

Materials for Future Fusion Reactors under Severe Stationary and Transient Thermal Loads

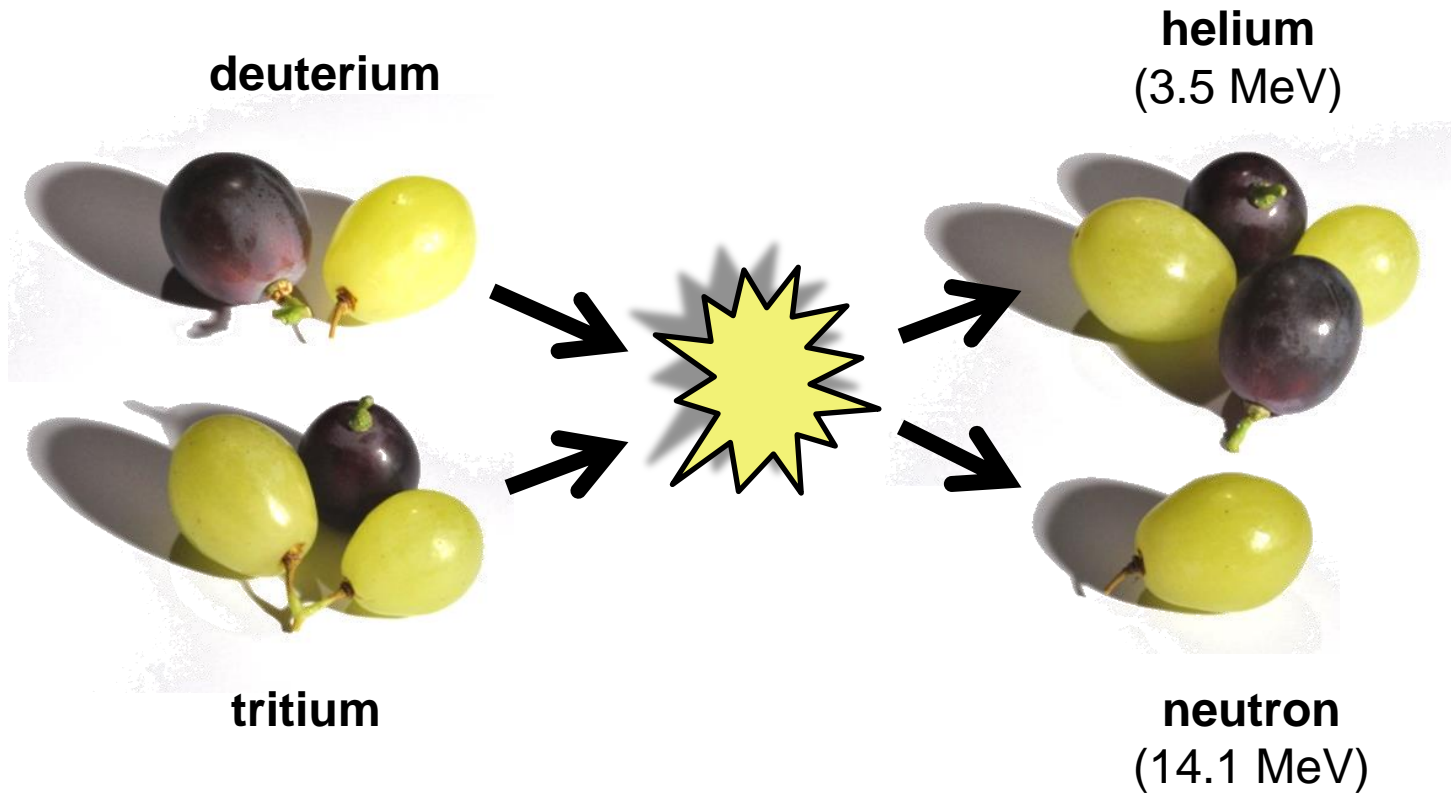
J. Linke, J. Du, N. Lemahieu, Th. Loewenhoff, G. Pintsuk, B. Spilker, T. Weber, M. Wirtz

Forschungszentrum Jülich, Institut für Energie- und Klimaforschung, 52425 Jülich

Mysterious fusion

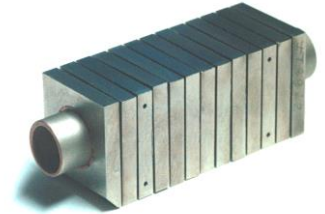


Mysterious fusion

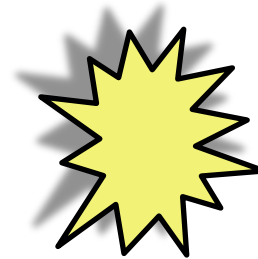


Outline:

A Thermal loads on plasma facing components



B Simulation of intense thermal loads



C Hydrogen and helium effects



D Material degradation by energetic neutrons

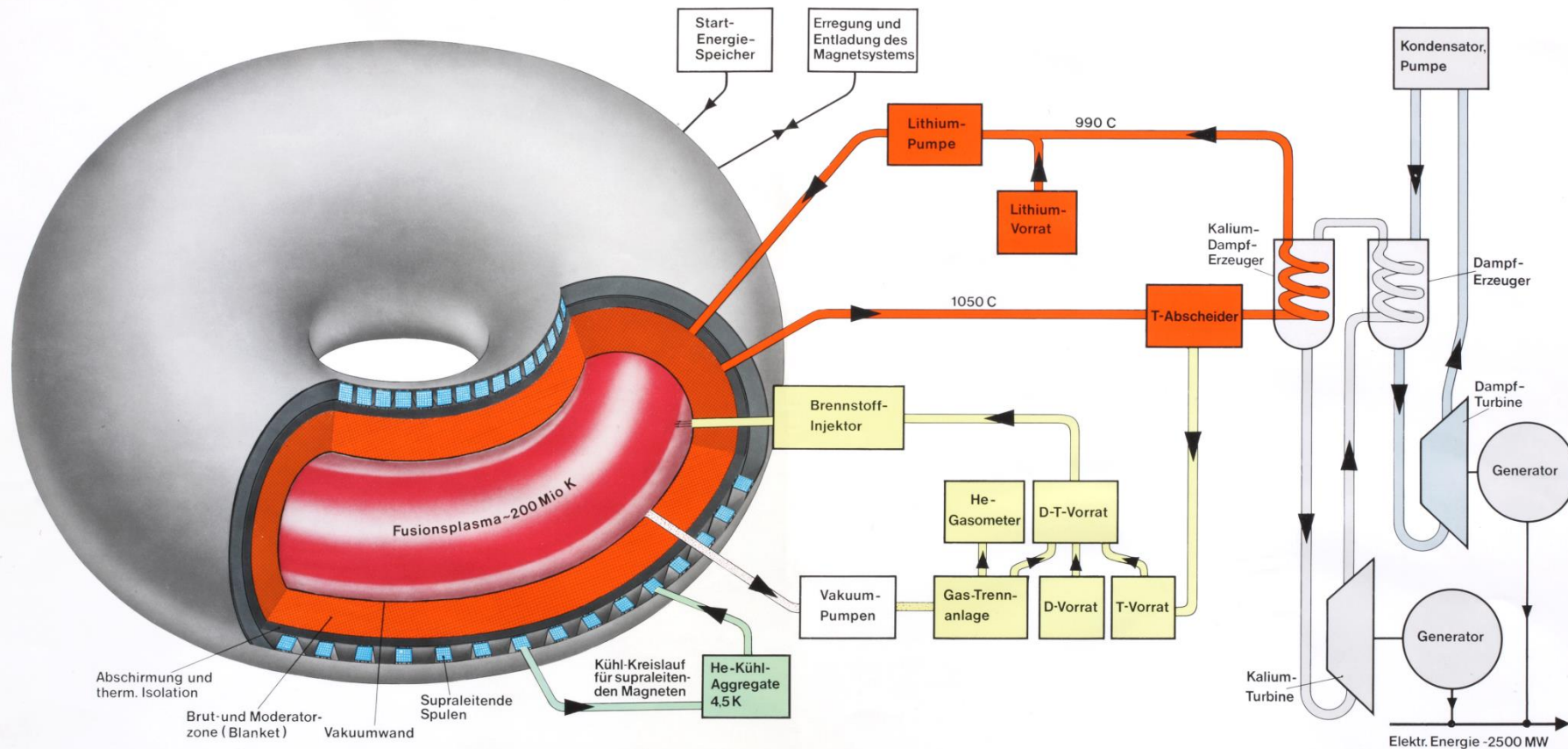


A

**Thermal loads on
plasma facing components**

Energy conversion in a thermo-nuclear reactor

Institut für Plasmaphysik · Garching 1970

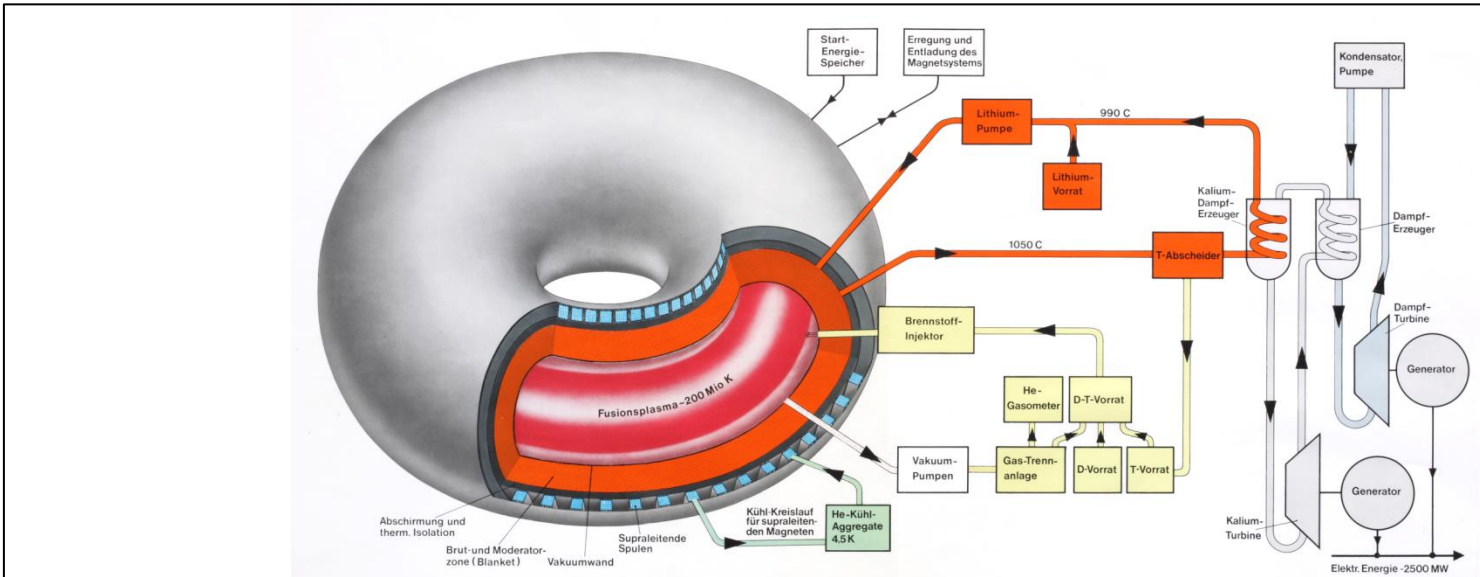


Prinzipieller Aufbau eines Fusionskraftwerkes $N = 5 \text{ GW}_{\text{th}}$

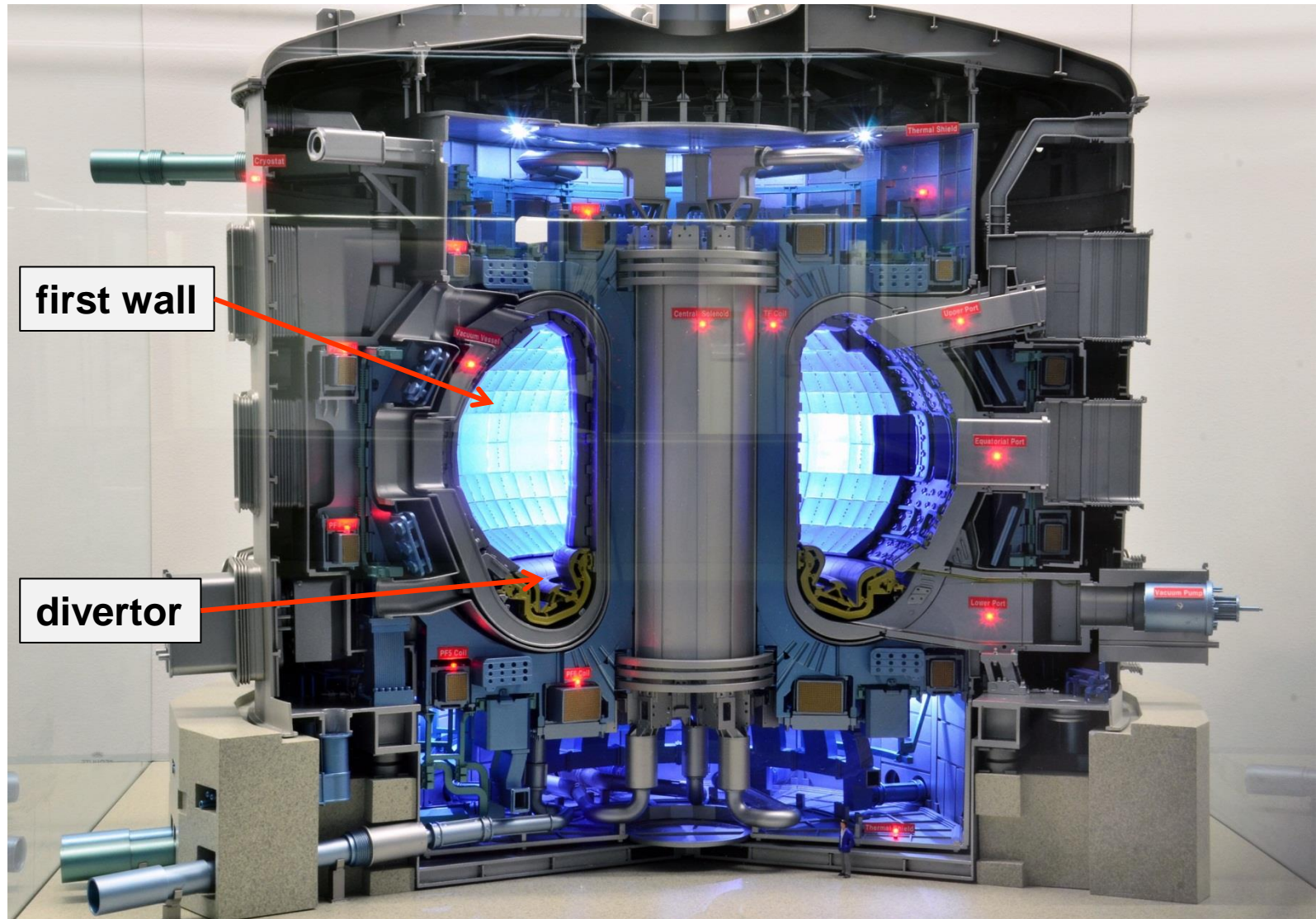
Torusdaten: Aussendurchmesser 18m · Rohrdurchmesser 7m

Steps towards the reactor

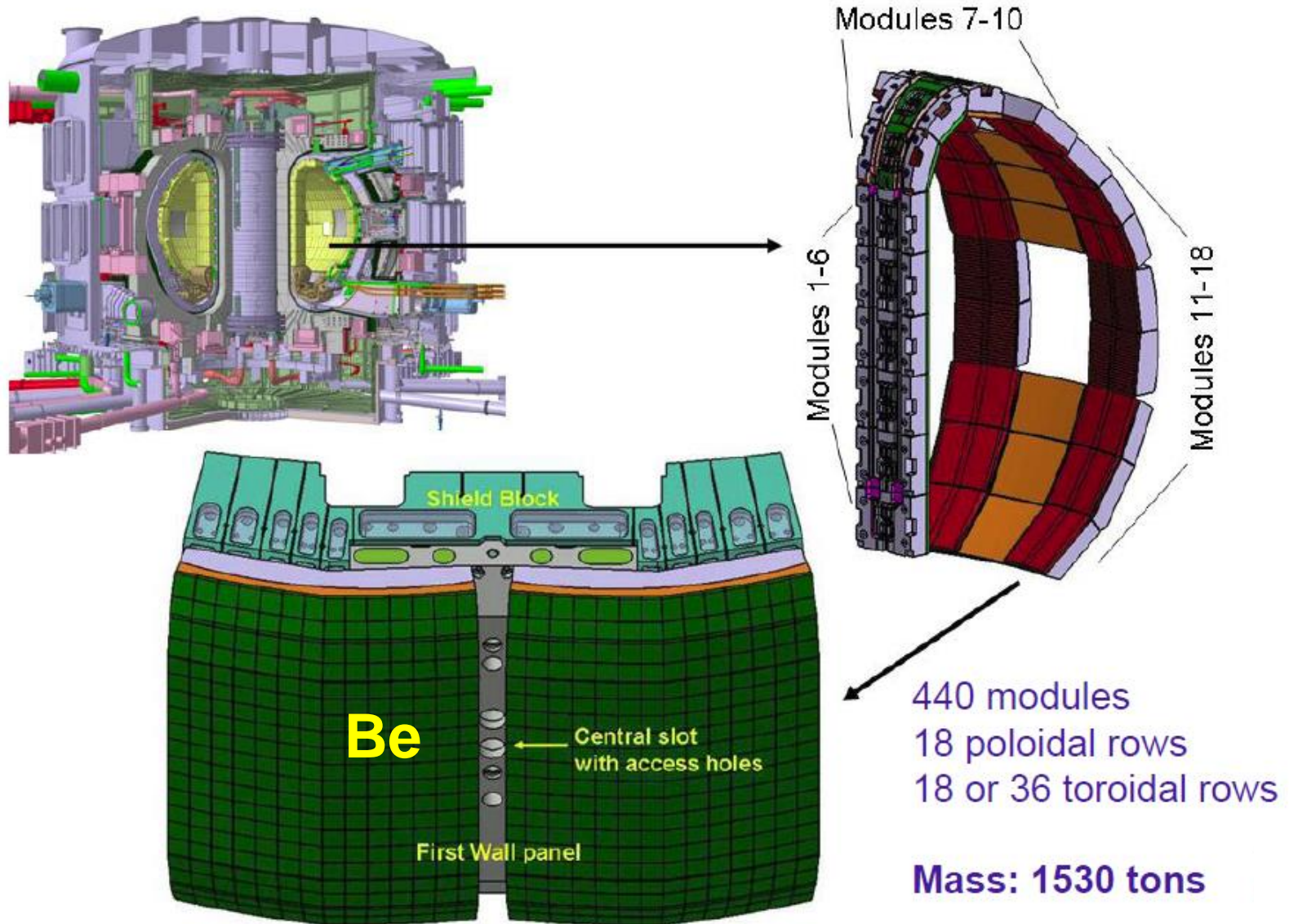
JET	ITER	DEMO
n-dose: 10^{-9} dpa	1 dpa	100 dpa



ITER and the plasma facing components

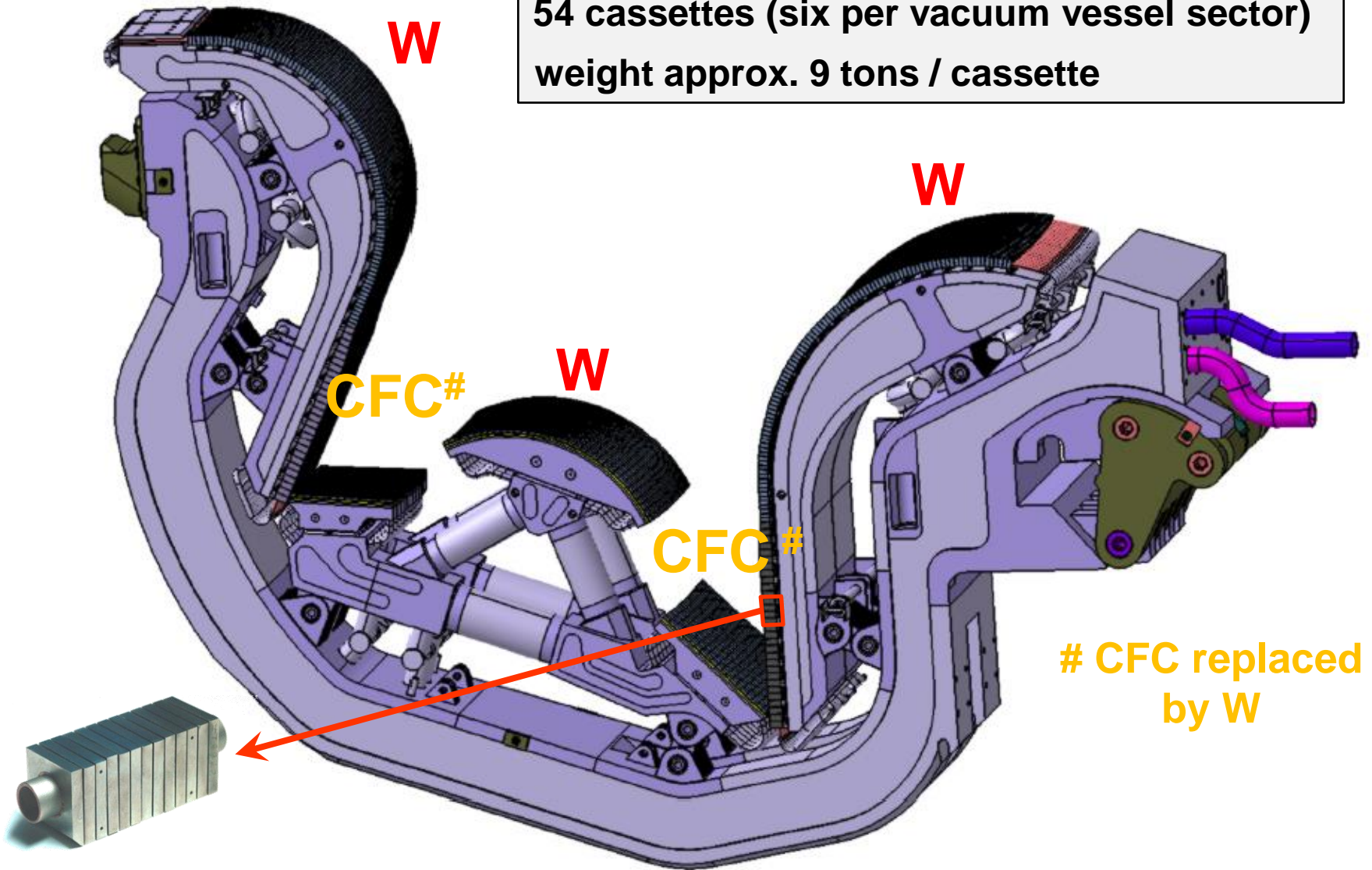


The ITER blanket design



The new ITER divertor cassette

54 cassettes (six per vacuum vessel sector)
weight approx. 9 tons / cassette

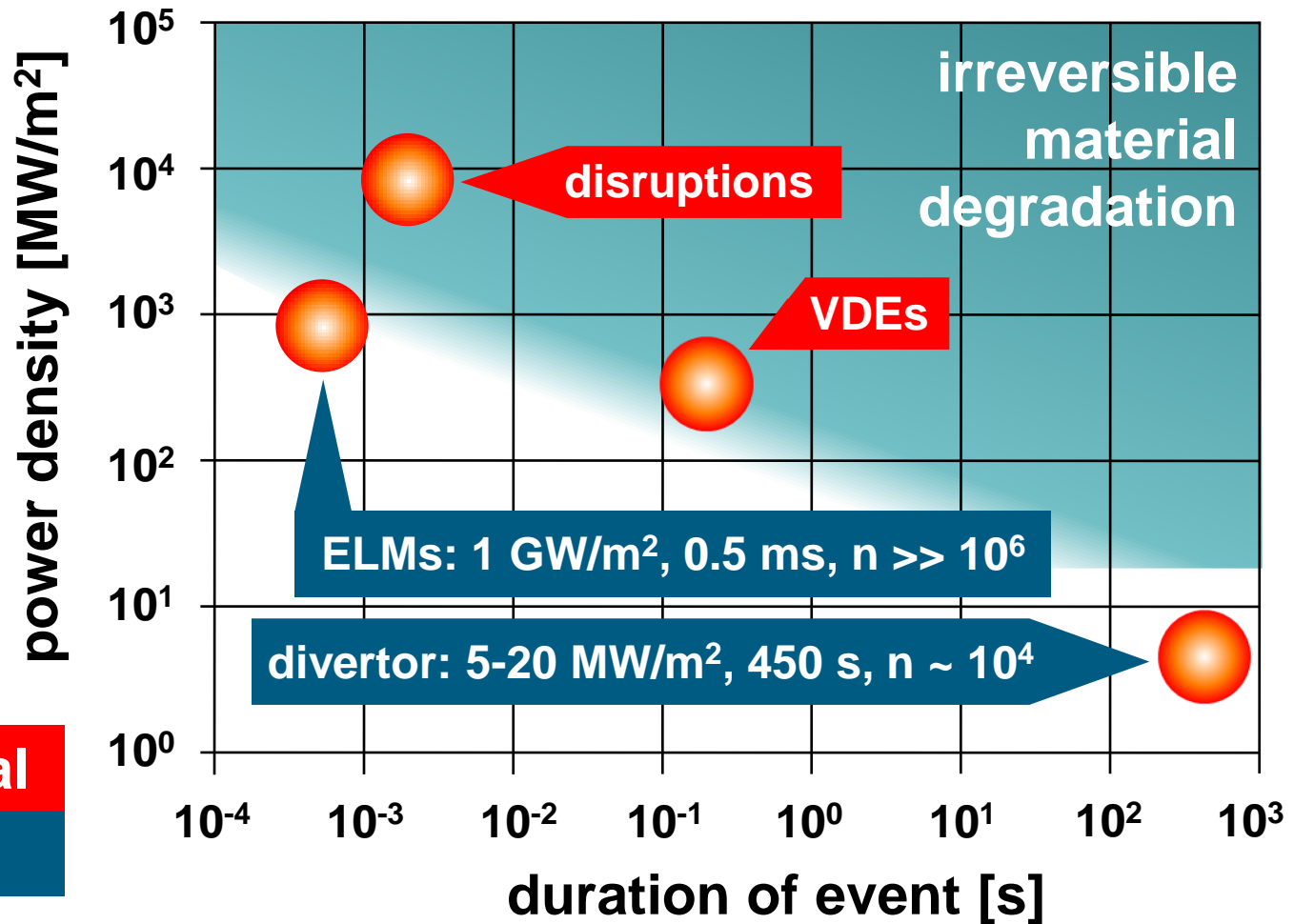


$L_{\max} \leq 100 \text{ mm}$

B

**Simulation of intense thermal loads
on plasma-facing components**

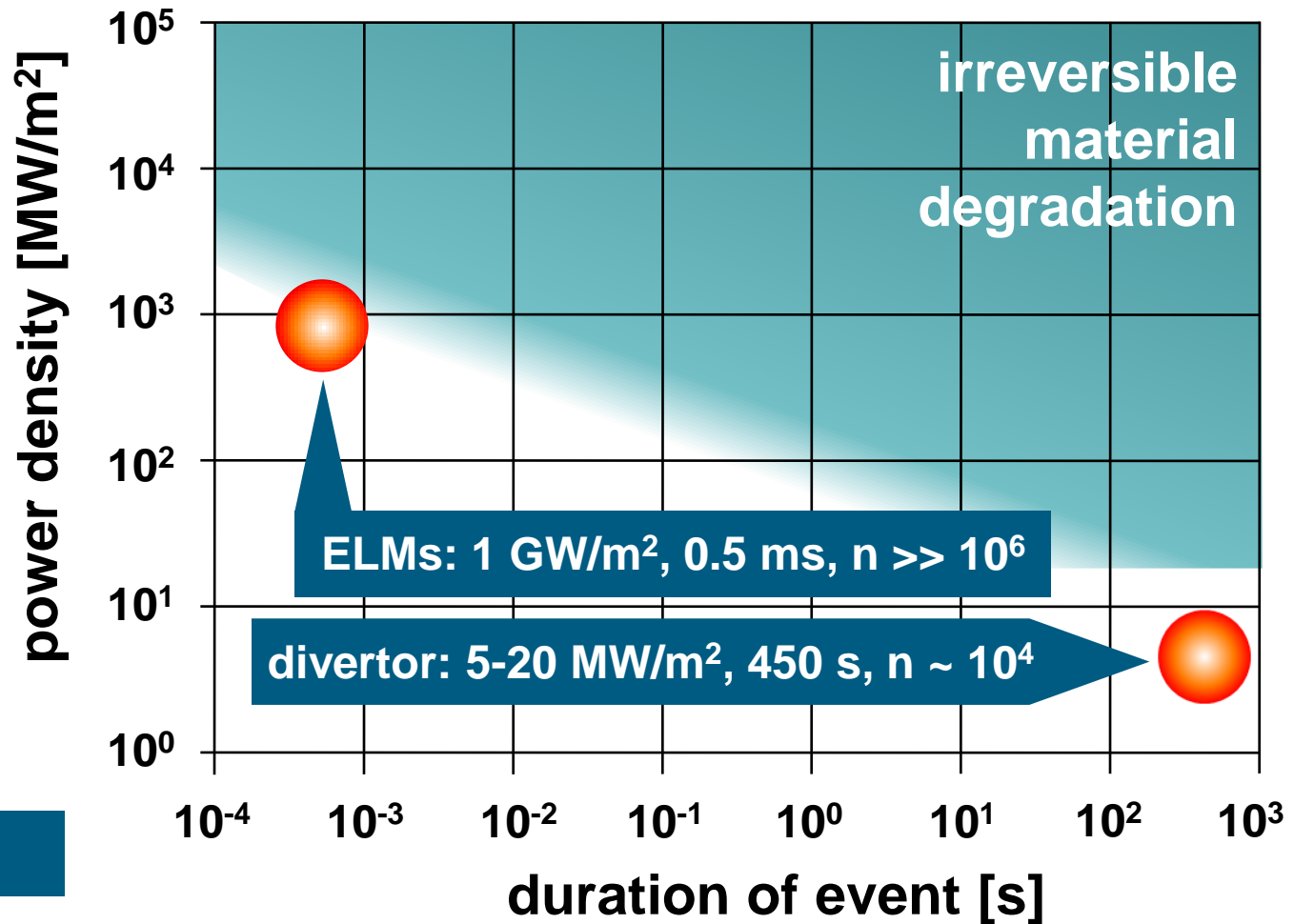
Expected heat loads on the ITER divertor



off-normal
normal

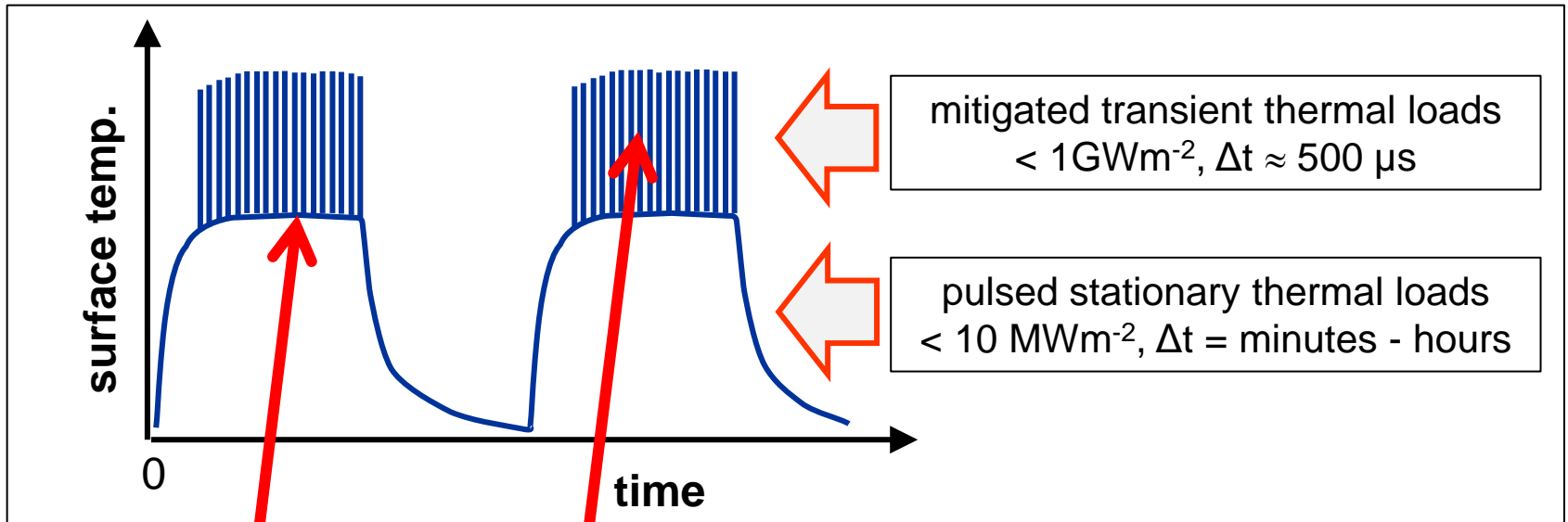
R. A. Pitts, et al., Journal of Nuclear Materials 438 (2013) S48-S56
J. Linke, Transactions of fusion science and technology 49 (2006) 455-464
A. Loarte et al., Plasma Physics and Controlled Fusion 45 (2003) 1549-1569

Expected heat loads on the ITER divertor



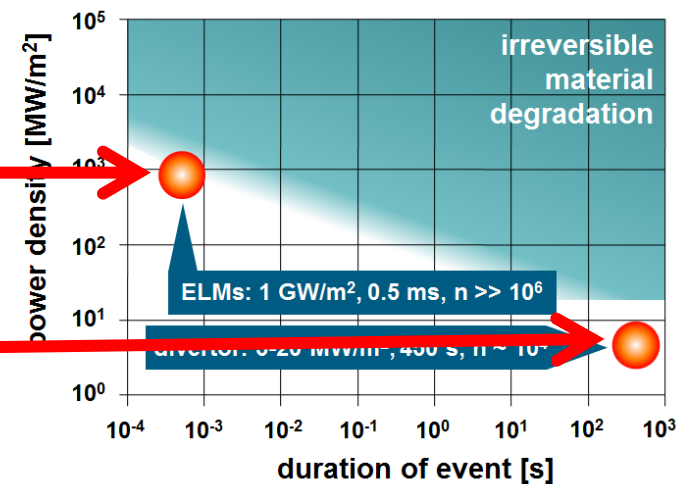
normal

Wall loading in a toroidally confined plasma (Tokamak)



thermal shock
cracking/melting
of PFM-surface

thermal fatigue
joints between PFM
and heat sink



Loads on plasma facing components



very high
thermal
loads

plasma
exposure

neutrons

Steady state heat loads:

up to 20 MWm^{-2} in ITER
(lower loads in DEMO)

- recrystallization
- failure of joints

Transient thermal loads:

up to 60 MJm^{-2}
(disrupt., ELMs, VDEs)

- crackings
- melting
- dust formation

**very high
thermal
loads**

**plasma
exposure**

neutrons

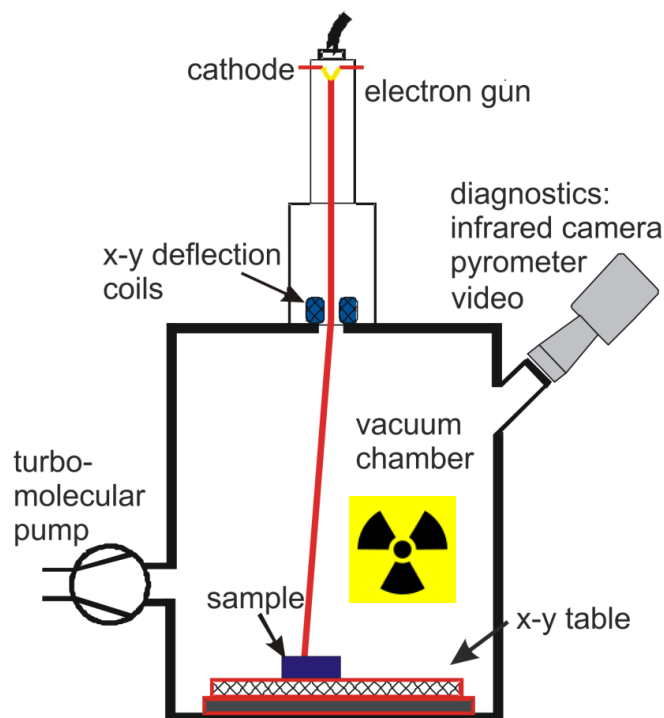
Plasma loads:

- sputtering
- hydrogen
- helium

Neutrons:

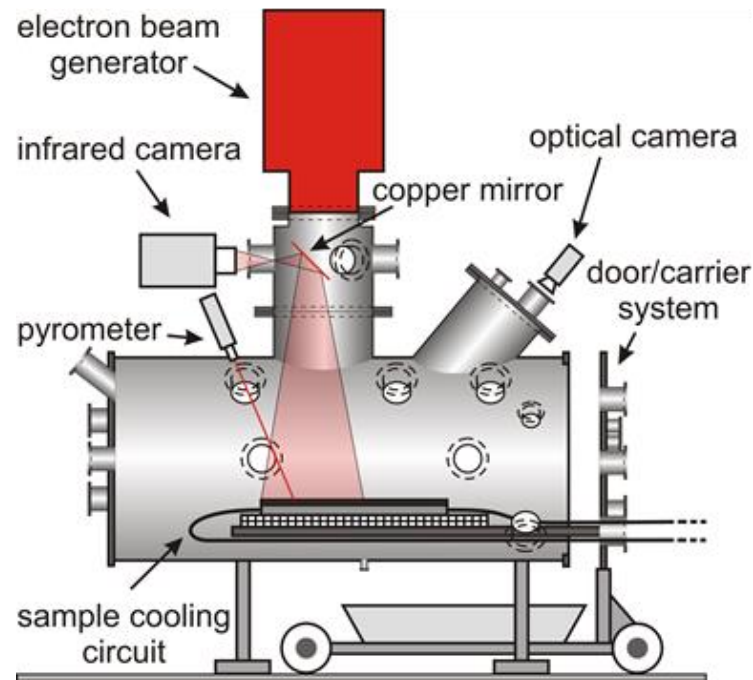
- up to 14 MeV
- defects
- transmutation

Electron beam facility JUDITH 1



- max. power 60 kW
- acceleration voltage < 150 kV
- EB diameter ~1 mm FWHM
- loaded area 10 x 10 cm²

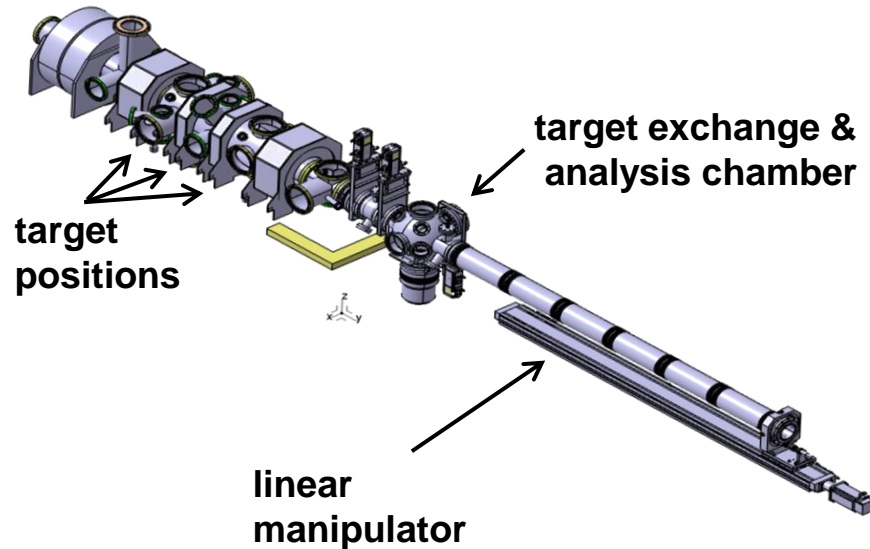
Electron beam facility JUDITH 2



- max. power 200 kW
- acceleration voltage 30 – 60 kV
- EB diameter ≤ 5 mm FWHM
- loaded area 40 x 40 cm²

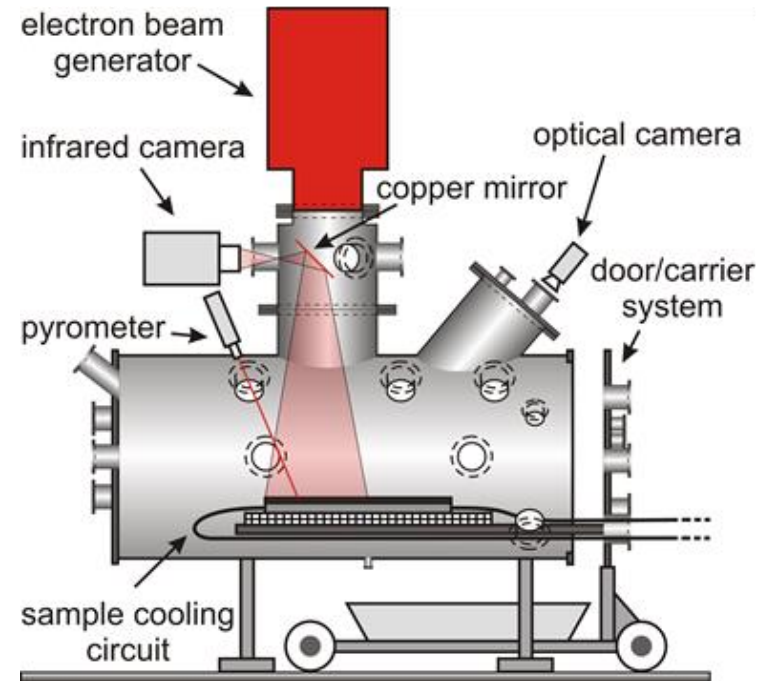
Linear Plasma Device PSI-2

plasma source



- plasma diameter 60 mm
- particle flux $\leq 10^{23} \text{ m}^{-2}\text{s}^{-1}$
- incident ion energy (bias) 10 – 300 eV
- Nd:YAG laser 1064 nm
- laser energy 32 J

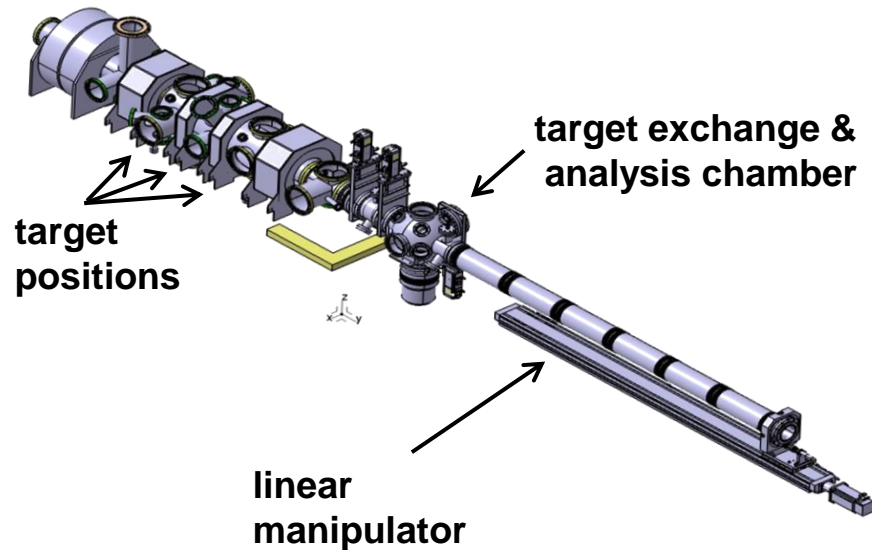
Electron beam facility JUDITH 2



- max. power 200 kW
- acceleration voltage 30 – 60 kV
- EB diameter $\leq 5 \text{ mm FWHM}$
- loaded area $40 \times 40 \text{ cm}^2$

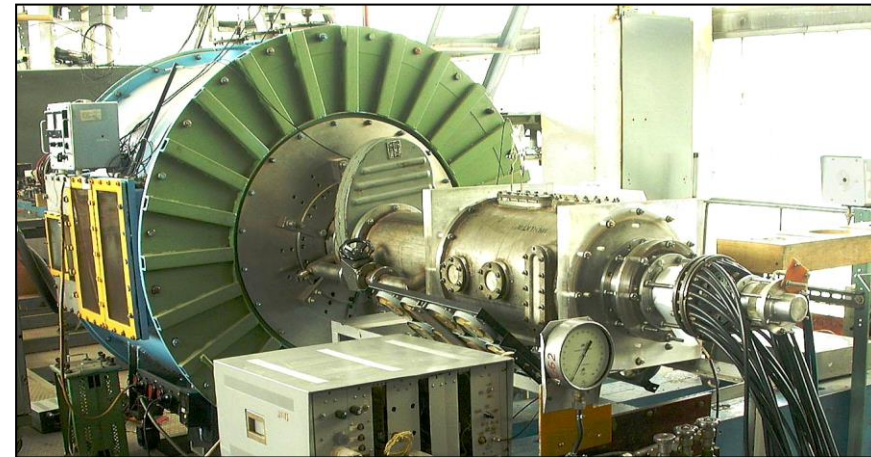
Linear Plasma Device PSI-2

plasma source



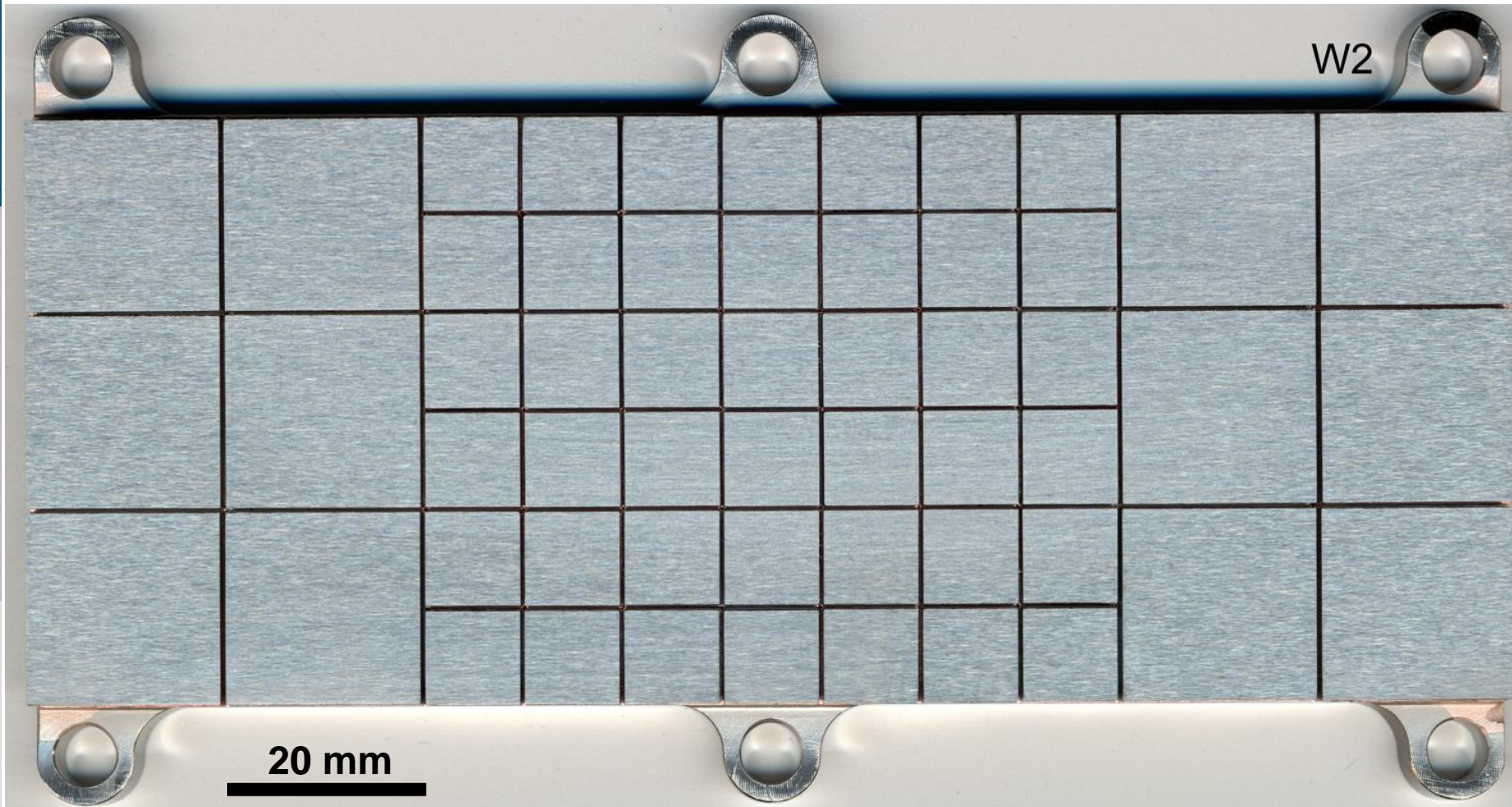
- plasma diameter 60 mm
- particle flux $\leq 10^{23} \text{ m}^{-2}\text{s}^{-1}$
- incident ion energy (bias) 10 – 300 eV
- Nd:YAG laser 1064 nm
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Quasi Stationary Plasma Accelerator (QSPA)



- heat load 0.5 – 2 MJ/m²
- pulse duration 0.1 – 0.6 ms
- plasma diameter 5 cm
- magnetic field 0 T
- ion impact energy $\leq 0.1 \text{ keV}$
- electron temp. $< 10 \text{ eV}$
- plasma density $\leq 10^{22} \text{ m}^{-3}$

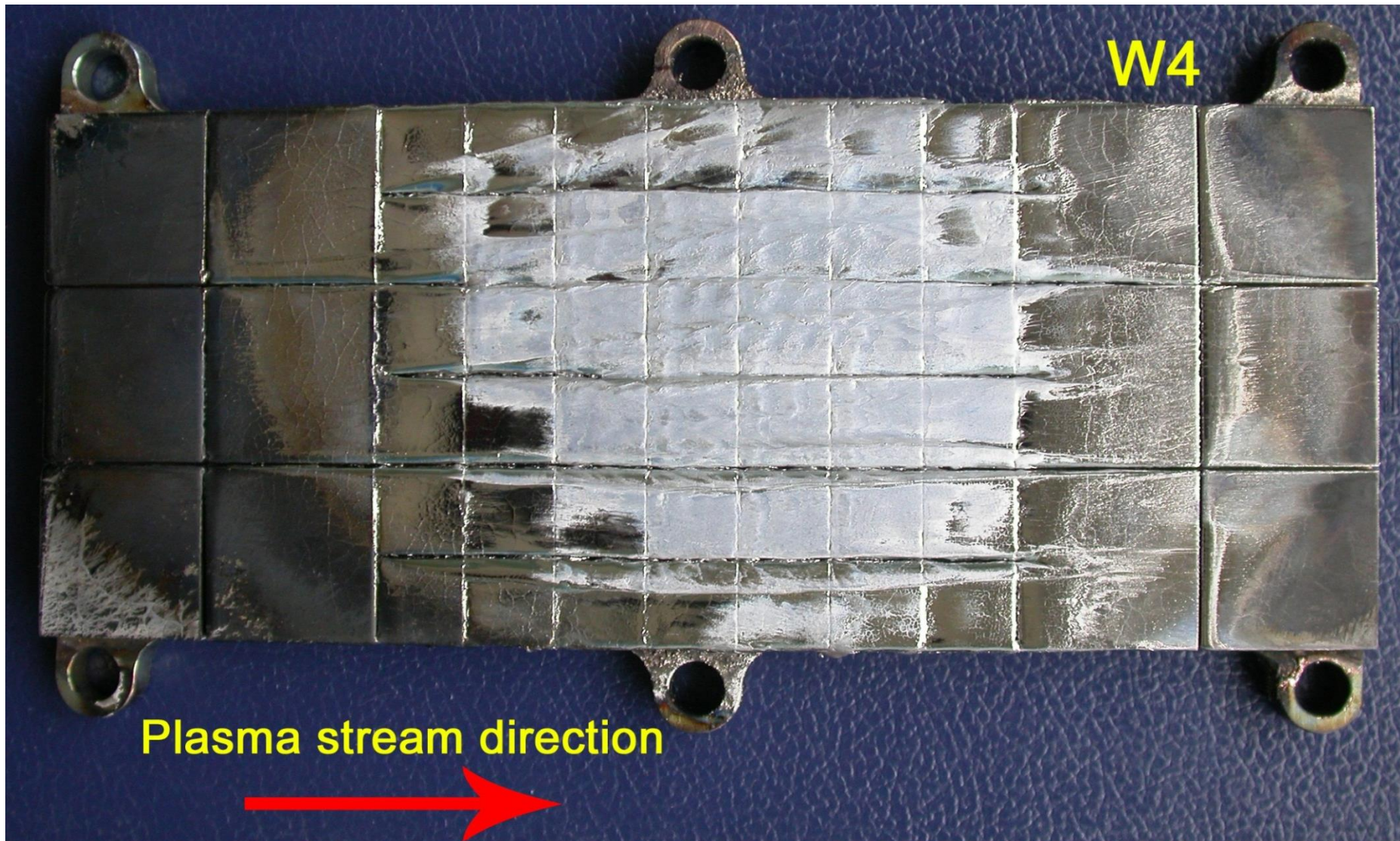
Simulation of ELMs in QSPA



Bridging of gaps due to melt motion

100 pulses @ $E = 1.6 \text{ MJ/m}^2$, $\Delta = 500 \mu\text{s}$

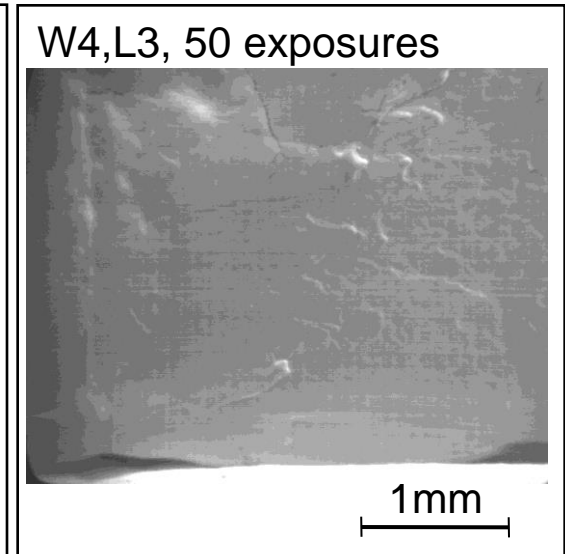
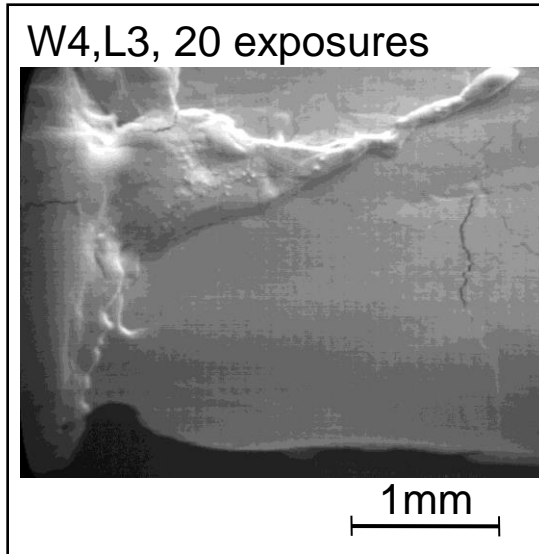
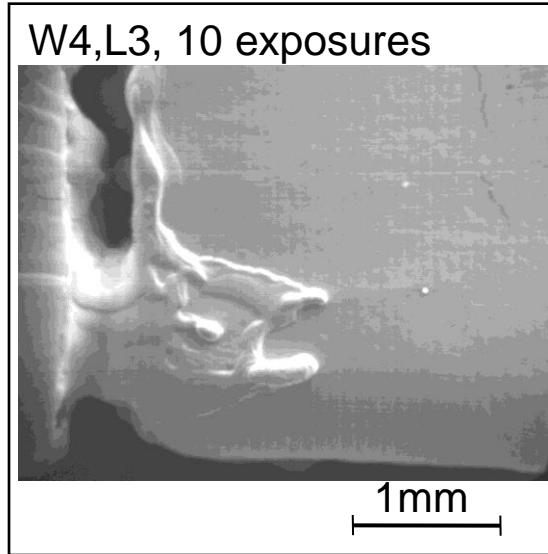
$H_{\text{HF}} = 71 \text{ MW/m}^2\text{s}^{0.5}$



Source: A. Zhitlukhin et al., SRC RF TRINITI, Troitsk

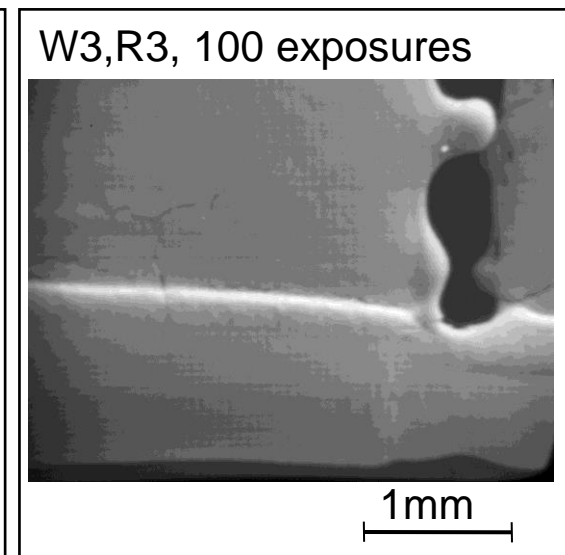
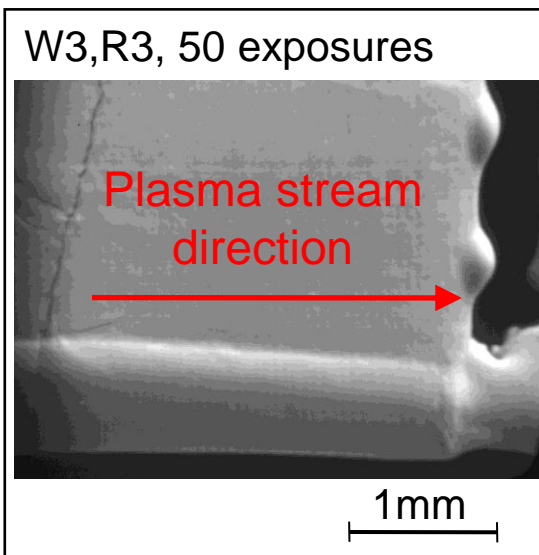
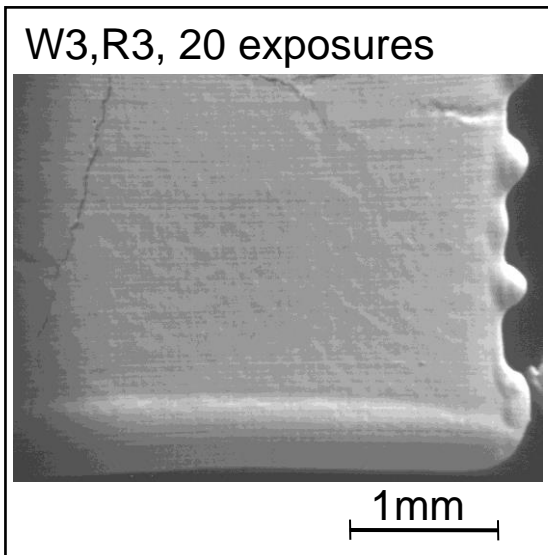
Bridge formation between tungsten tiles

$w = 1.6 \text{ MJ/m}^2$



$H_{HF} = 71 \text{ MW/m}^2 \cdot \text{s}^{0.5}$

$w = 1.0 \text{ MJ/m}^2$



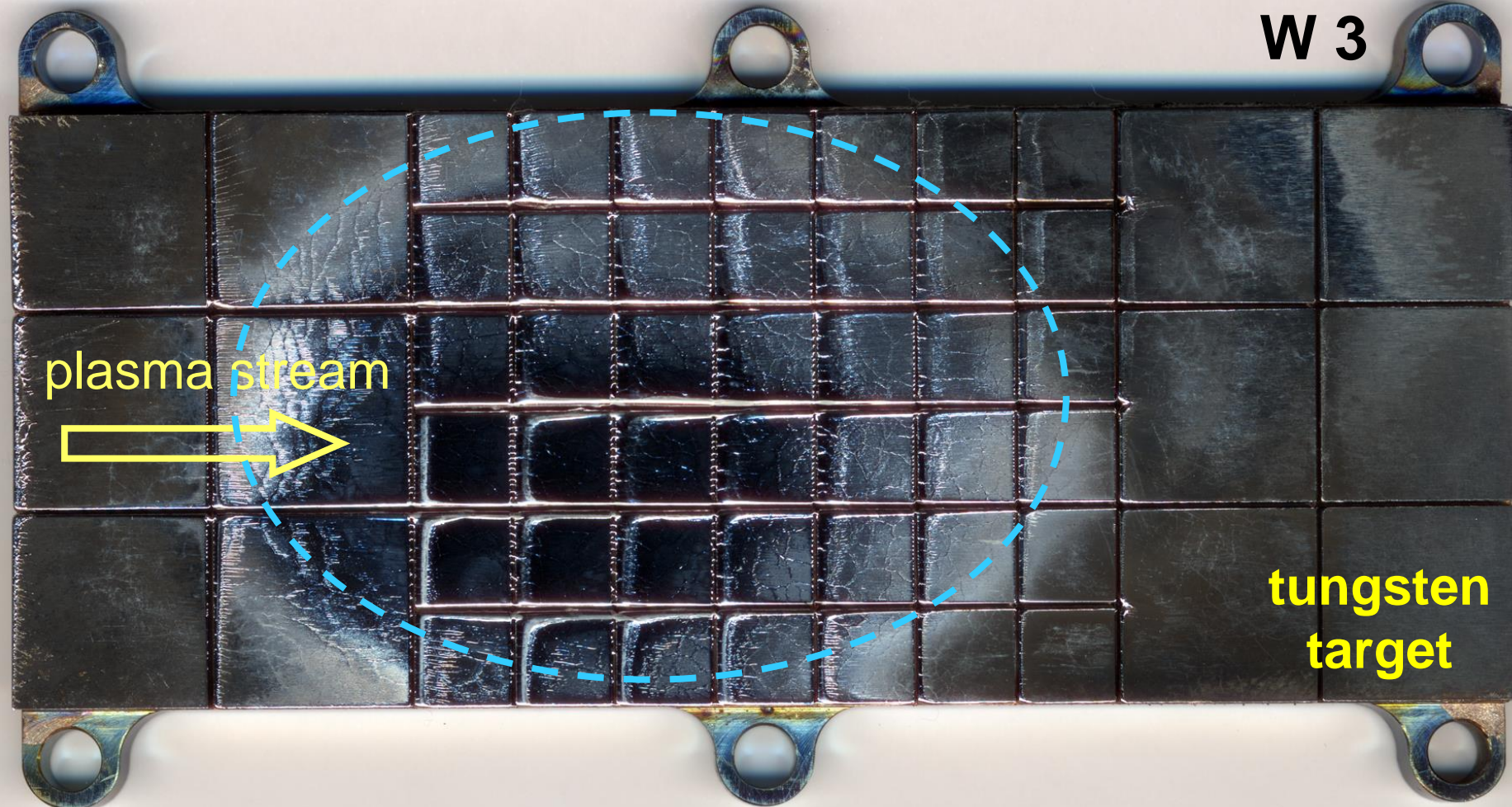
$H_{HF} = 44.7 \text{ MW/m}^2 \cdot \text{s}^{0.5}$

$\Delta t = 500 \mu\text{s}$

Simulation of ELMs in QSPA

$$H_{\text{HF}} = 44.7 \text{ MW/m}^2\text{s}^{0.5}$$

W 3



$$E = 1.0 \text{ MJm}^{-2}$$

$$\Delta t = 500 \text{ } \mu\text{s}$$

100 pulses

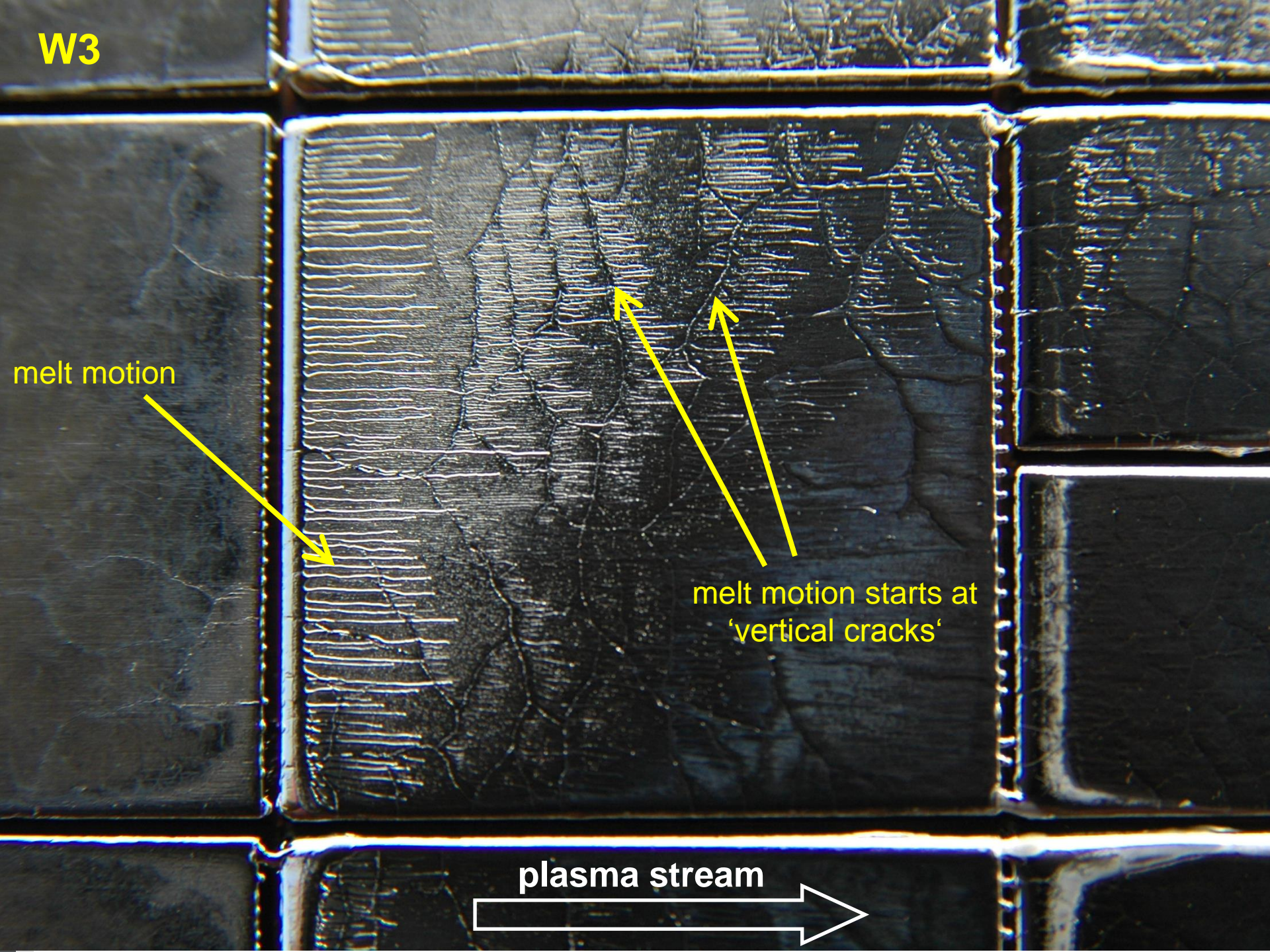
$$T_0 = 500^\circ\text{C}$$

W3

melt motion

melt motion starts at
'vertical cracks'

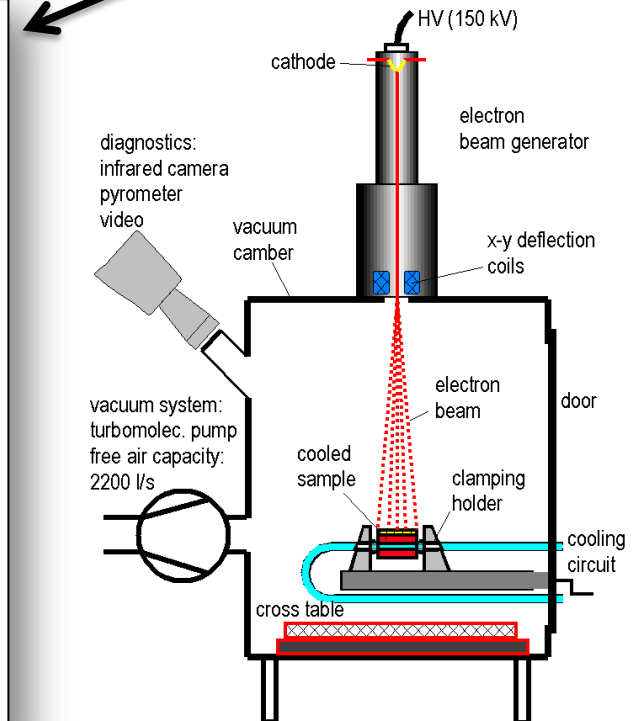
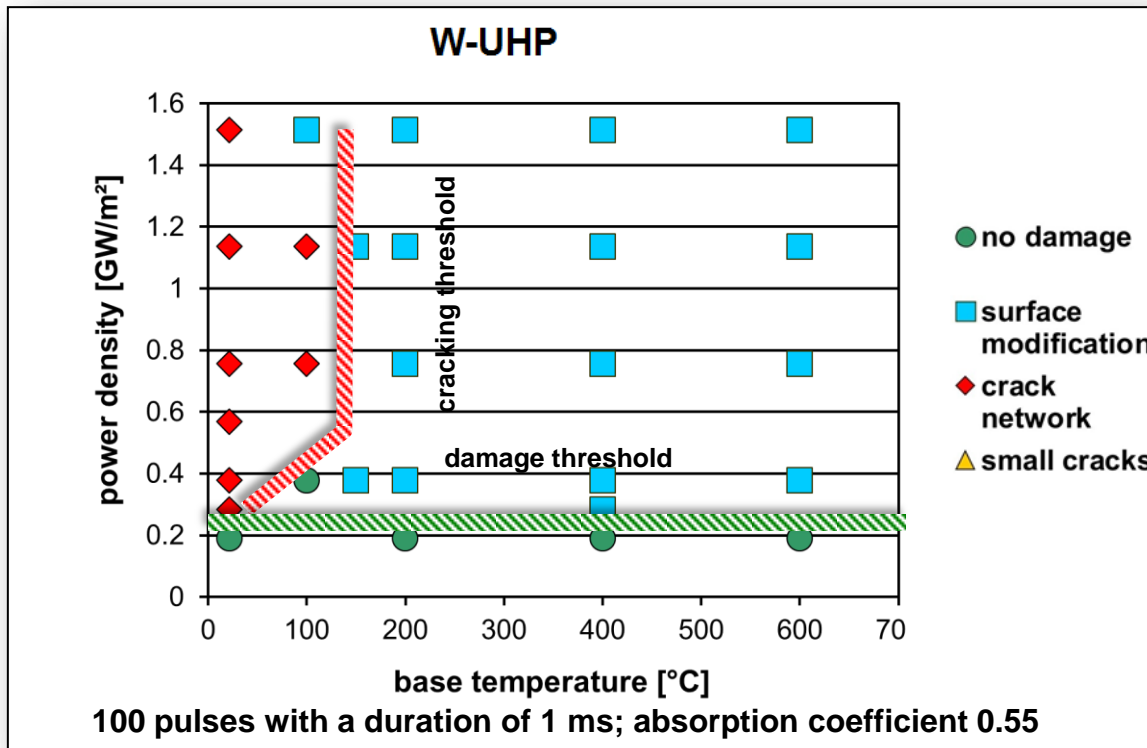
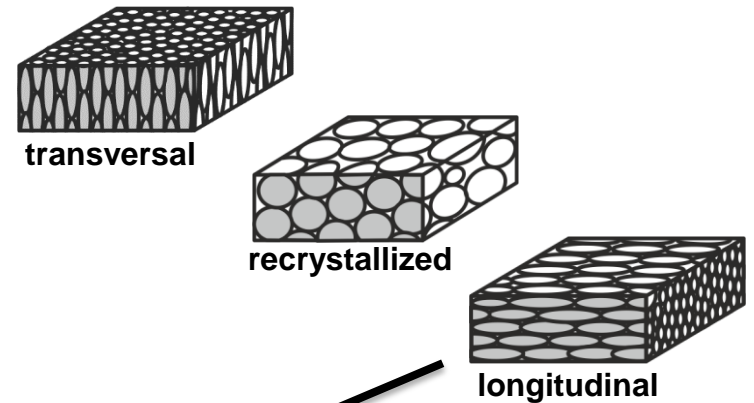
plasma stream



Thermal shock tests on tungsten

Experimental setting

- Sample size $12 \times 12 \times 5 \text{ mm}^3$
- Loaded area $4 \times 4 \text{ mm}^2$
- Base temperature: RT up to $1000 \text{ }^\circ\text{C}$
- Power densities: 0.19 to 1.51 GW/m^2

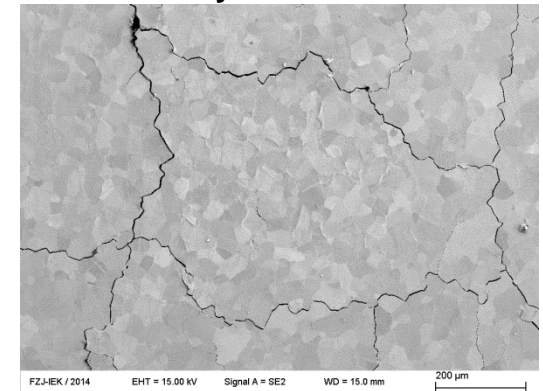
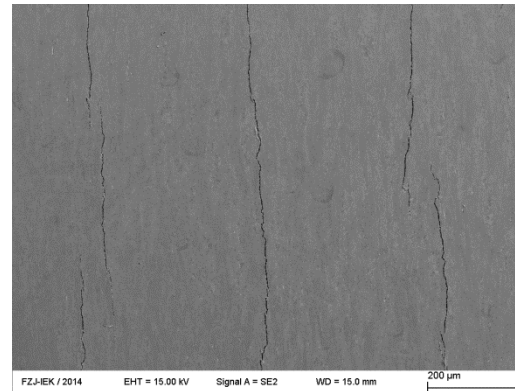
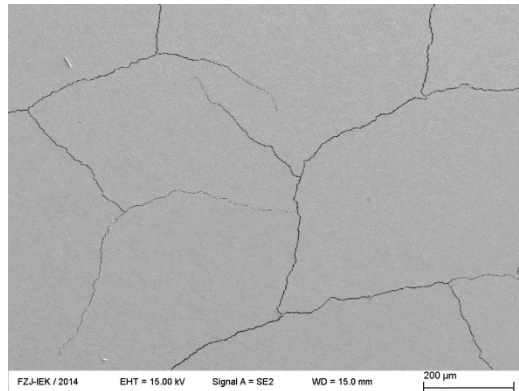


Crack Formation

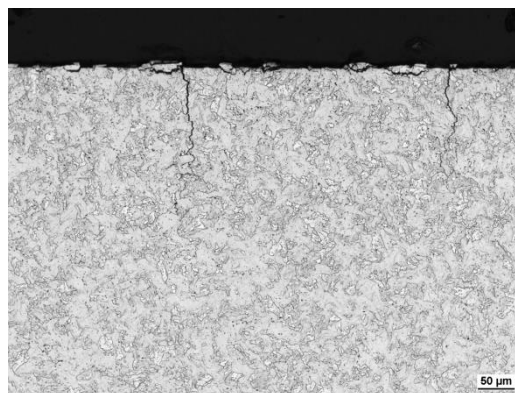
- Plansee pure tungsten according to ITER specifications (“IGP”)
- $L_{\text{abs}} = 0.38 \text{ GW/m}^2$ ($F_{\text{HF}} = 12 \text{ MW/m}^2\text{s}^{1/2}$), $T_{\text{base}} = \text{RT}$



loaded surface



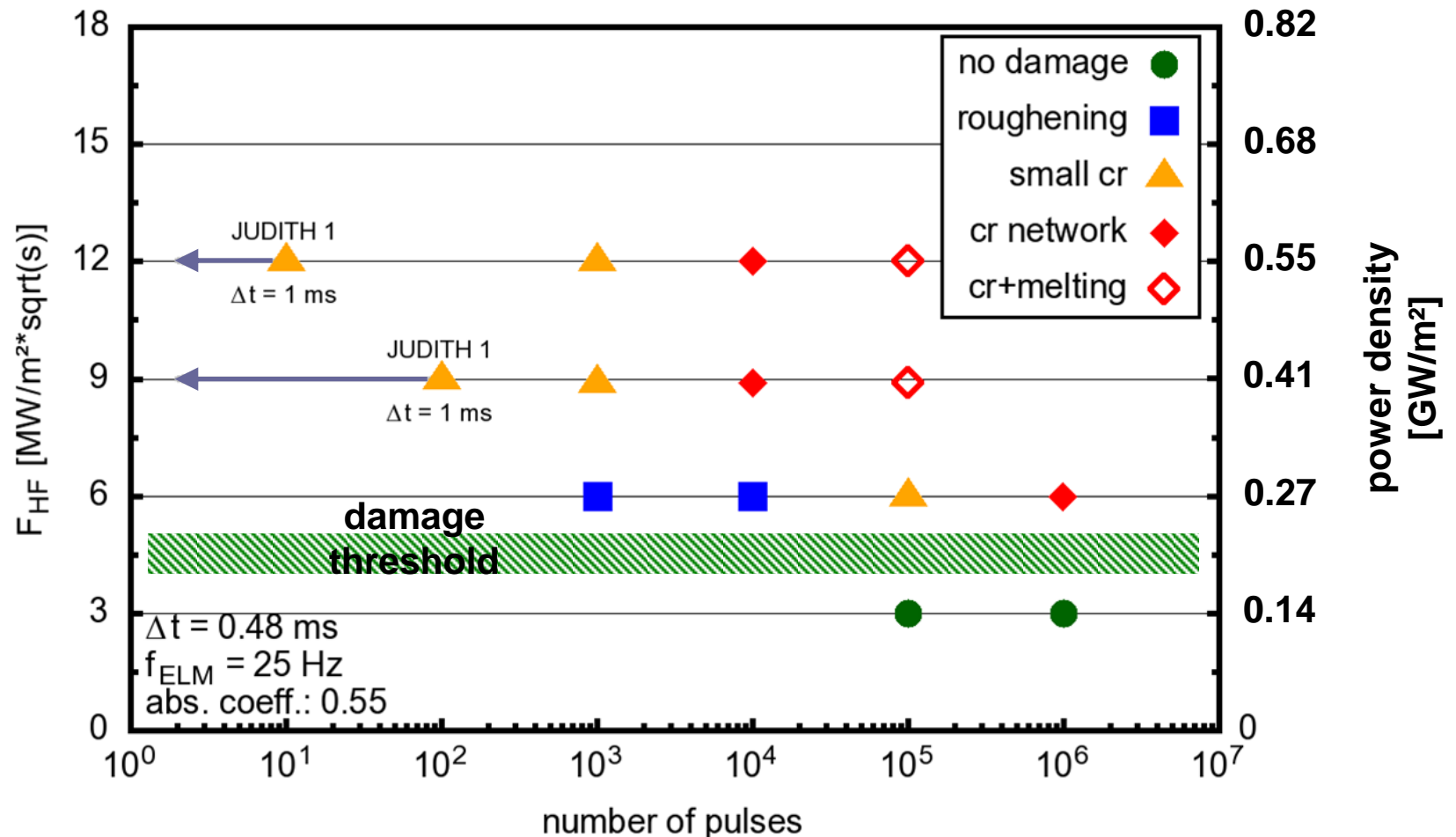
cross section



ELM simulation using e-beams with high repetition rates in JUDITH 2



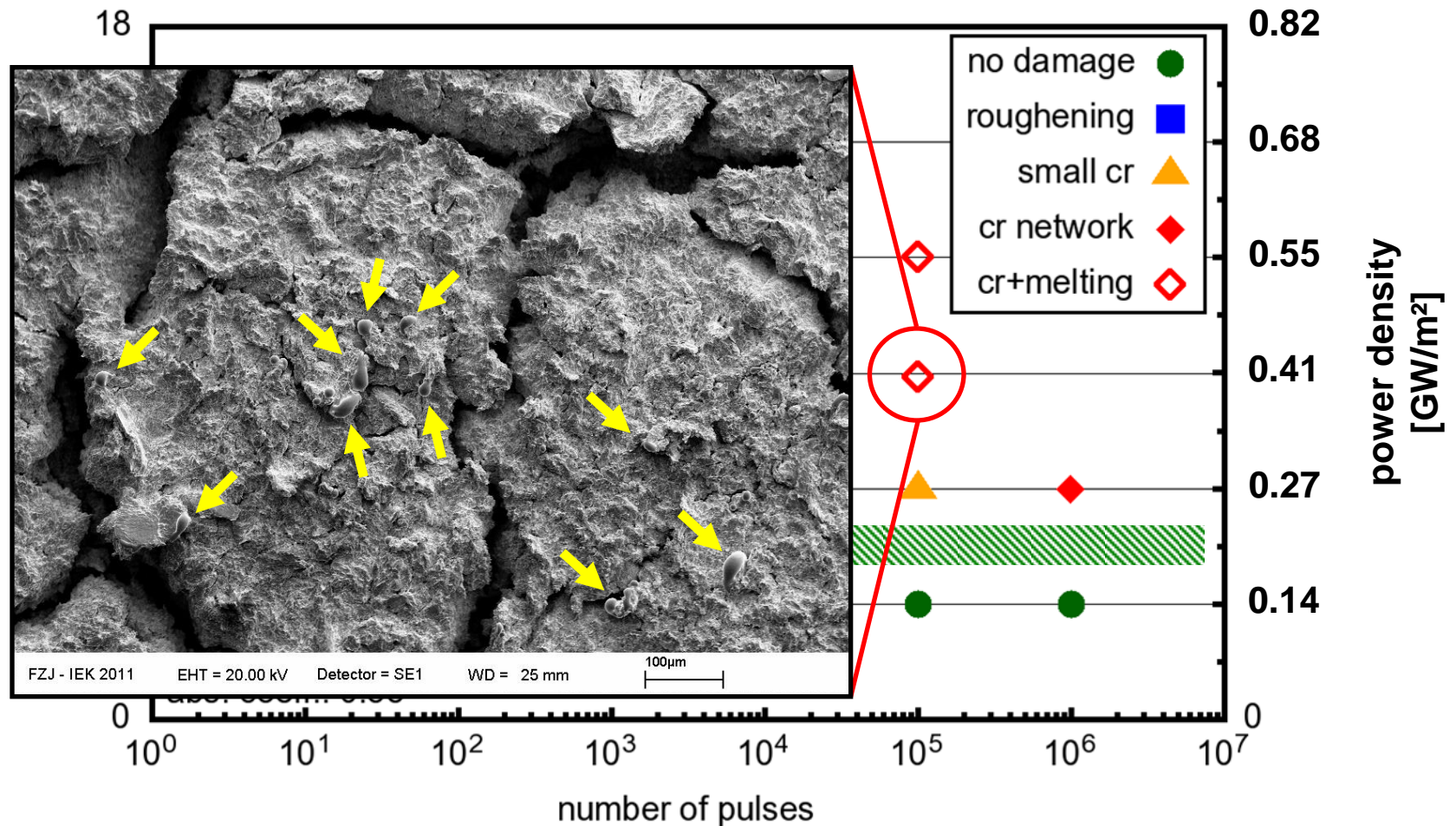
Surface condition after testing pure W at $T_{\text{surf}} \approx 700 \text{ °C}$ (10 MW/m^2 SSHL)



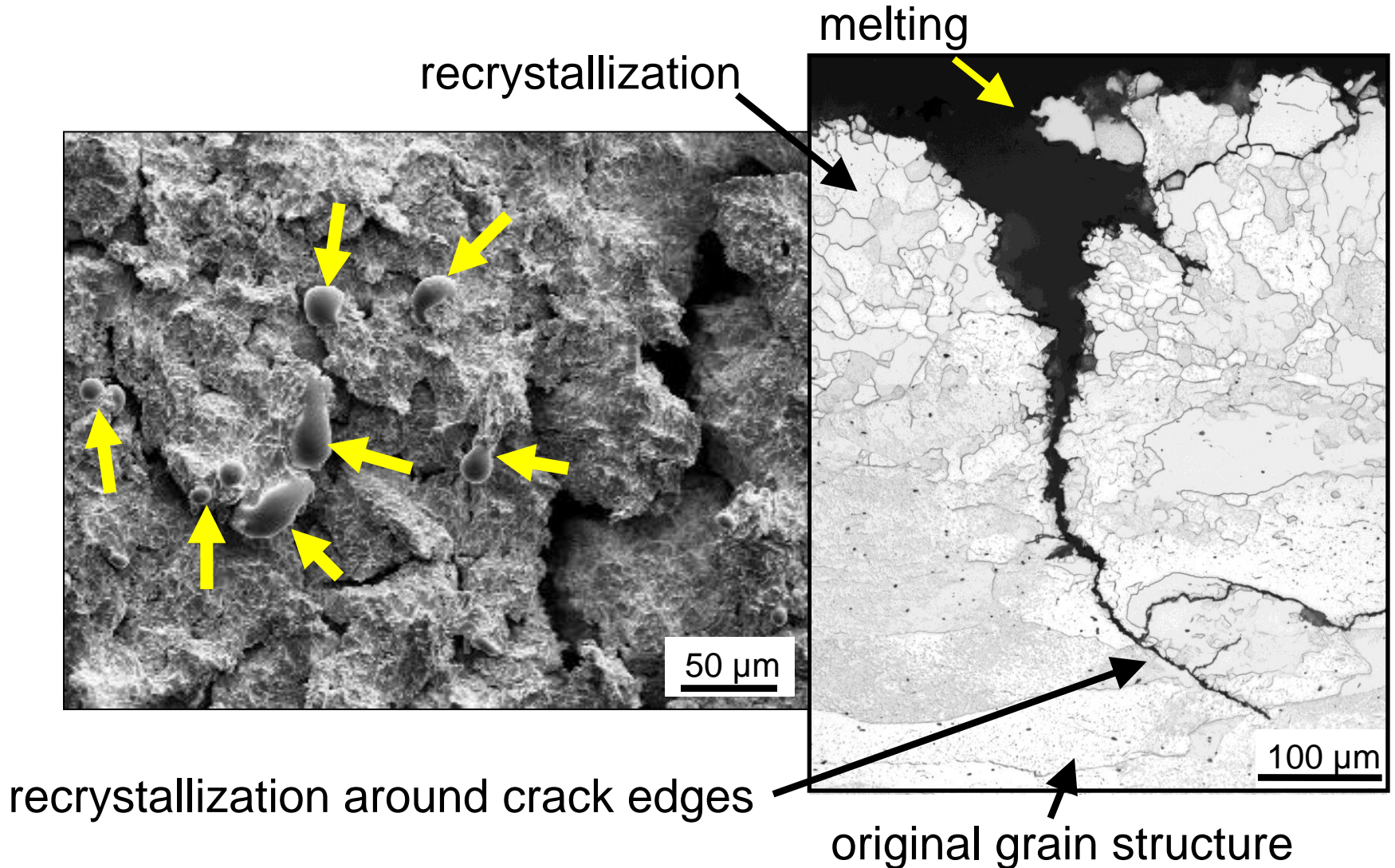
ELM simulation using e-beams with high repetition rates in JUDITH 2



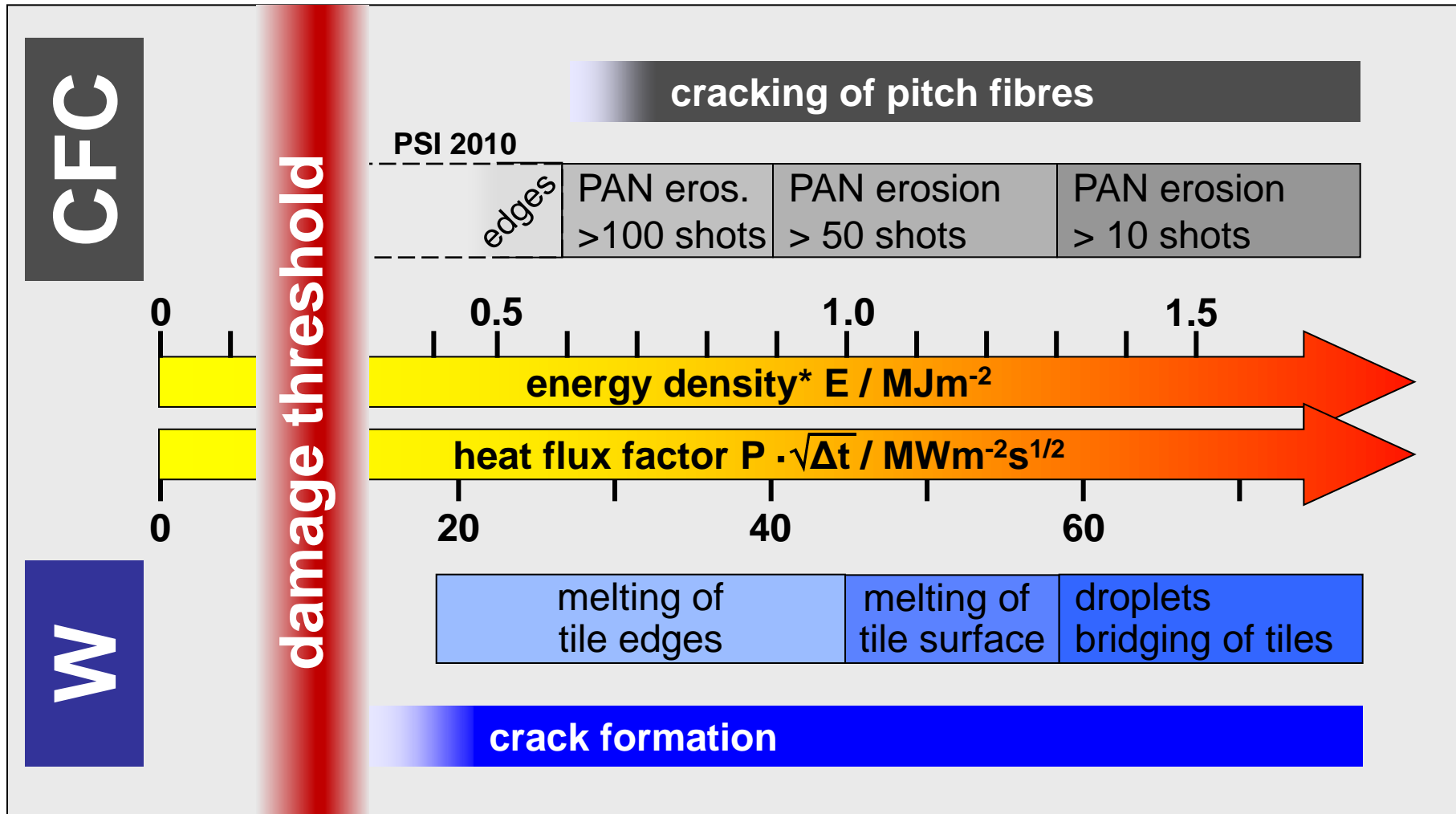
Surface condition after testing pure W at $T_{\text{surf}} \approx 700 \text{ °C}$ (10 MW/m^2 SSSL)



ELM simulation using e-beams with high repetition rates in JUDITH 2

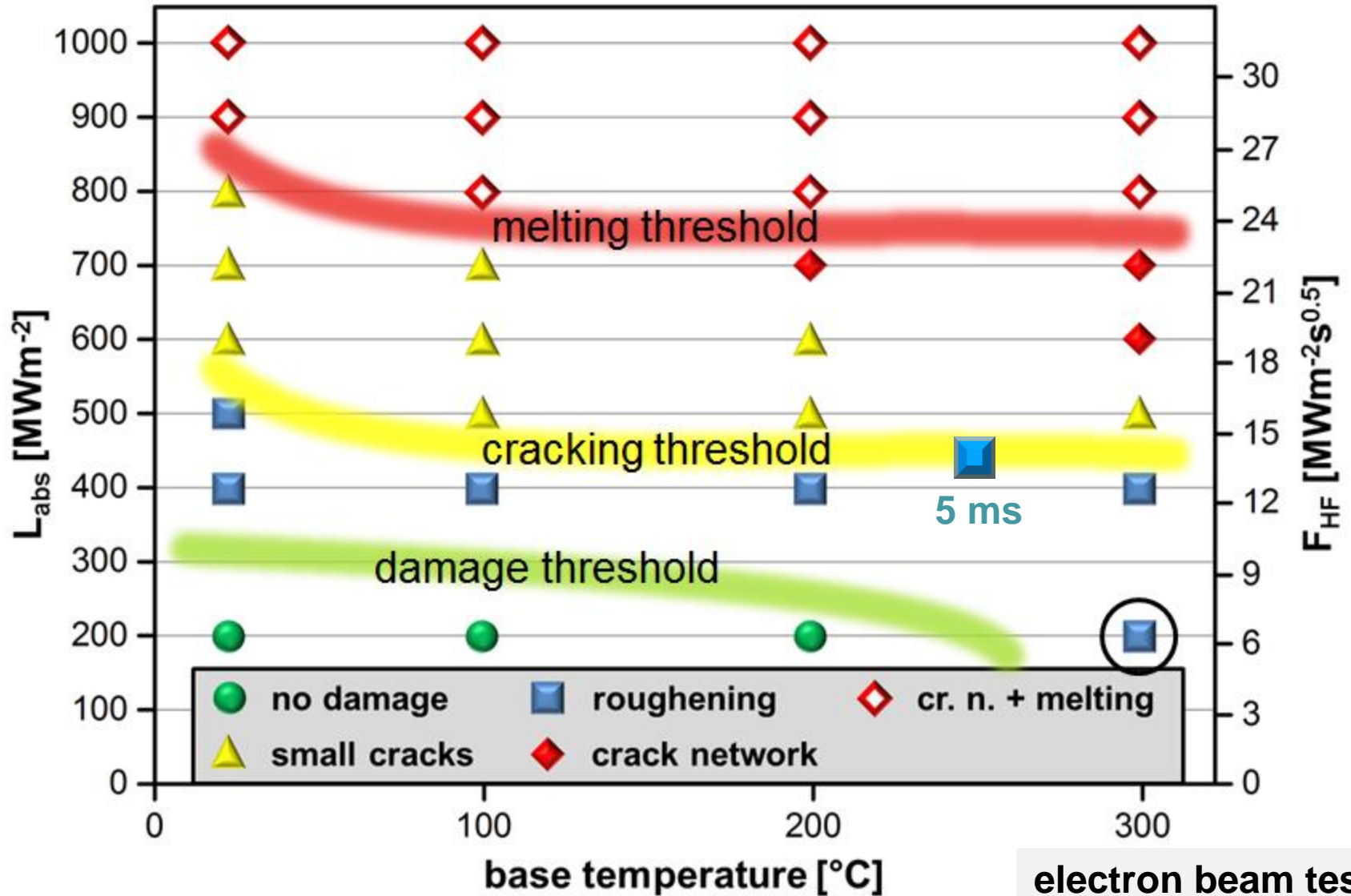


Threshold values for ELM loads



* $\Delta t = 500 \mu\text{s}$
 $T_0 = 500^\circ\text{C}$
 CFC: NB31
 W: forged rod material

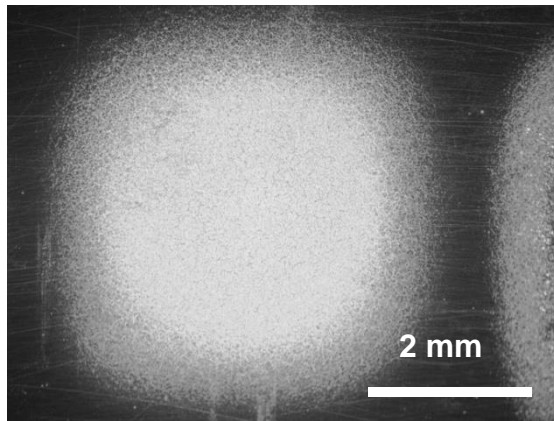
Thermal shock testing of beryllium



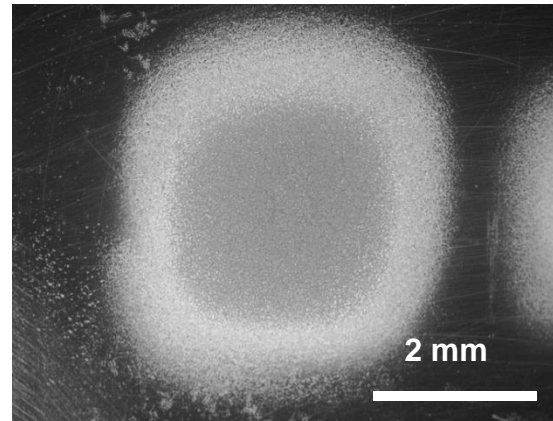
electron beam tests
with 100 cycles

Repeated thermal shock testing of Be

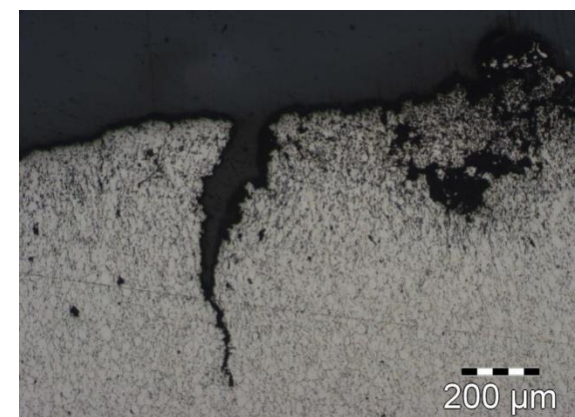
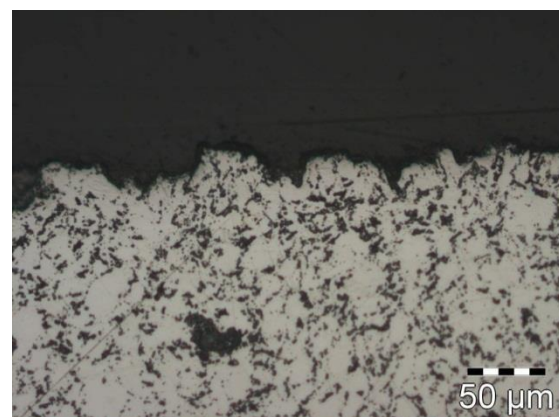
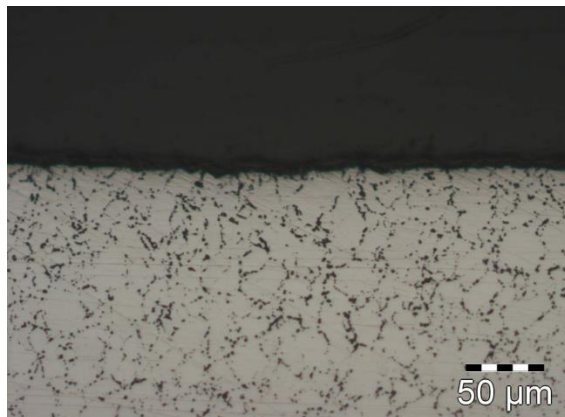
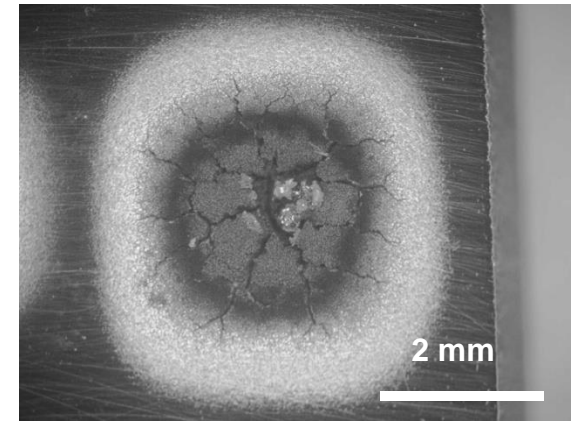
n = 100



n = 1000



n = 10000



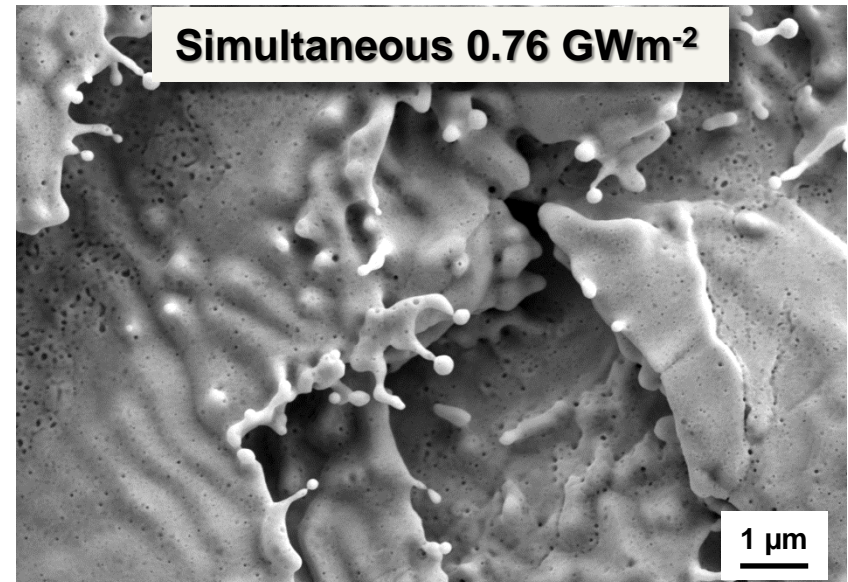
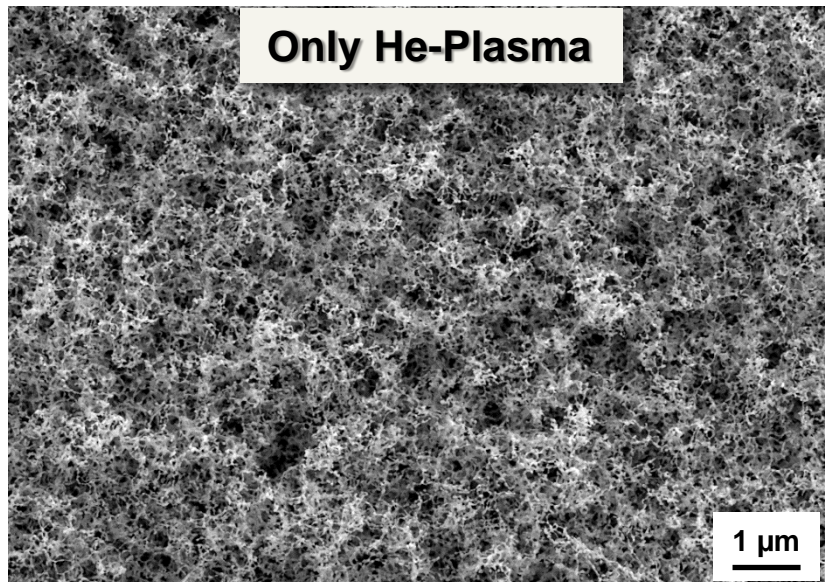
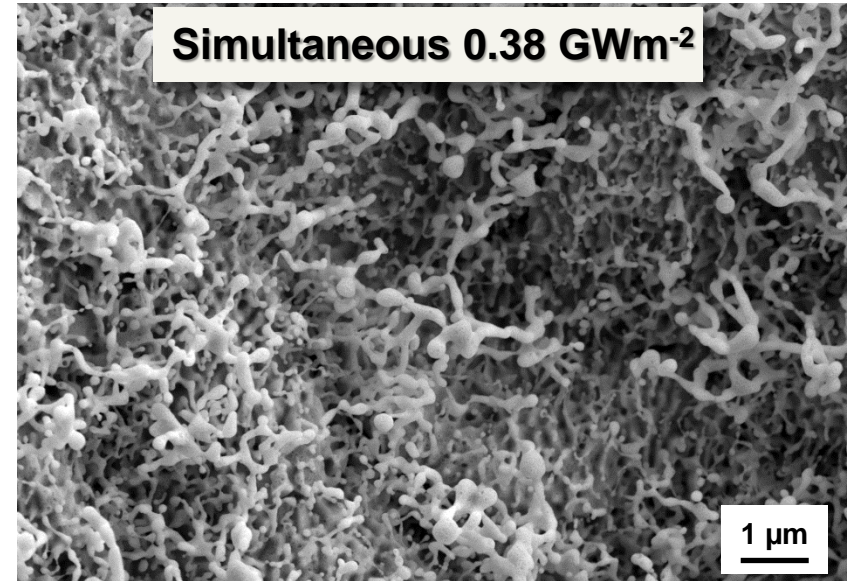
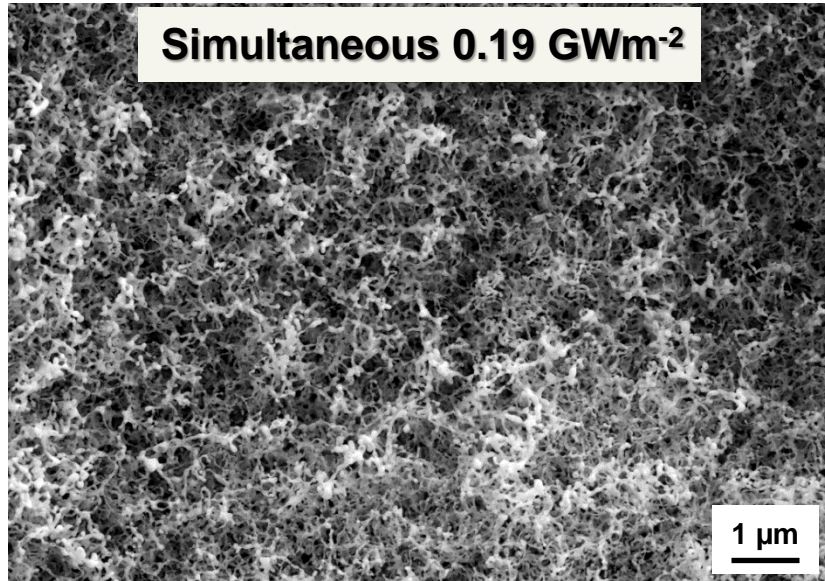
power density $P = 1.0 \text{ MJ/m}^2$
 $P \cdot \sqrt{\Delta t} = 14 \text{ MW/m}^2\text{s}^{1/2}$

pulse duration $\Delta t = 5 \text{ ms}$
base temperature $T_0 = 250^\circ\text{C}$

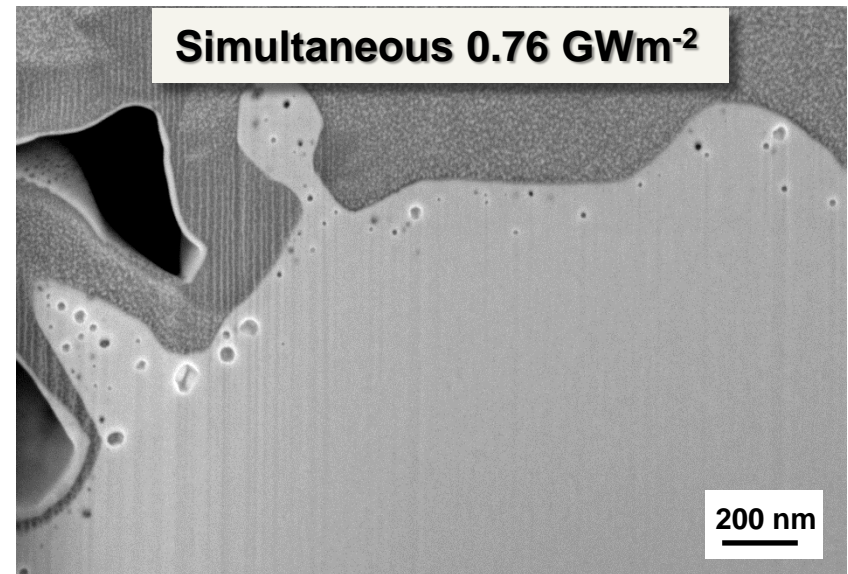
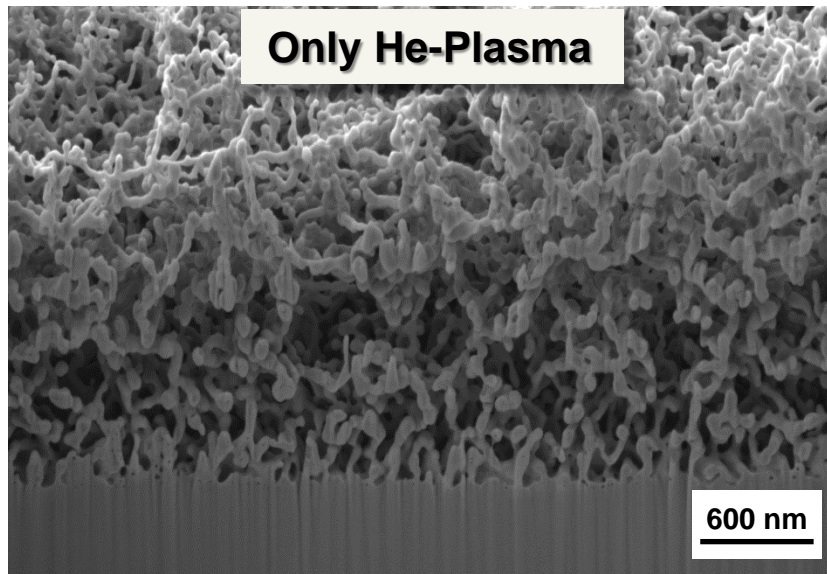
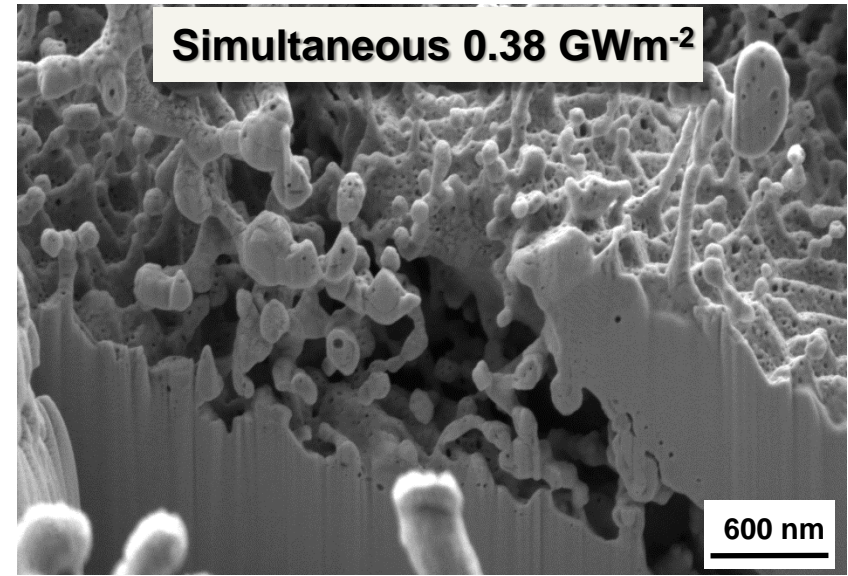
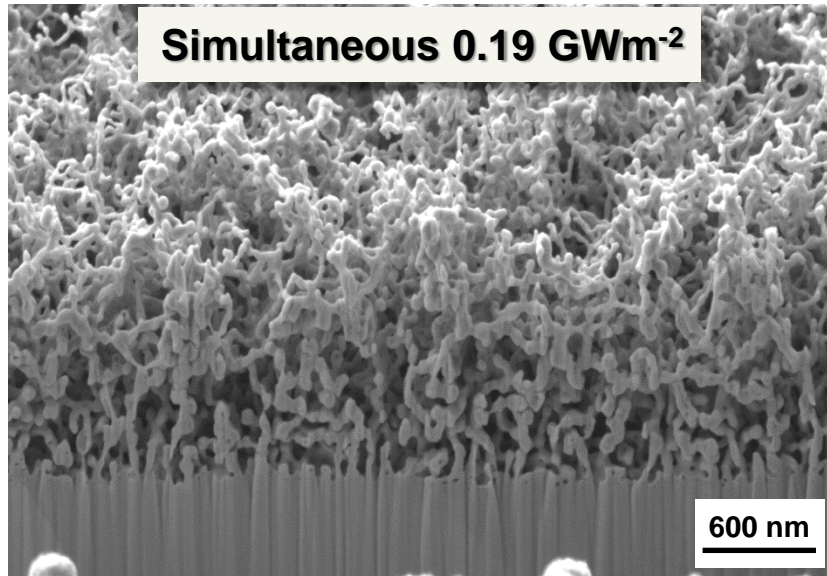
C

Hydrogen and helium effects

Thermal shock and He-loading



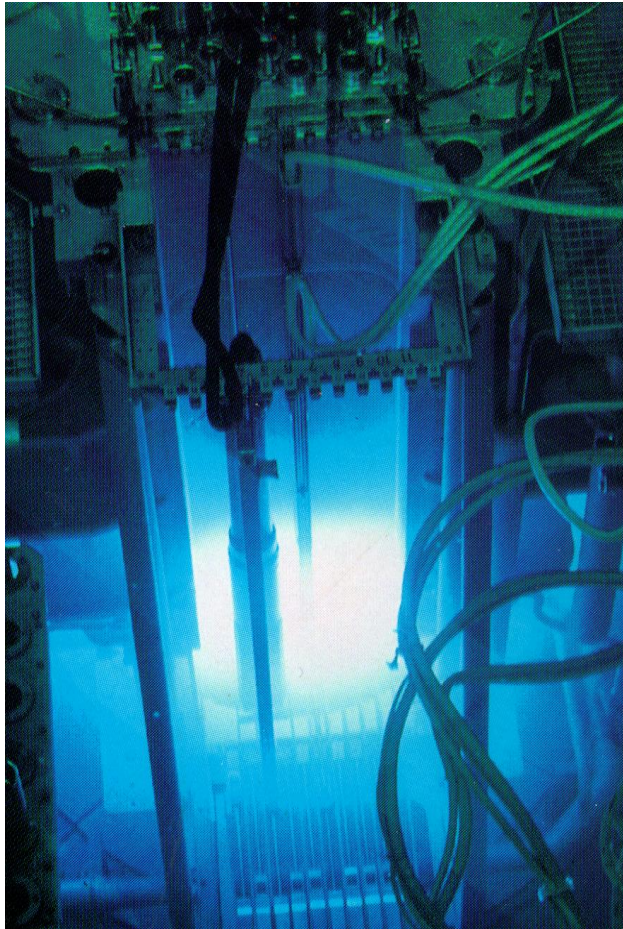
Thermal shock and He-loading



D

Materials degradation by energetic neutrons

Neutron-induced material degradation

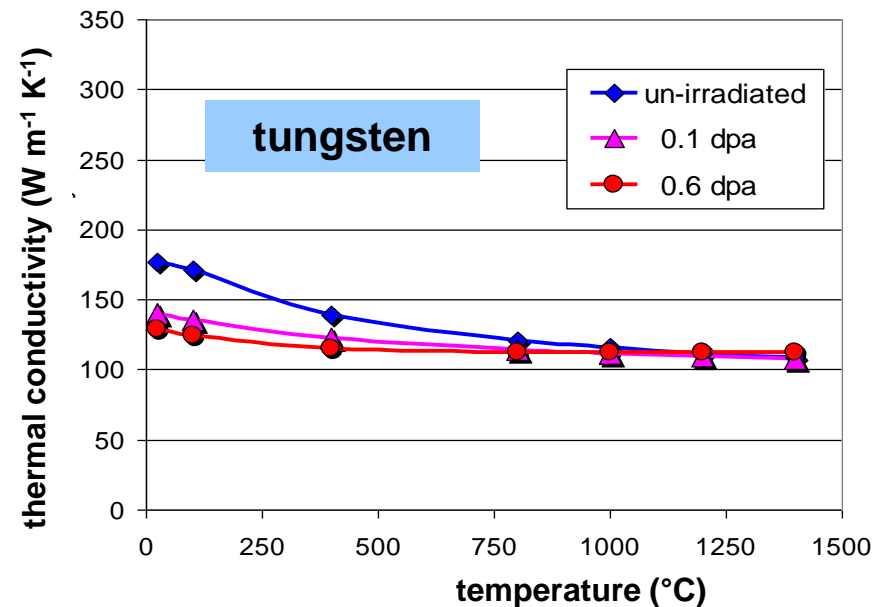
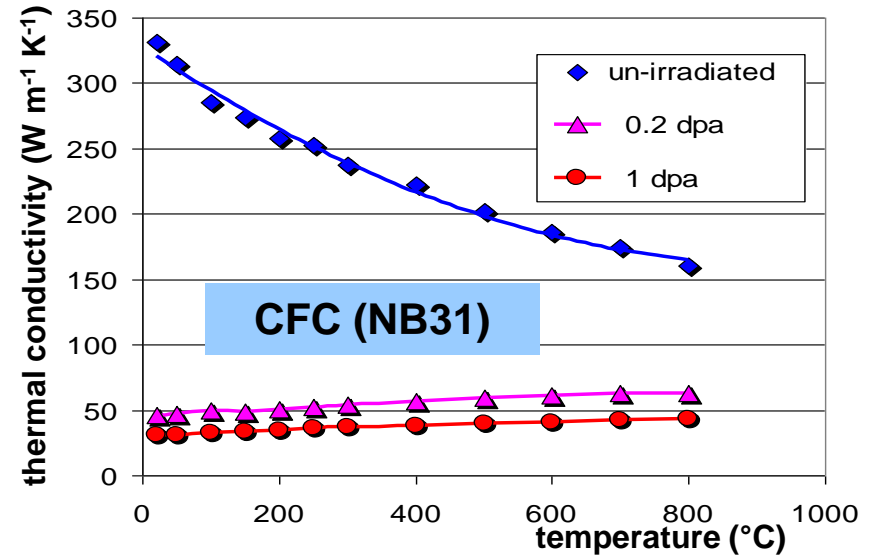
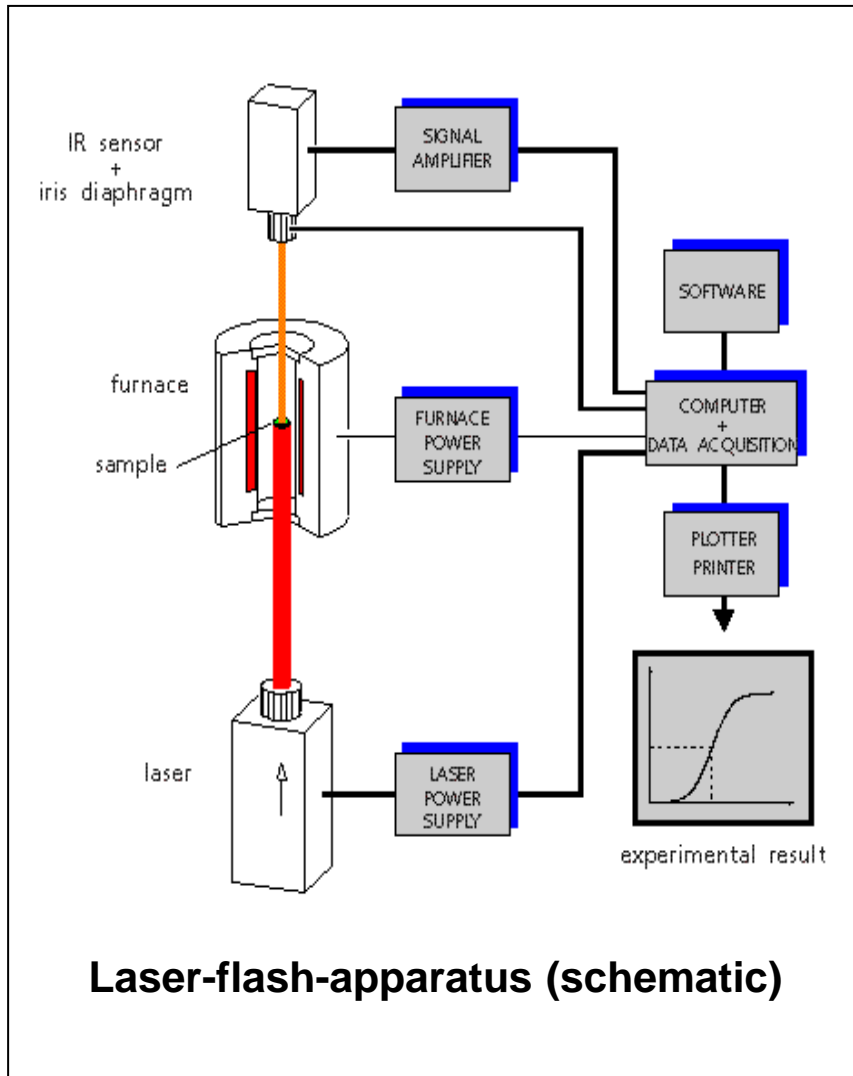


**High Flux Reactor (HFR)
Petten, The Netherlands**

Neutron induced effects:

- **activation** of plasma facing and structural materials
e.g. Co, Ag
- **transmutation** due to 14 MeV neutrons
 $W \rightarrow Re \rightarrow Os$
 $Be \rightarrow He, T$
- **degradation** of thermal and mechanical properties
*thermal conductivity,
hardening,
embrittlement*

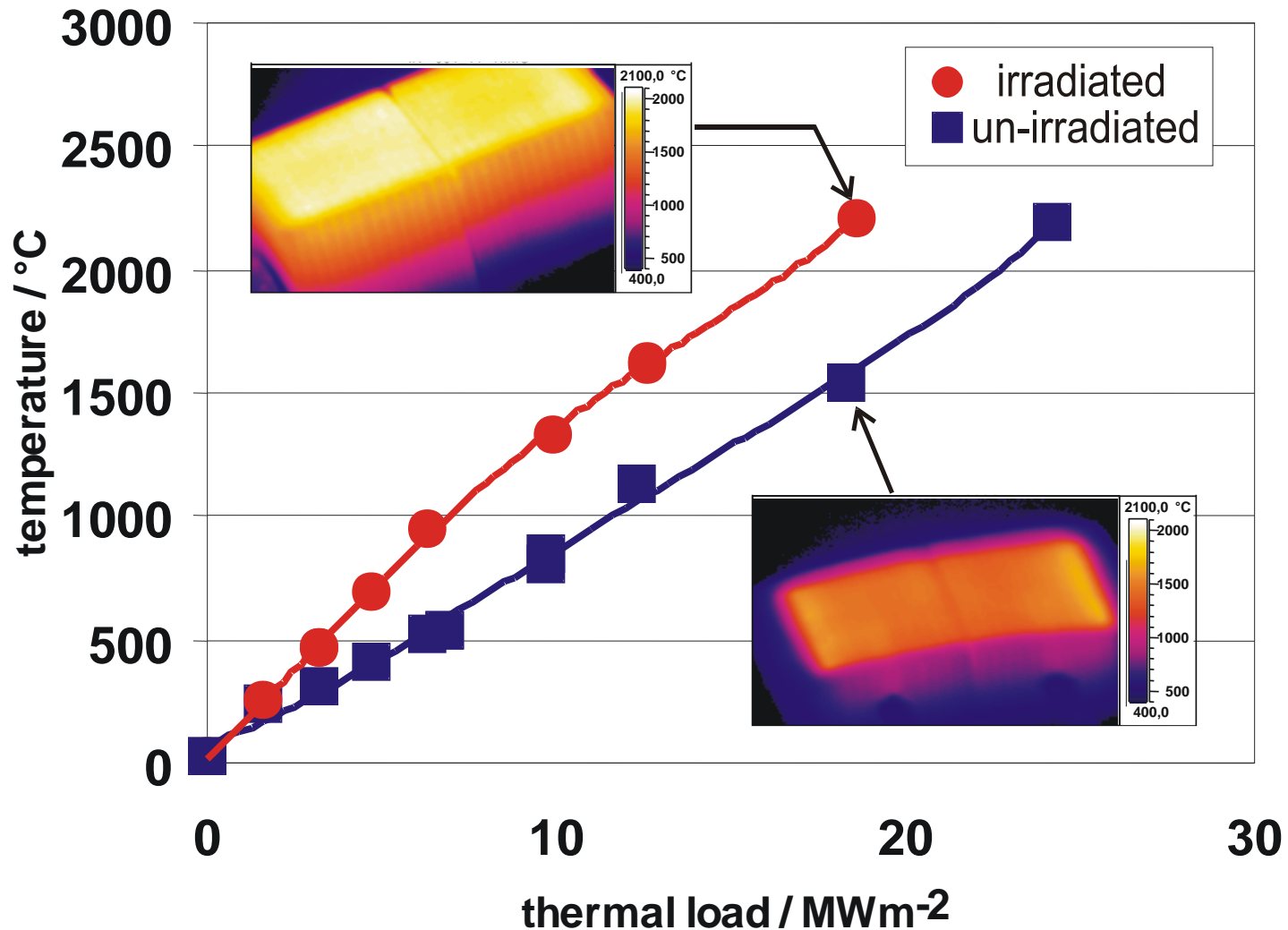
n-irradiation effect on thermal conductivity



HHF performance of neutron irradiated divertor modules

Dunlop Concept 1 (12 mm) / CuCrZr

$T_{\text{irr}} = 350^\circ\text{C} / 0.3 \text{ dpa}$



Future fusion materials research in



**very high
thermal
loads**

