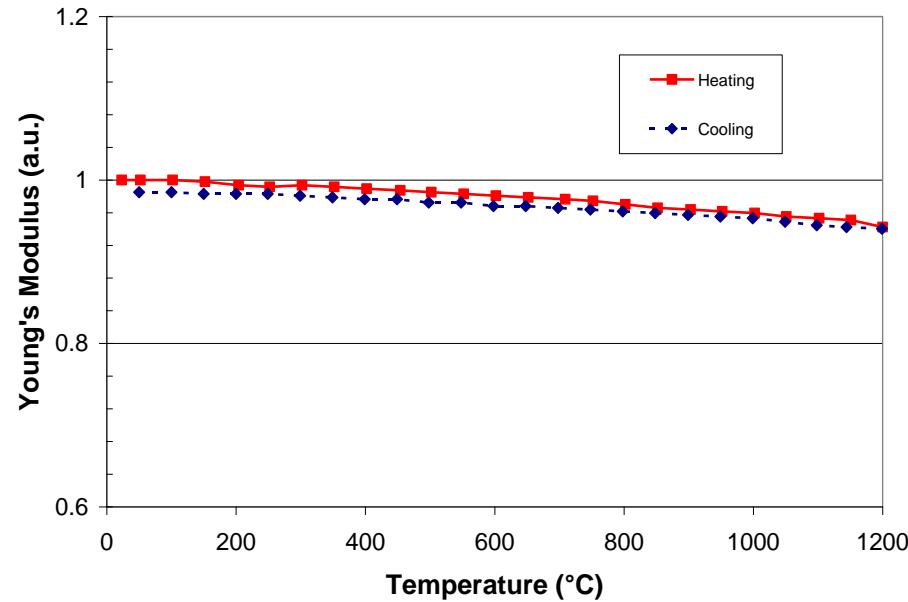
# DPF Ceramics:

## Mechanical Properties

### Young's Modulus



Cordierite



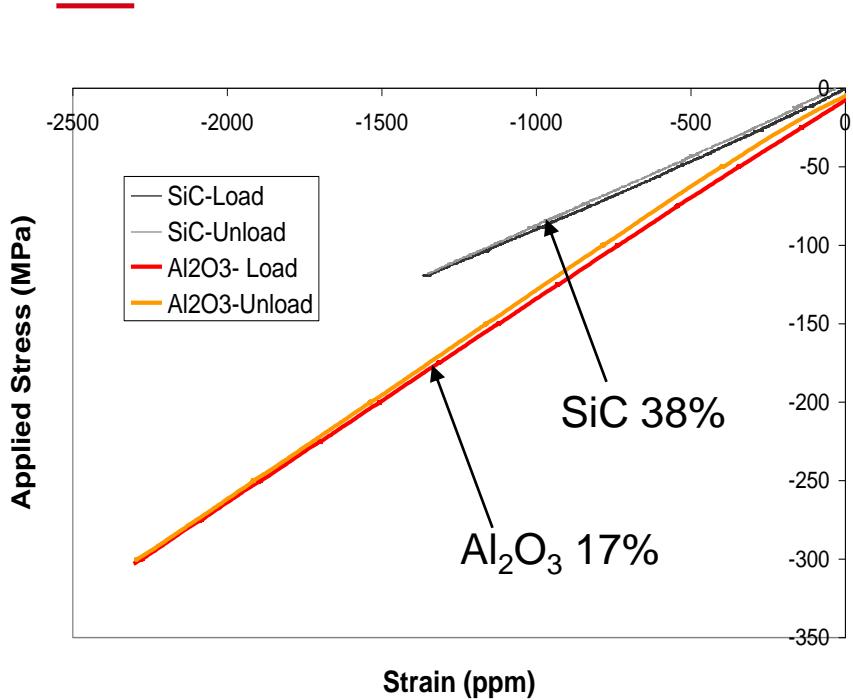
Silicon Carbide

Microcracking often occurs because of lattice thermal expansion anisotropy (NB: low crystal symmetry ceramics)

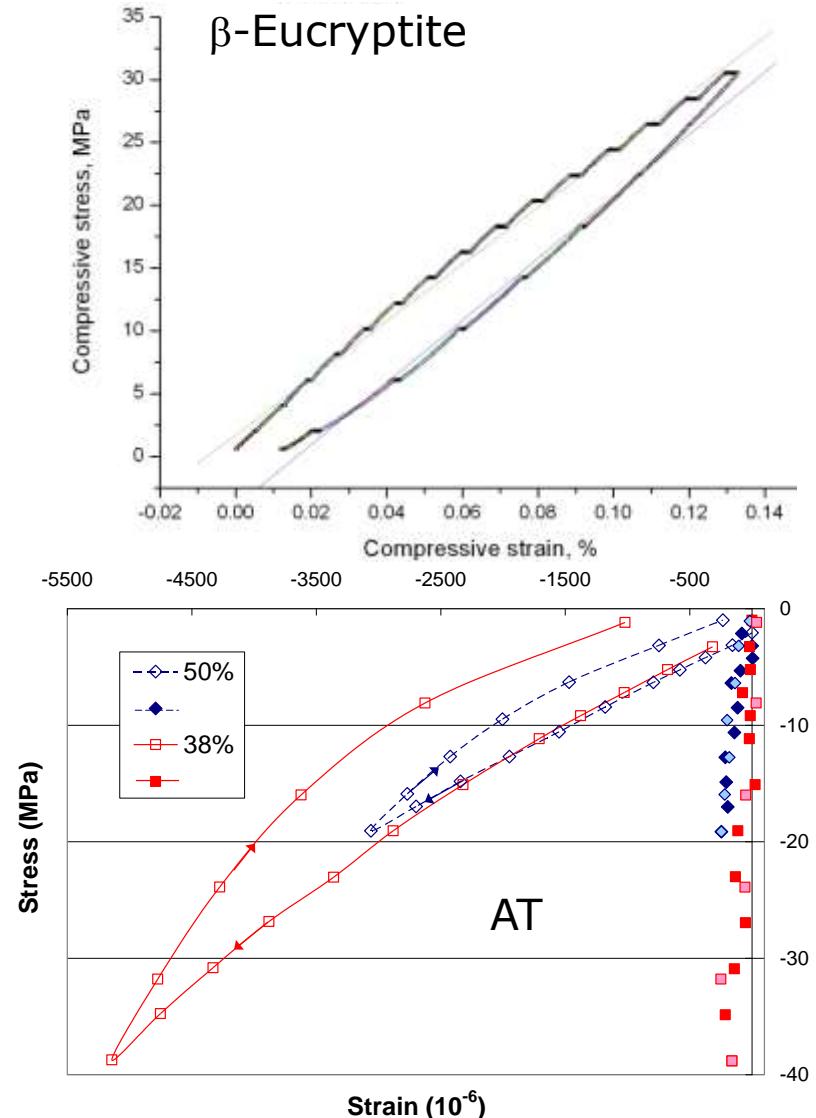
Hysteresis of dilation and Young's modulus  $\text{vs } T$ : thermal microcracking

# Non-linear stress-strain behavior

Mechanical microcracking



Very visible in microcracked materials, present in non-microcracked

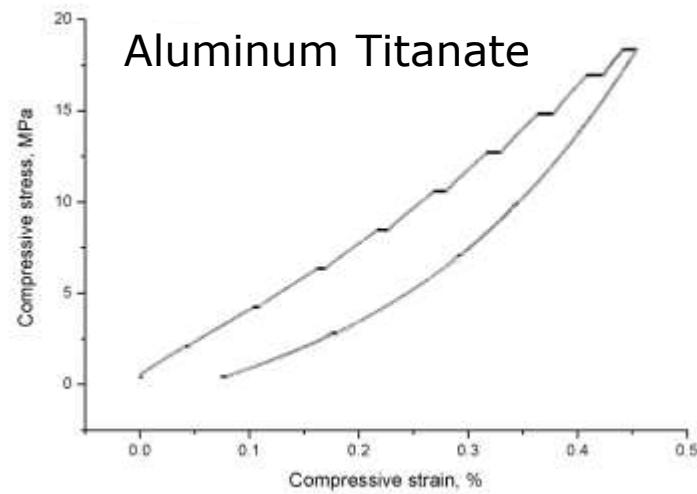
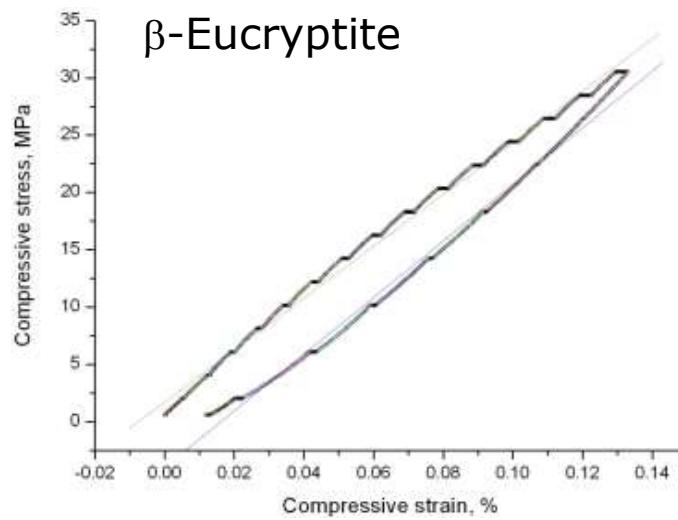
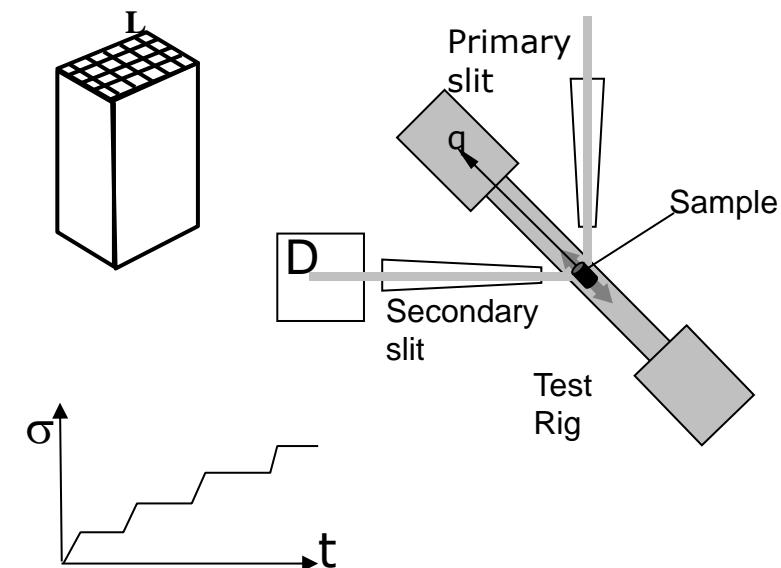
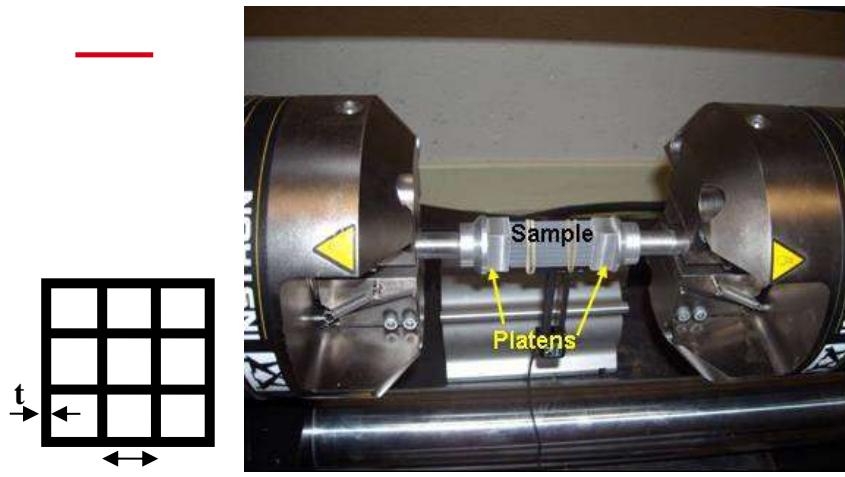


Mechanical behavior and its modeling

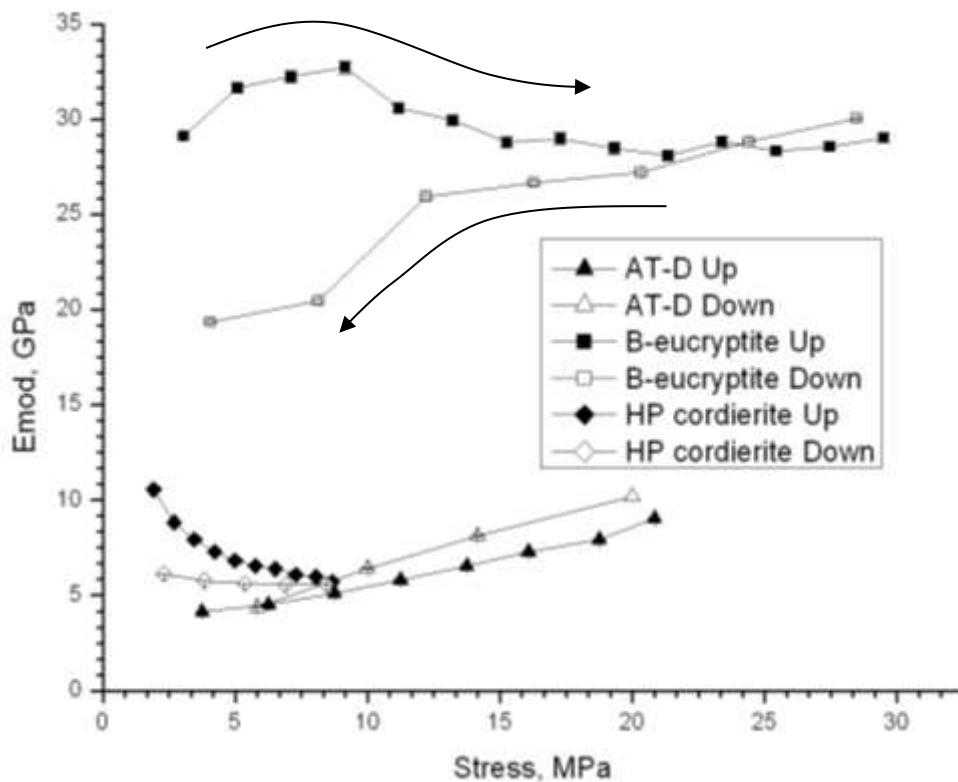
Thermal behavior and its modeling

Microstructural aspects

# Stress-strain curves



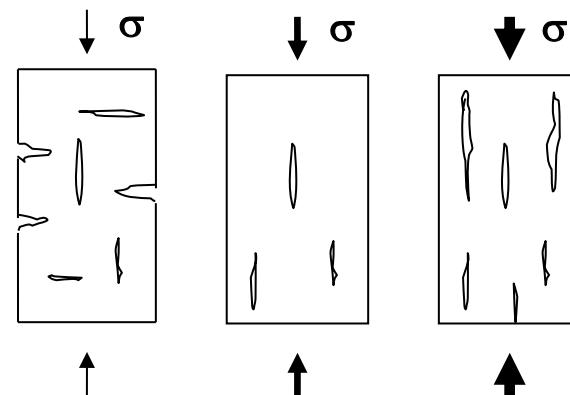
# New constitutive laws for porous and microcracked ceramics



Emod vs load:

- increases continuously for AT
- decreases continuously for UHPC
- has two regimes for  $\beta$ -eucryptite

From  $\mu$ -crack closure to opening



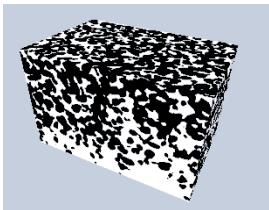
- Stress Modeling needs to take the dynamic behavior into account
- Operating conditions cannot be described by static properties
- Mechanical microcracks are irreversible and cannot be closed by load release: they are directional and larger

# Modeling (AT)

## Micromechanics: Differential Scheme

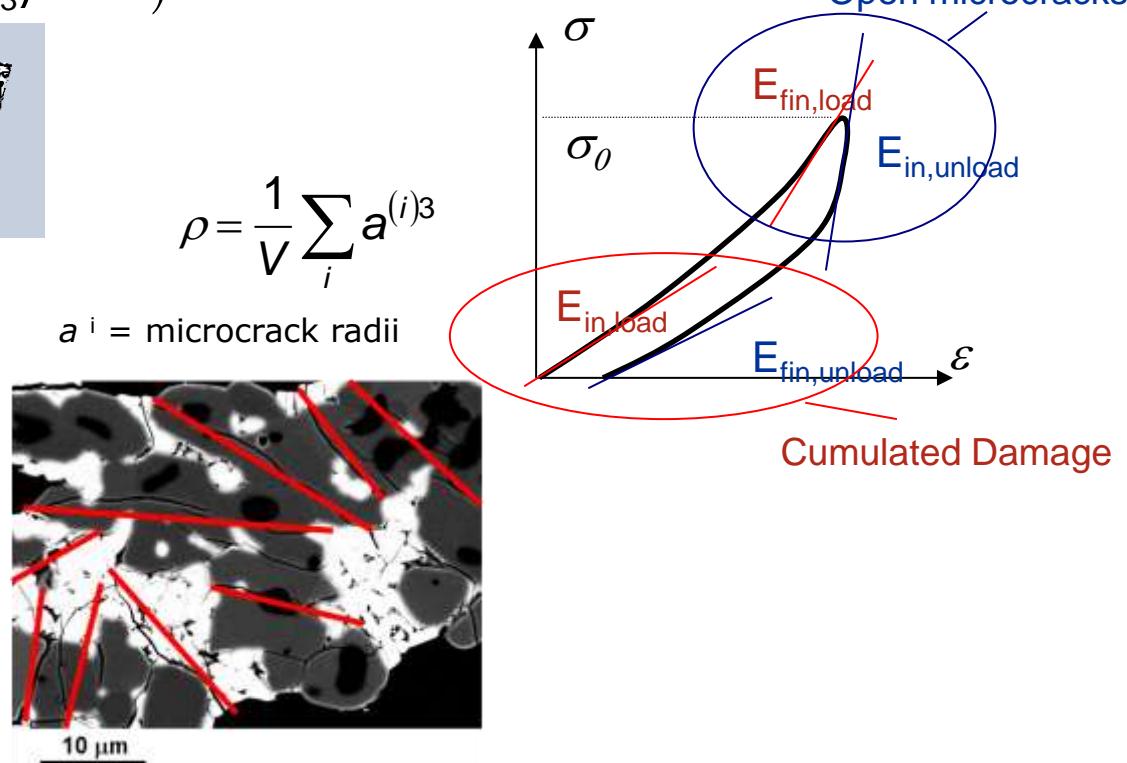
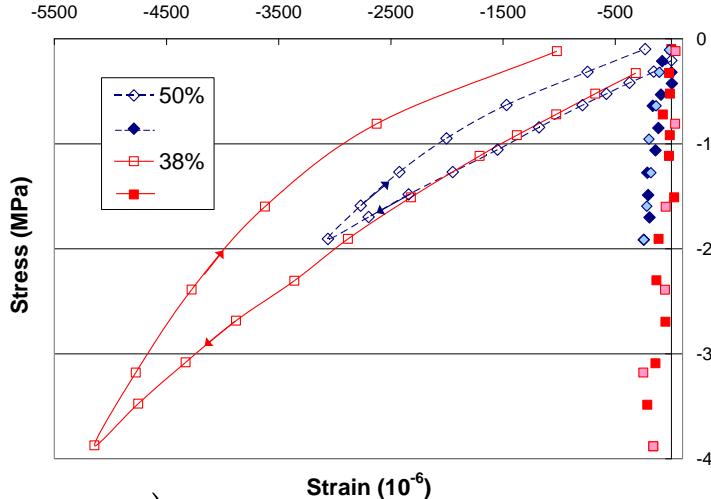
$$\frac{E_0}{E_{\text{eff}}} = (1 - p)^{-C_1} \cdot \exp(C_2 \rho^{\text{open}} + C_3 \rho^{\text{sliding}})$$

From tomography



Density Parameter	Theory + Stress-Strain Curves	
	Porosity (%)	
38	50	
$\rho^{\text{open}, \text{initial}}$	1.44	1.17
$\rho^{\text{open}, \text{peak}}$	1.01	0.97
$\rho^{\text{sliding}, \text{peak}}$	1.08	0.83

$$\rho^{\text{open}, \text{peak}} + \rho^{\text{sliding}, \text{peak}} > \rho^{\text{open}, \text{initial}}$$



# Mechanical Properties Summary

---

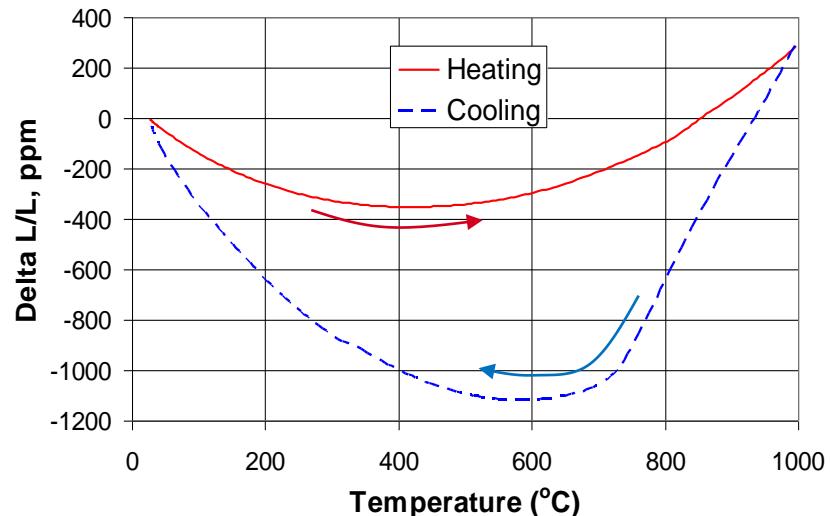
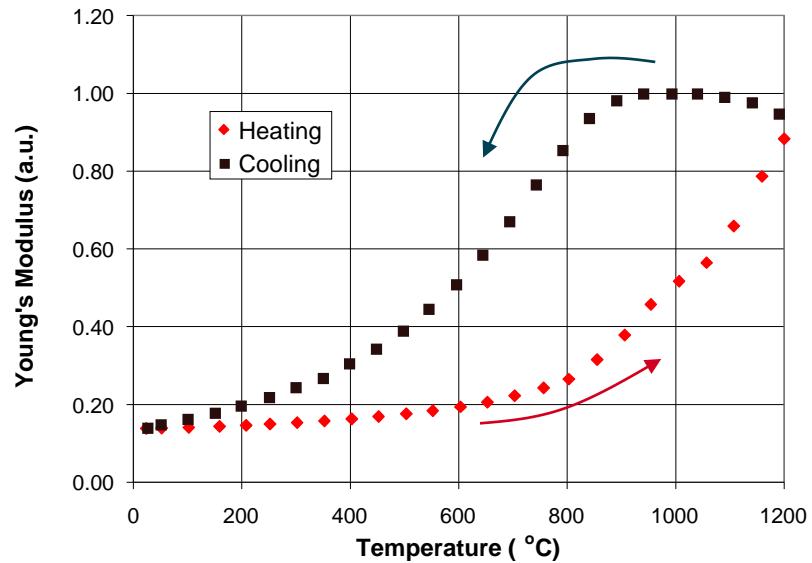
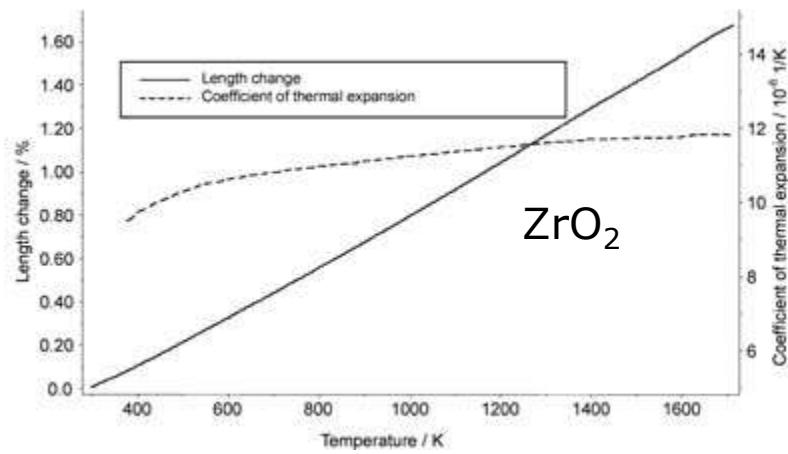
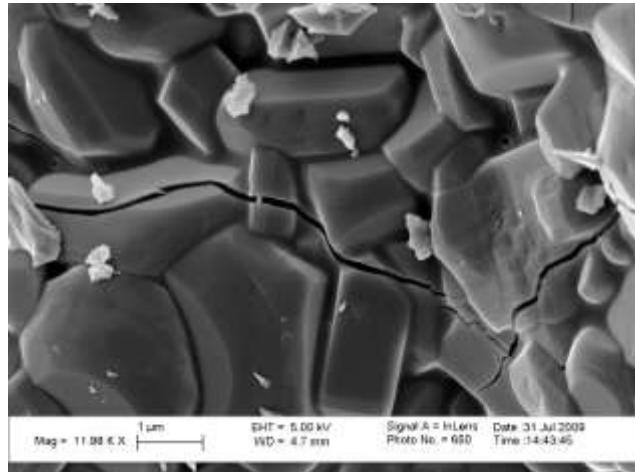
- **New relations** between macro and micro stress and strain for porous materials
- Microcracking induces a viscous behavior (stress-strain curves become time dependent)
- At least two parameters are needed to describe the  $E$  vs.  $p$
- Differential model yields microcrack density (agreement with Eshelby approach on Emod vs T data): microcrack sliding is extremely important
- Diffraction Young's modulus rescales with porosity

Mechanical behavior and its modeling

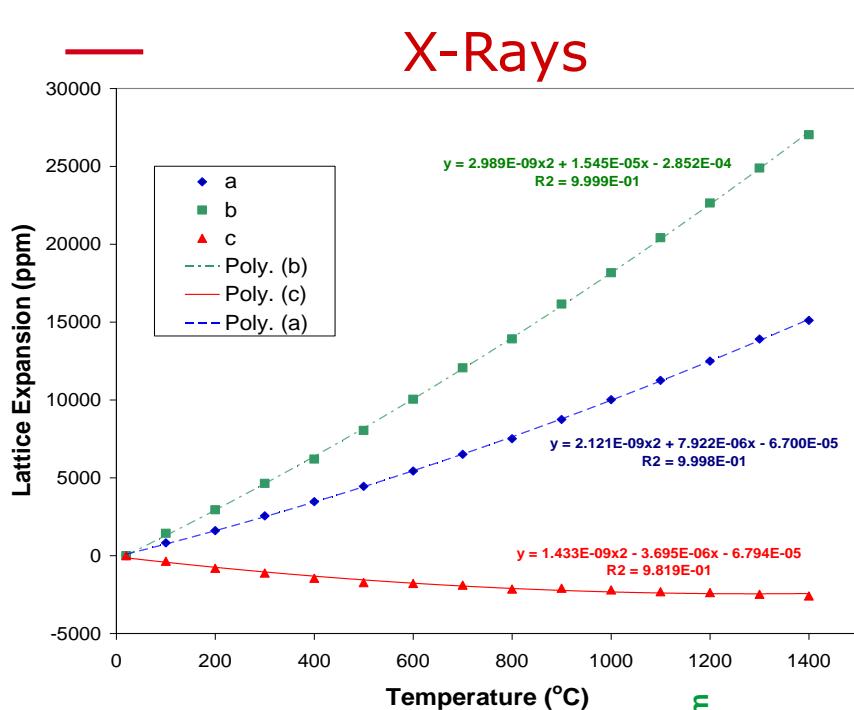
Thermal behavior and its modeling

Microstructural aspects

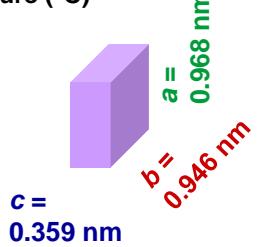
# Thermal expansion of Aluminum Titanate



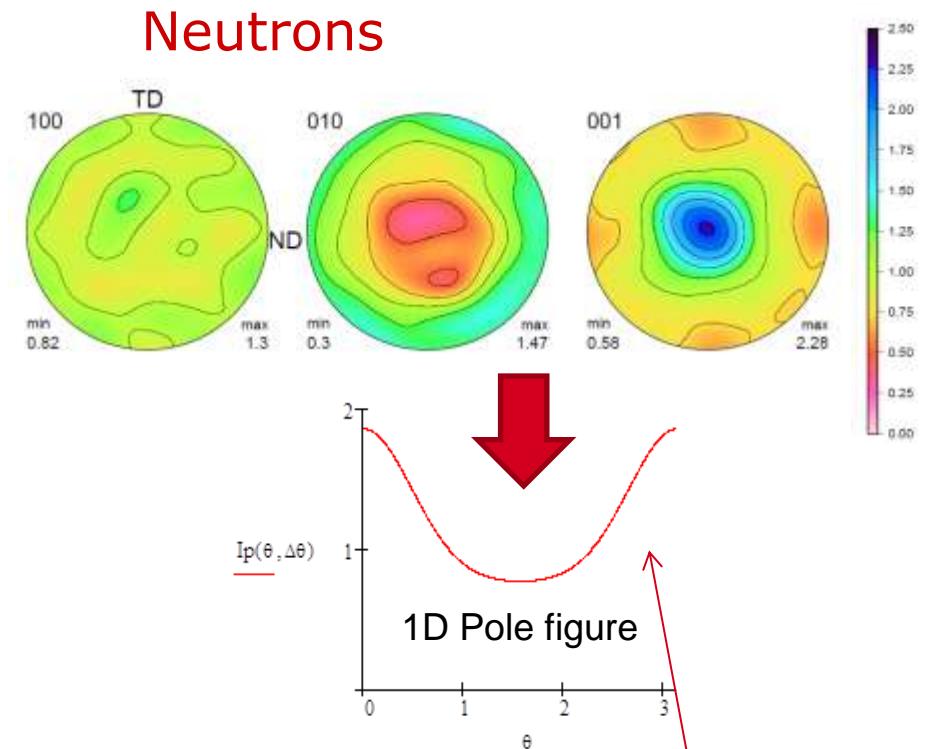
# Lattice expansion and Texture of AT



- Different a,b,c
- Negative c-axis



**Integrity Factor model** (Efremov, Phil Mag., 2013)  
AT macroscopic axial CTE simulation

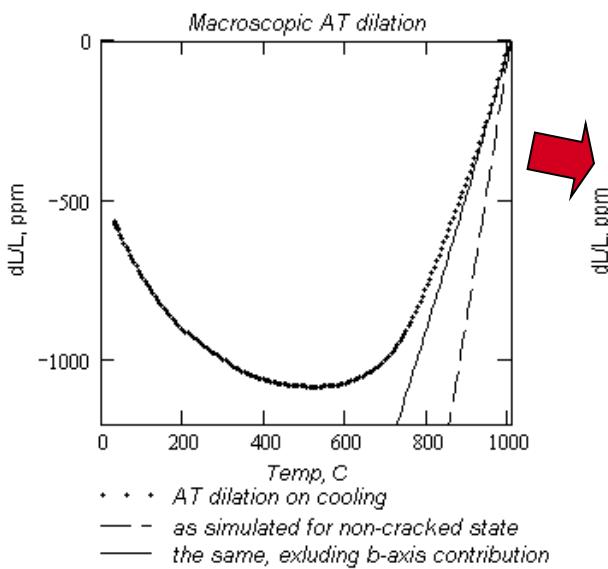


$$\varepsilon^{bulk} = \frac{\sum \varepsilon^{lattice}_i \cdot IF_i \cdot V_i \frac{E_i}{E_{Pi} + E_i}}{\sum IF_i \cdot V_i \frac{E_i}{E_{Pi} + E_i}}, \quad \sum V_i \cdot \sigma_i = 0$$

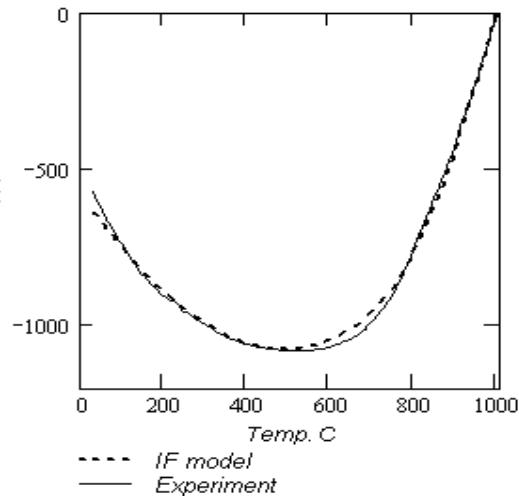
$$\sigma_i = (\varepsilon^{bulk} - \varepsilon^{lattice}_i) \cdot IF_i \cdot \frac{E_i \cdot E_{Pi}}{E_{Pi} + E_i} \cdot A$$

# Modeling

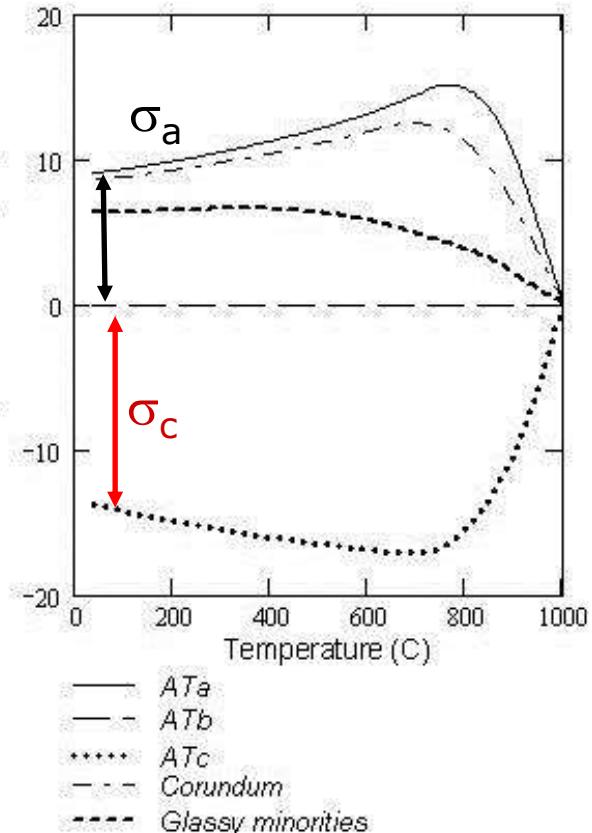
## IF model- Matching the slope at HT



## IF model- dilation curve



## IF model- stress



- At all temperatures the **c-axis** remains attached to the body and is under **compression**
- Even at high temperatures the **b-axis** must be **disconnected**
- At RT, the **c-axis** is under **compression**, the **others** are under **tension**

# Thermal Properties Summary

---

- **Mechanical and thermal microcracks** have different orientations
- Aluminum titanate behaves highly anisotropically: internal micro-stresses
- The **Integrity Factor Model** can rationalize the high-temperature behavior of Thermal Expansion and calculate stresses

Mechanical behavior and its modeling

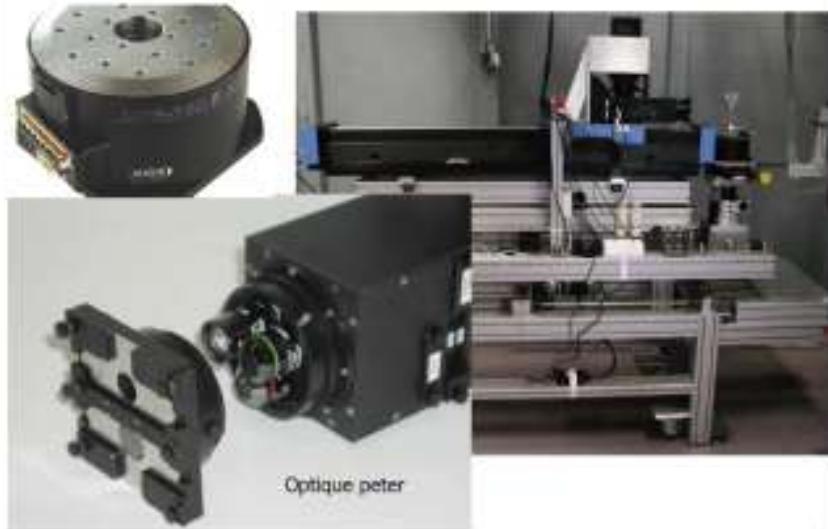
Thermal behavior and its modeling

Microstructural aspects

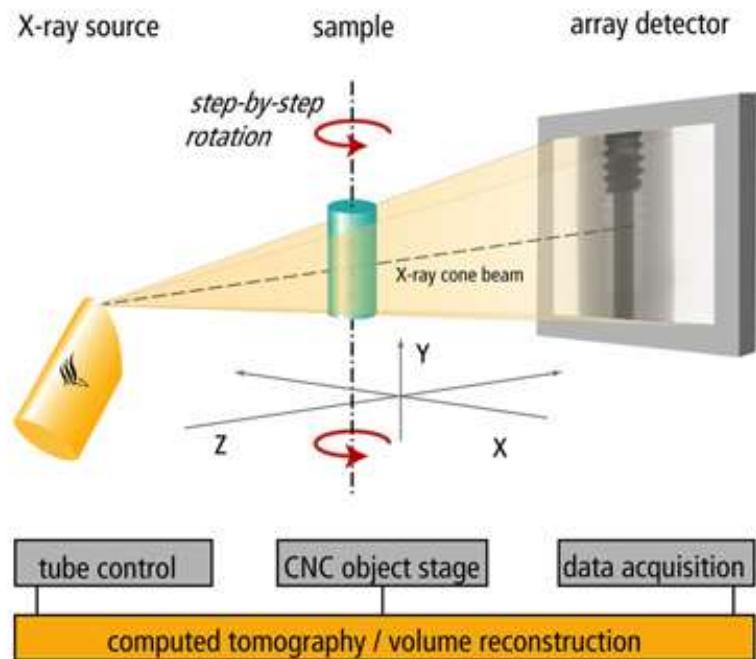
# Pore orientation by means of Computed Tomography



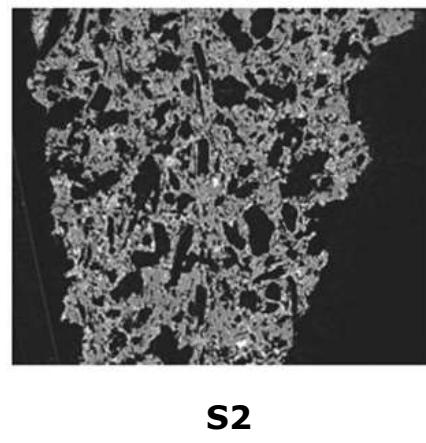
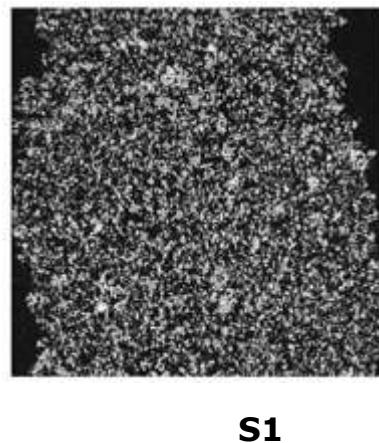
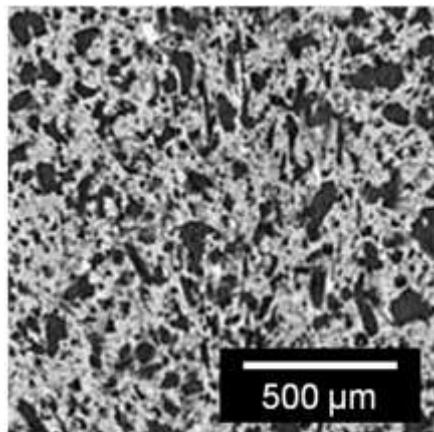
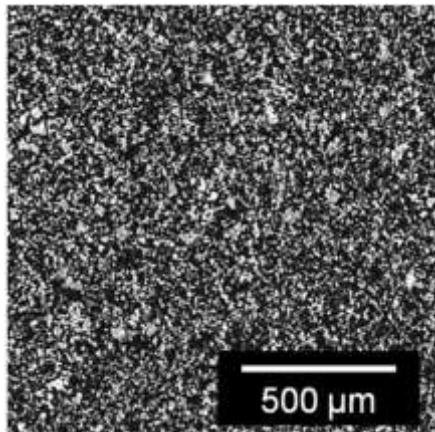
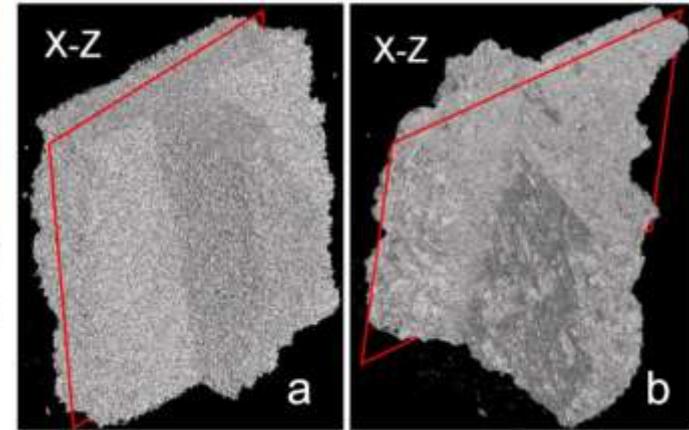
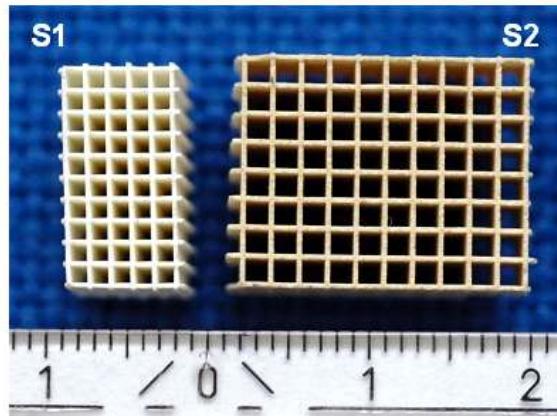
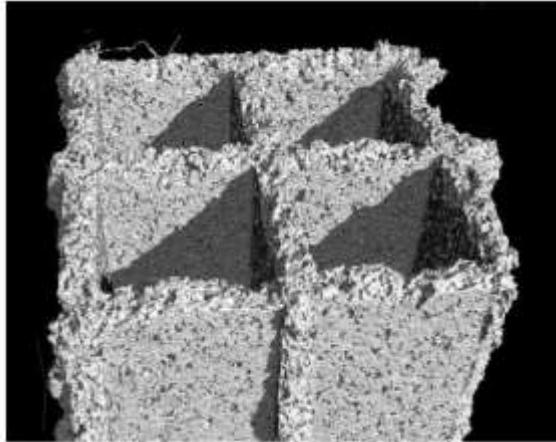
GE v|tome|x  
Pixel size ~ 4 mm



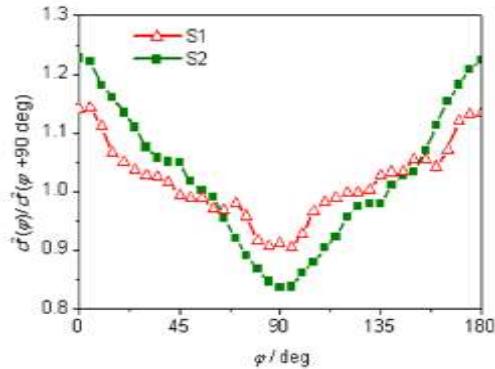
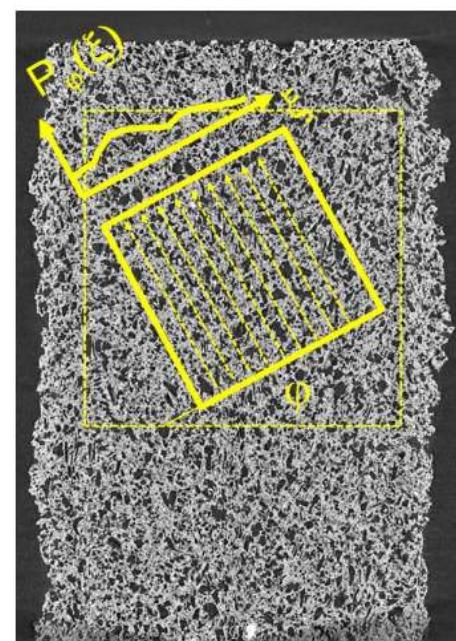
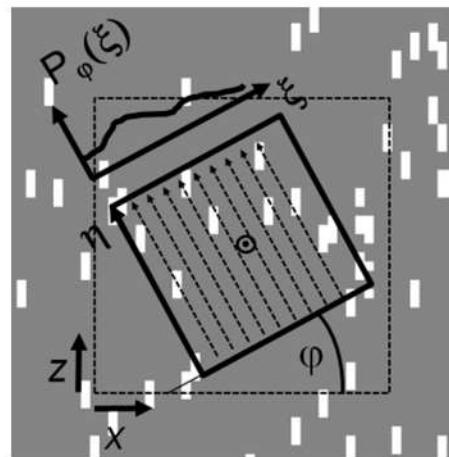
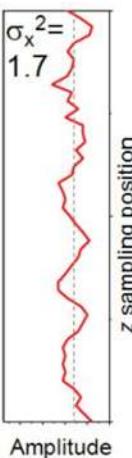
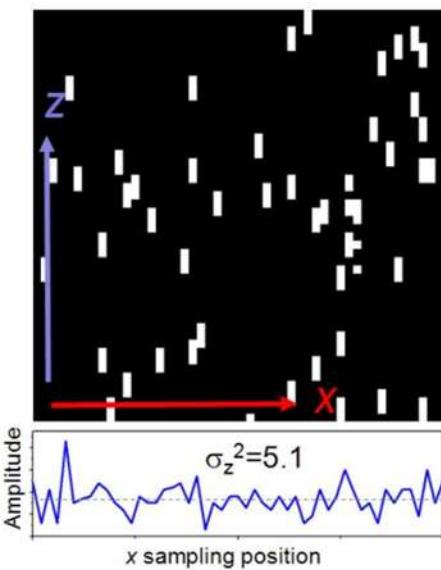
BAMLine, BESSY, Berlin,  
Germany  
Pixel size ~ 0.4 mm



# Results- CT reconstructions



# CT Data Analysis: DIVA



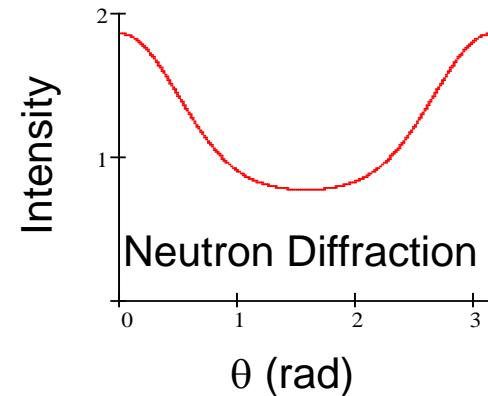
	X-ray Refraction (  /⊥)	μ-CT DIVA (  /⊥)	Synch. CT (  /⊥)	Neutron Diffraction
S1	0.92	0.92	0.85	-
S2	0.86	0.84	0.74	0.77

- Calculation of the Variance of Gradients

$$\sigma_P^2(\varphi) = \frac{\sum_{\xi_i}^n (P_\varphi(\xi_i) - \langle P_\varphi \rangle)^2}{n}$$

$$P_\varphi(\xi) = \int_V |\nabla \mu(\mathbf{r})| d\eta$$

- Orientation parameter  $O_D$  by ratio of max to min variance



**Morphology and crystal orientations coincide**

# Microstructure Summary

---

- **Morphological and crystallographic** orientations are the same in cordierite
  - High resolution CT yields more complete information, yet not substantially different
  - Integral information is as valuable as local one
-

# Conclusions

---

- DPF (complex) materials need high resolution techniques at multi-scale levels
  - One technique (or even a few techniques) is not enough
  - Do not forget the MACRO scale
- Neutrons (and Synchrotrons) are very powerful tools, yet
  - ONLY in combination with others
  - *In-situ* is a MUST
- Modeling is necessary to capitalize experimental data

Questions = Interest

---