

Brief Background on Volcanic Ash Oxford

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Starting Point NEWAC

- Build a simple test rig to heat coolant to 650°C
 - Use cutaway of turbine blade to provide sample for testing
 - Use blowtorch to obtain reasonable external boundary conditions
 - Showed that internal deposition is possible in cooling holes
 - Icelandic ash reground from Cranfield sample used.
- Match velocities but not pressures



General Set-Up

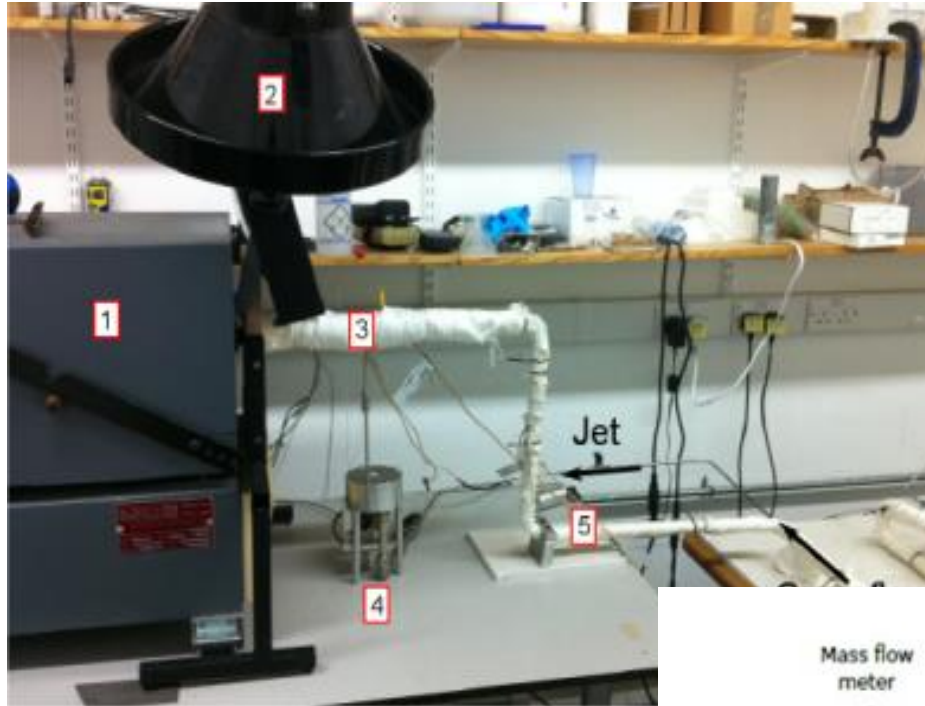


Fig 3.4 – rig in operation [11].

Key:

1 = Electric furnace

2 = Extractor

3 = Mixing chamber

4 = Continuous Delivery System (CDS)

5 = Heater tape

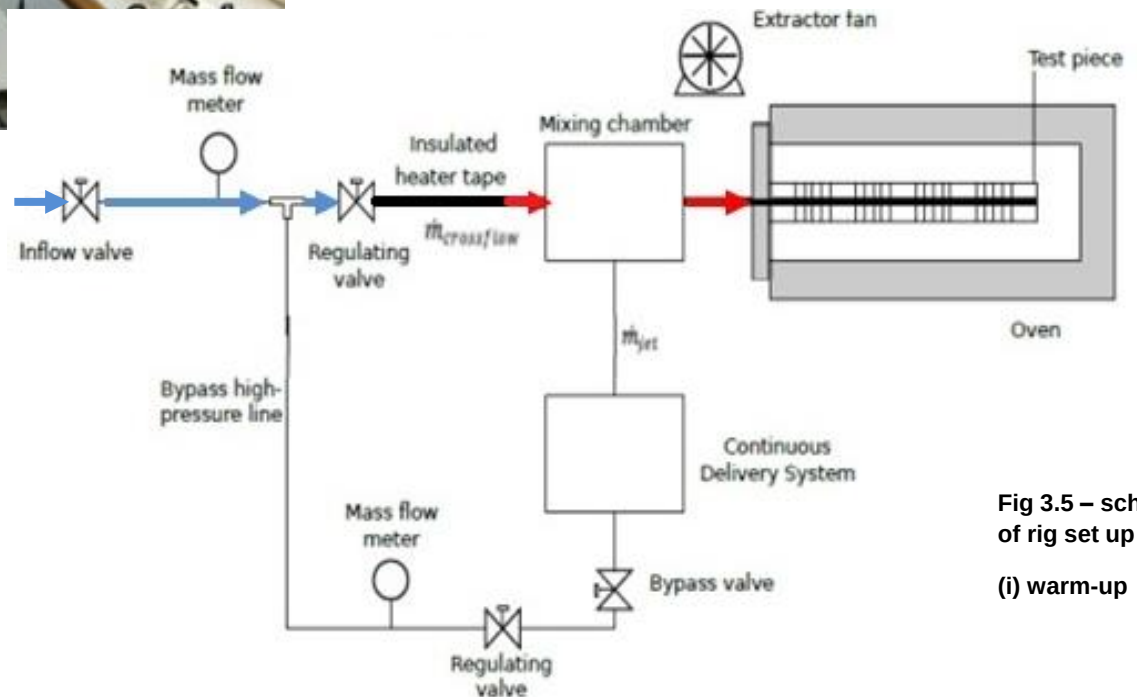
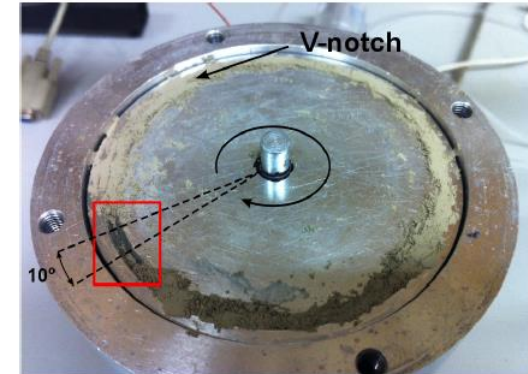


Fig 3.5 – schematic of rig set up for:

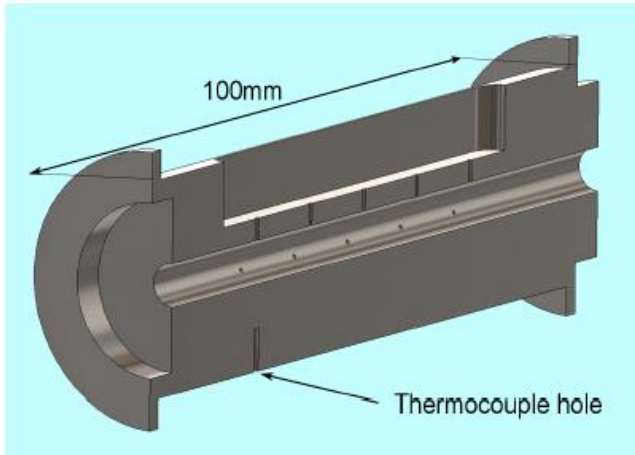
(i) warm-up

Experimental Improvements

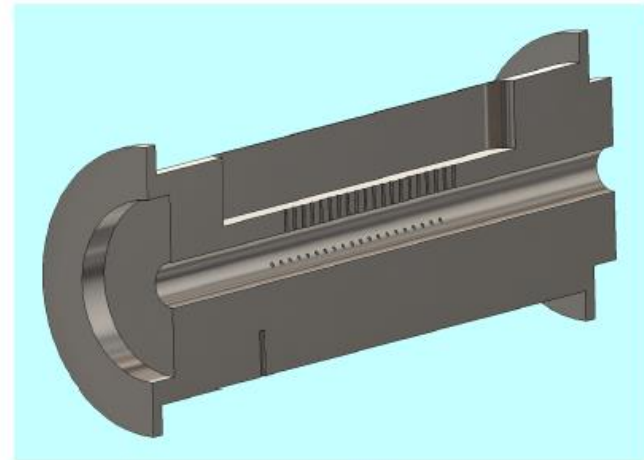
- Improved particle delivery system
 - Rotating ash snorter with mixing chamber
- Preheat of sample in oven up to 900 - 1200°C
- Currently no funded programme
- 4 x 4YP students, Sam Hussain, James Parry-Crooke, Alex Bucknell and Seb Wylie



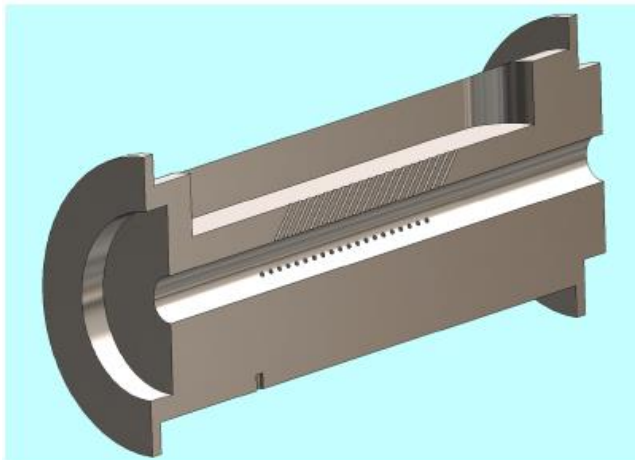
Improved Trial Test Pieces



(a) Low hole-density, 90° to flow (LD90, 1 of 4 pieces)



(b) High hole-density, 90° to flow (HD90)



(c) High hole-density, 45° or 135° to flow (HD45 or HD135)

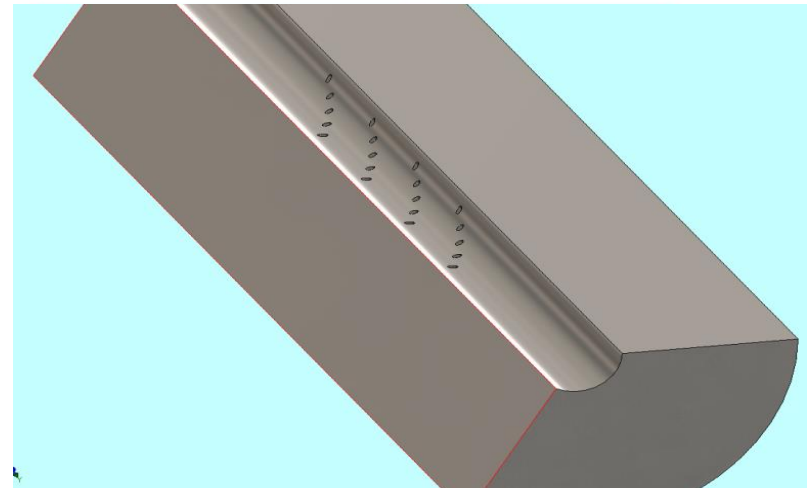


Fig 3.2 – Isometric view of a 120° section of HD90-S, showing the central channel interior. Used in meshing and analysis

Flow parameter measurements

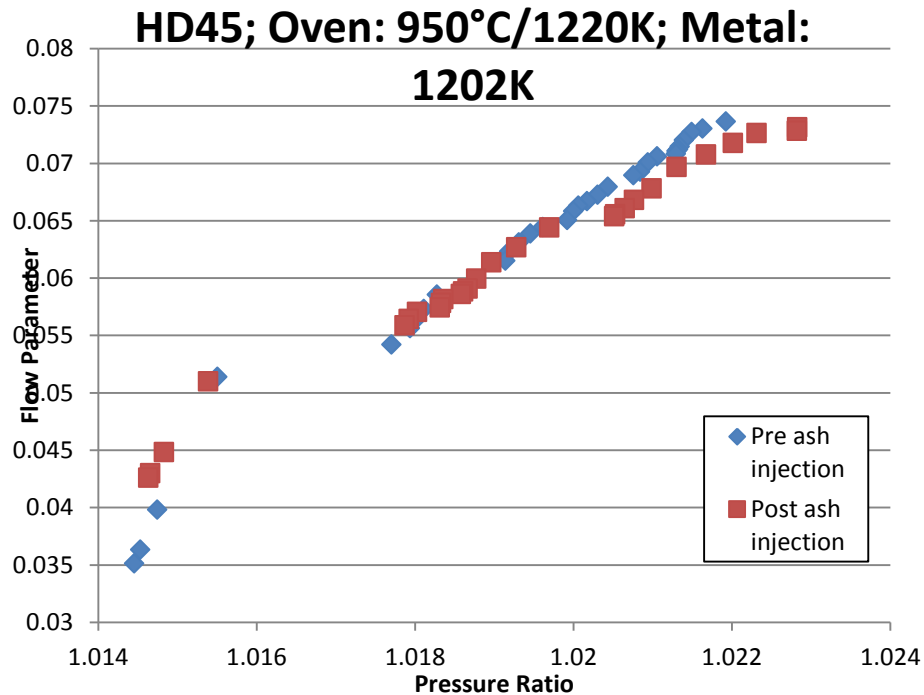


Fig. 6.2 – FP plotted against test section pressure ratio at 950°C, HD45

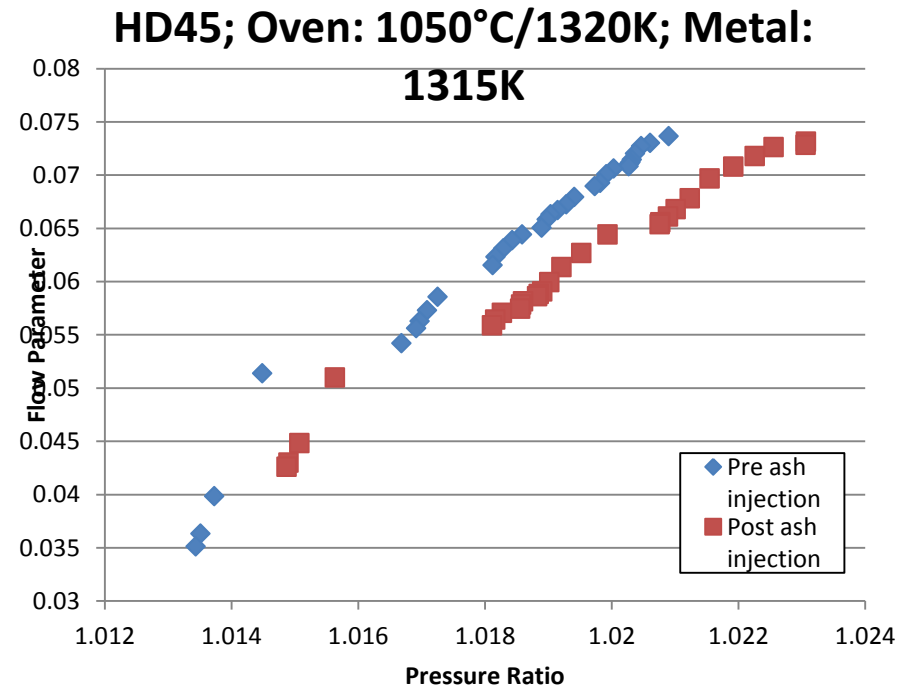


Fig. 6.3 – FP plotted against test section pressure ratio at 1050°C, HD45



Fig. 6.6 – Deposition in first four cooling holes of HD45, 1050°C

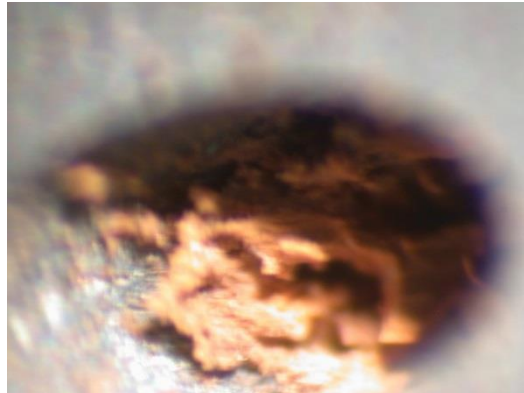


Fig. 6.7 – Blocked cooling hole in HD45, 1050°C

$$FP = \frac{\dot{m}_{coolant} \sqrt{T_{coolant} R}}{P_{coolant} d^2}$$

Comparison of reduction in Flow parameter

Mean RFP as a Function of Hole Inclination and Temperature

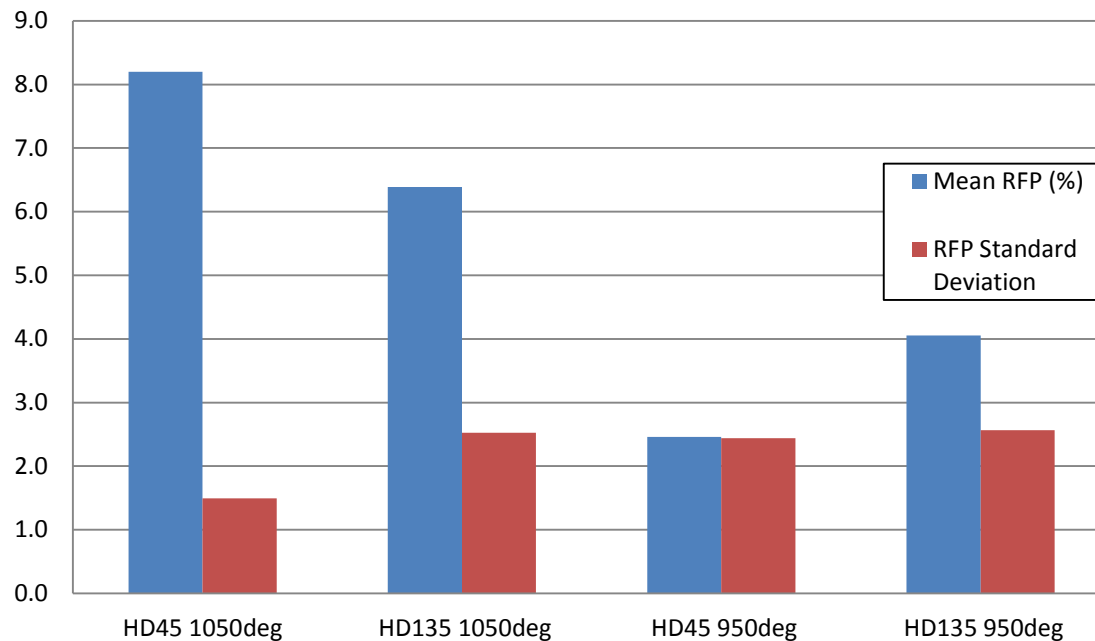
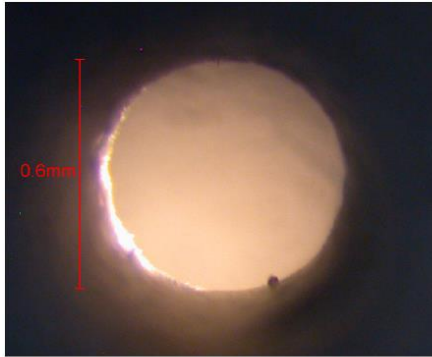
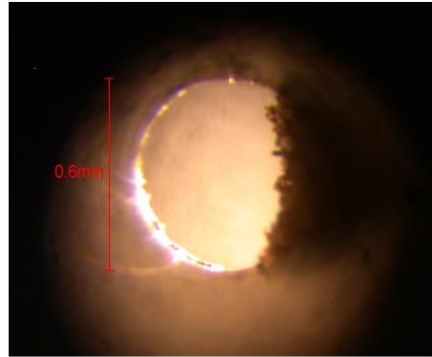


Figure 6.11 – Mean RFP for HD45 and HD135 at 950 and 1050°C

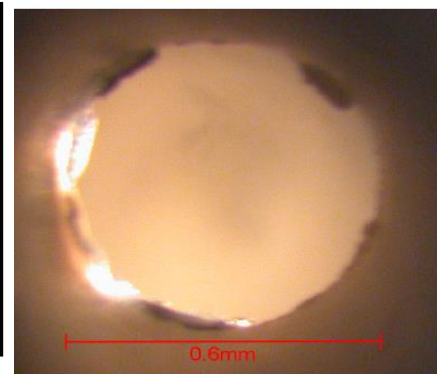
Qualitative Data on deposition



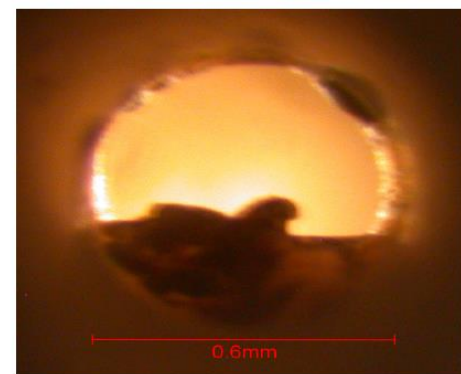
(a) Blockage-free cooling hole in LD90, $T_{metal} = 1100K$



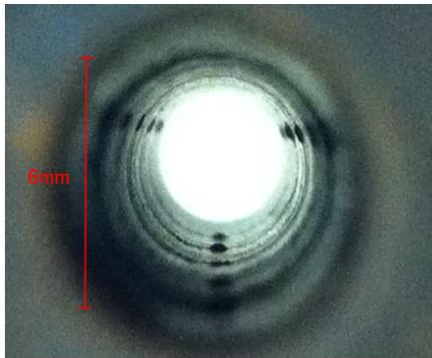
(b) Partially-blocked cooling hole in LD90, $T_{metal} = 1100K$



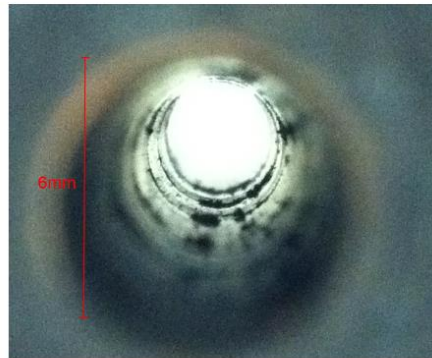
(a) Blockage-free cooling hole, $T_{metal} = 1100K$



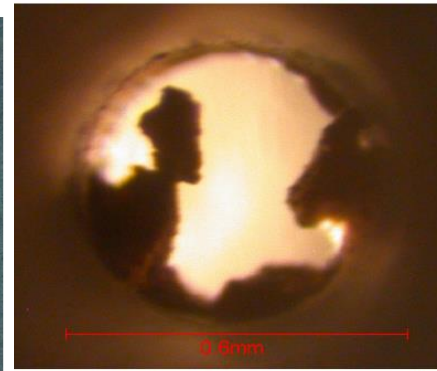
(b) Partially-blocked cooling hole, $T_{metal} = 1200K$



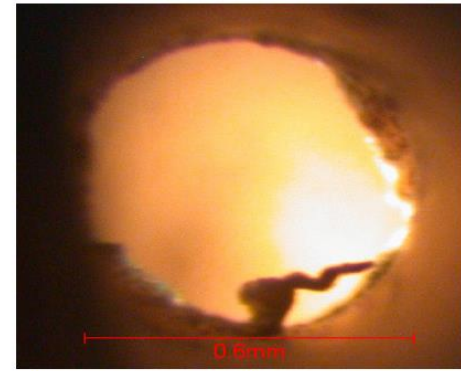
(c) Bulb-like deposits, LD90 main passage, $T_{metal} = 1200K$



(d) Pronounced deposits, LD90 main passage, $T_{metal} = 1300K$



(c) Intricate deposition in a cooling hole, $T_{metal} = 1200K$



(d) Typical cooling hole deposition pattern, $T_{metal} = 1300K$

Cooling Passage

Cooling Hole

CFD Modelling in Fluent

- Conjugate CFD for walls and flow with particle size injection from a uniform entrance plane.

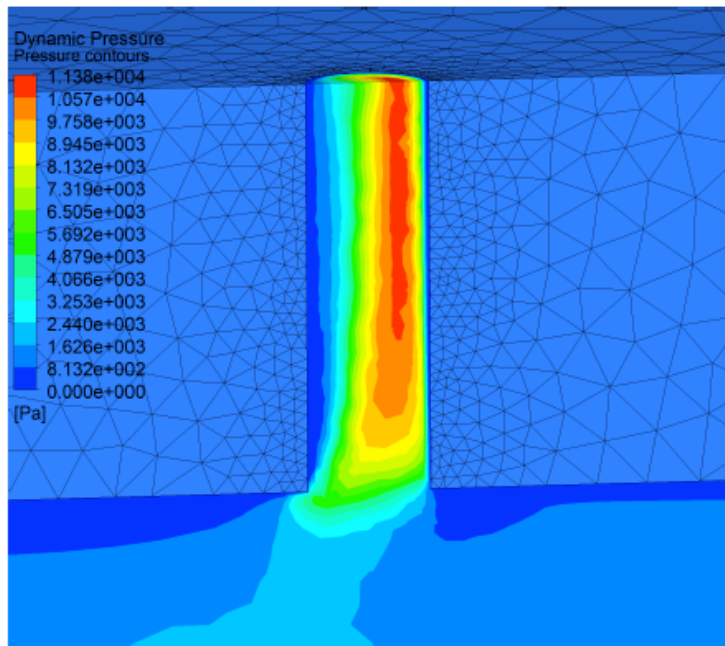


Figure 4.11: Dynamic pressure contours inside a cooling hole in LD90. Flow direction is left to right.

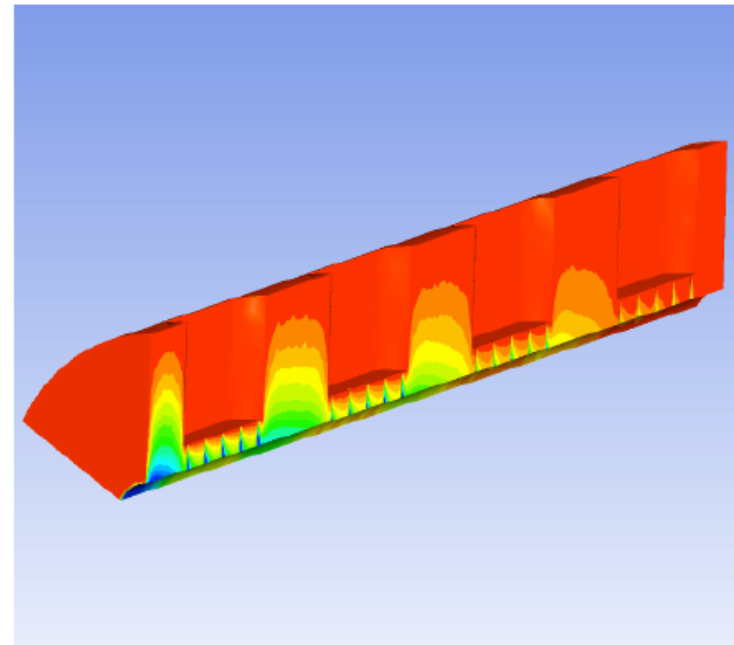
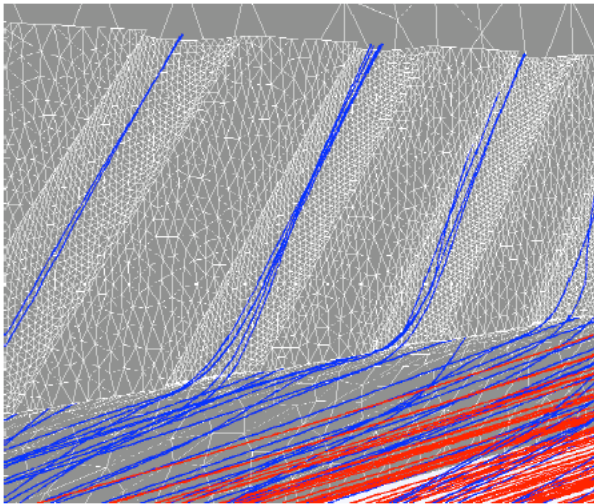
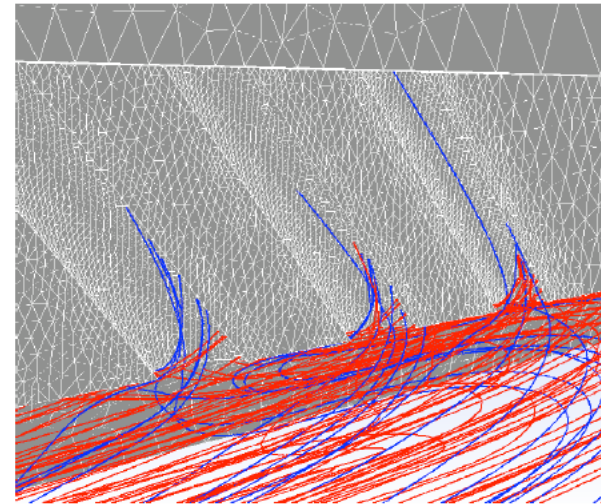


Figure 4.12: LD90 wall temperatures. Outer wall maintained at 1200K, inner wall cooling up to 15K. Flow direction is left to right.

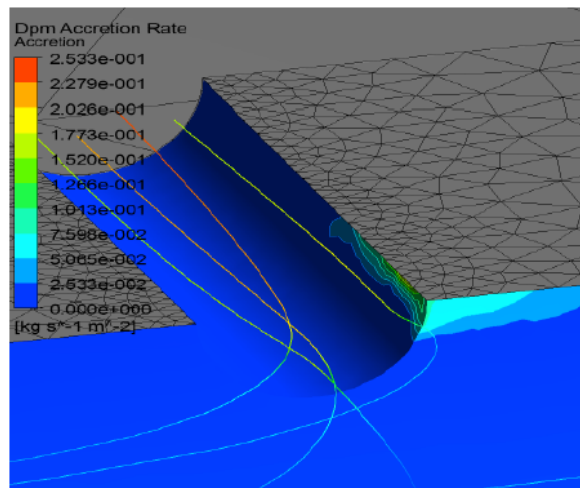
Particle 'capture' using Fluent in-built models & Lagrangian tracking



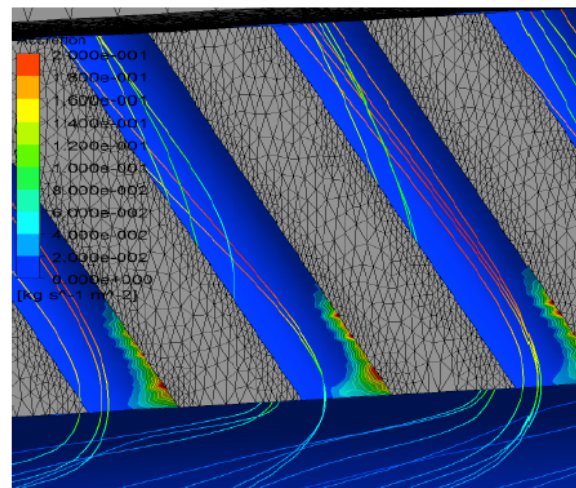
(a) 3µm (blue) and 15µm (red) particles in HD45, holes 9-12



(b) 3µm (blue) and 15µm (red) particles in HD135, holes 18-20



(a) Accretion pattern around LD90 cooling hole 10



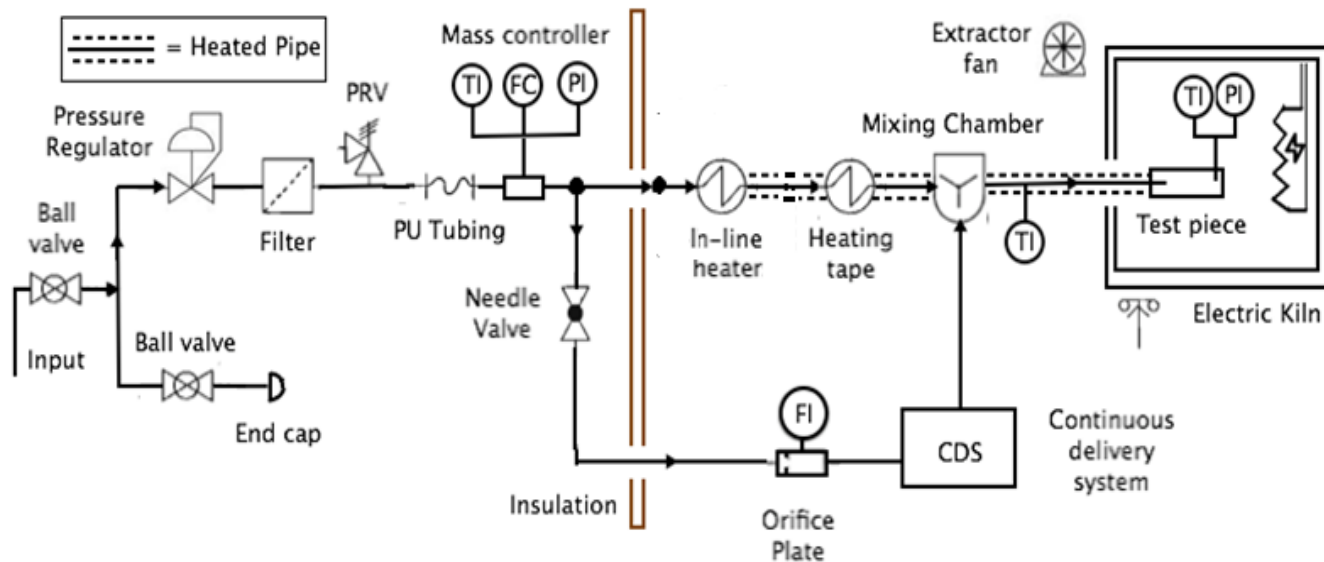
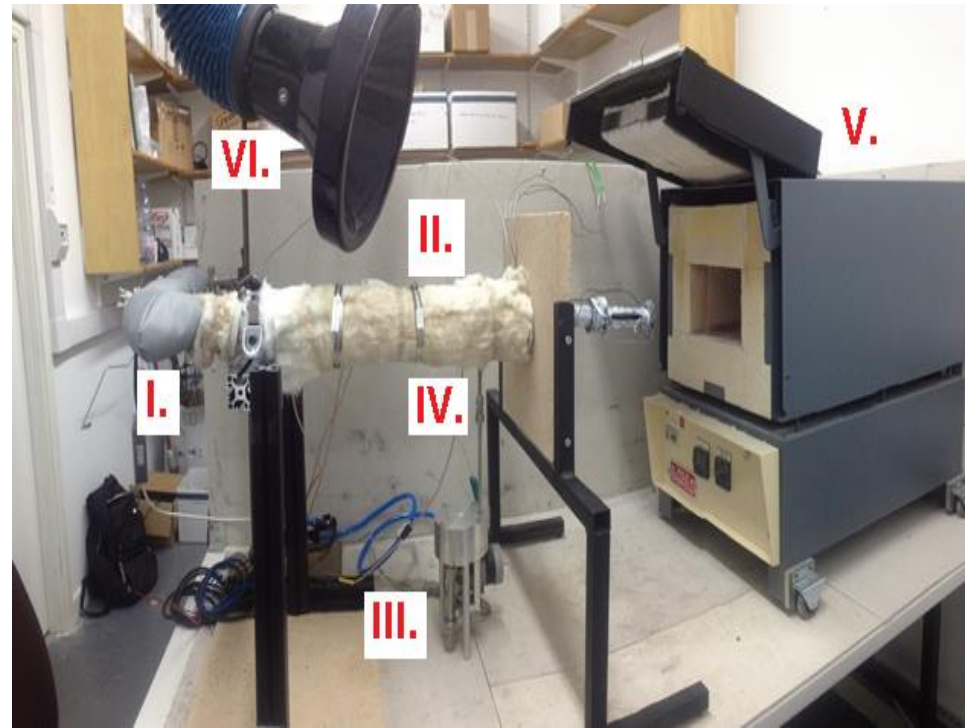
(b) Accretive effects deep inside HD135 cooling holes 9-11

Current Work – Seb Wylie

- Rebuild test rig to allow better operating conditions
- Better control on mass flow rate with no variation when dust delivery employed
- Focus on high density cooling holes
- Better definition of volcanic ash particle sizes and distribution
- Better control of temperature of solid test pieces
- Rerun baseline CFD
- Collaborating with Loughboro on particle stick slip model
- Working with different ash sources to determine similarities and differences.

Experimental Setup

- I = In-line heater
- II = Electric heater tape and insulation
- III = CDS
- IV = Mixing chamber
- V = Furnace
- VI = Extractor fan.

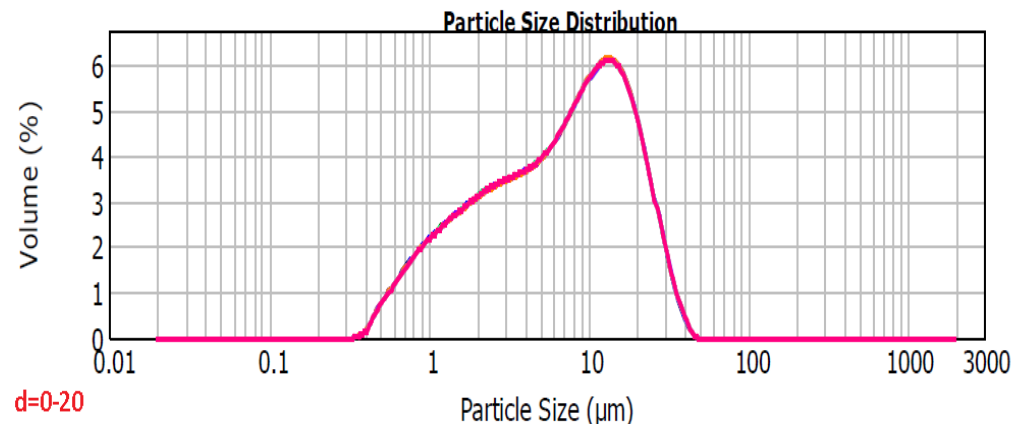
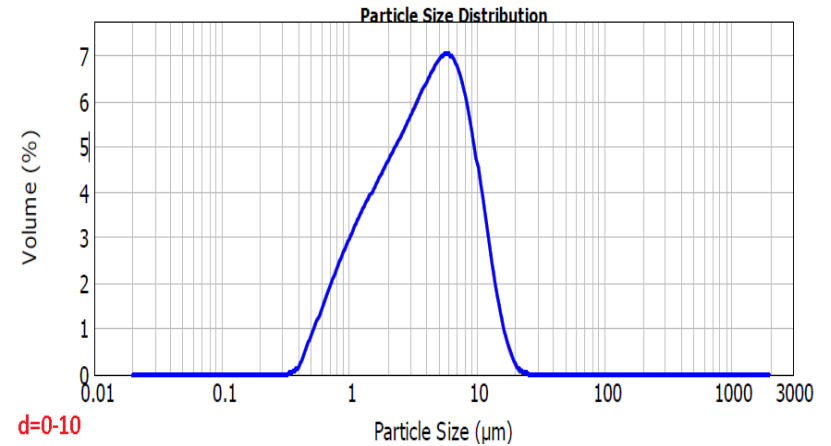


Particle Characterization – Size distribution

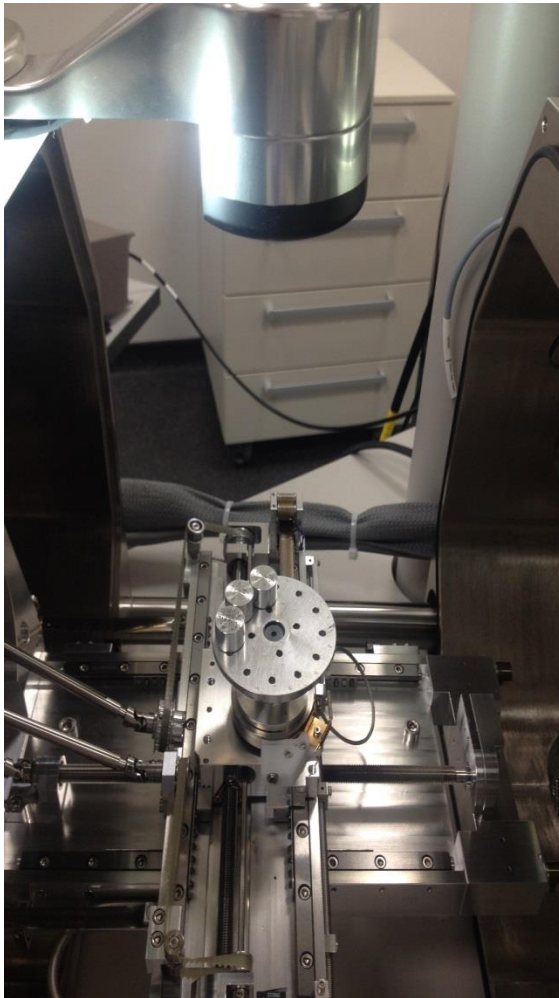


Particle Diameter Bands:

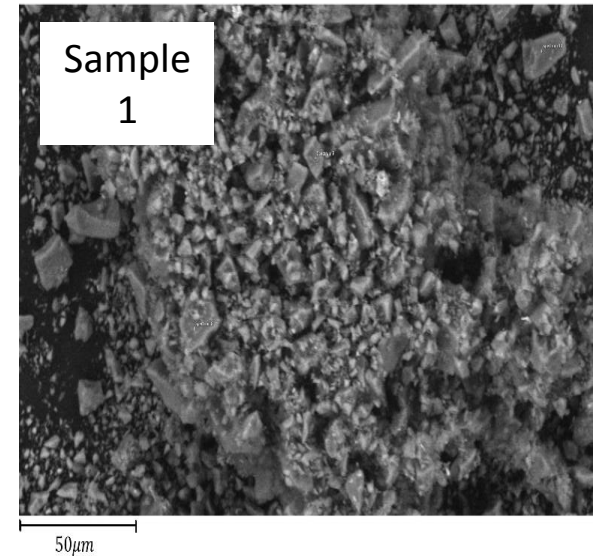
1. $0-10\mu m$
2. $10-20\mu m$
3. $0-20\mu m$
4. $20-38\mu m$
5. $38-100\mu m$



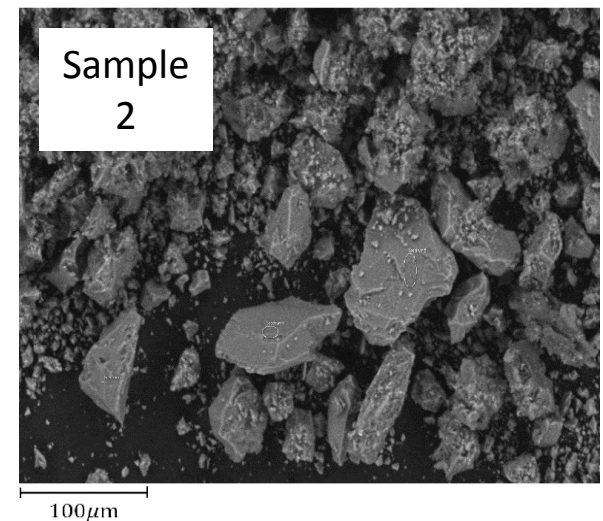
Particle Characterization - SEM



Sample 1: $d = 0\text{-}20\mu m$



Sample 2: $d = 38\text{-}100\mu m$



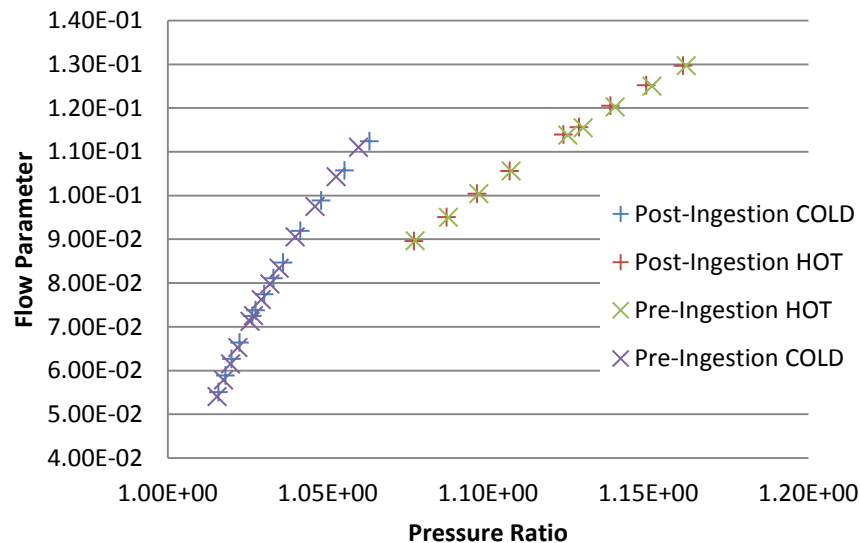
Variation in Metal Temperature

$$T_c = 627^{\circ}\text{C}$$

Below ATT

Volcanic Ash Ingestion

Conditions: $T_m = 936^{\circ}\text{C}$, $0 < d < 20$

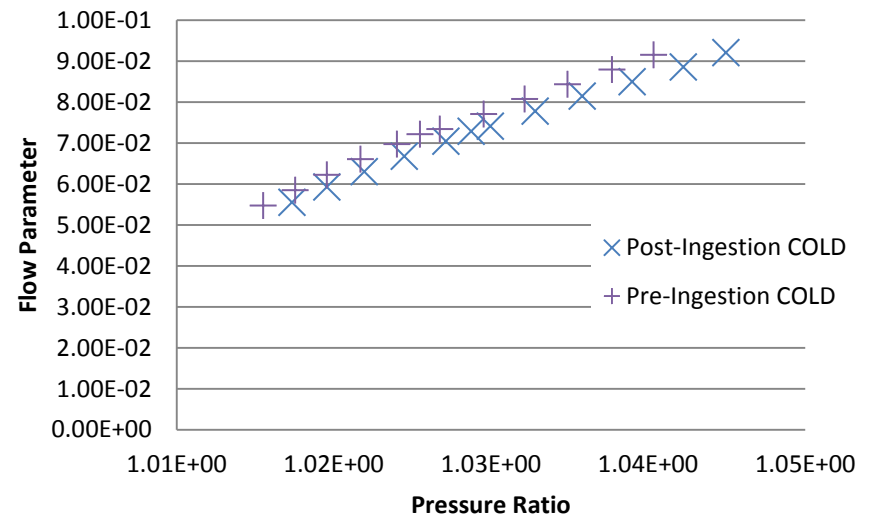


Above ATT

Volcanic Ash Ingestion:

$T_m = 1000^{\circ}\text{C}$, $0 < d < 20$

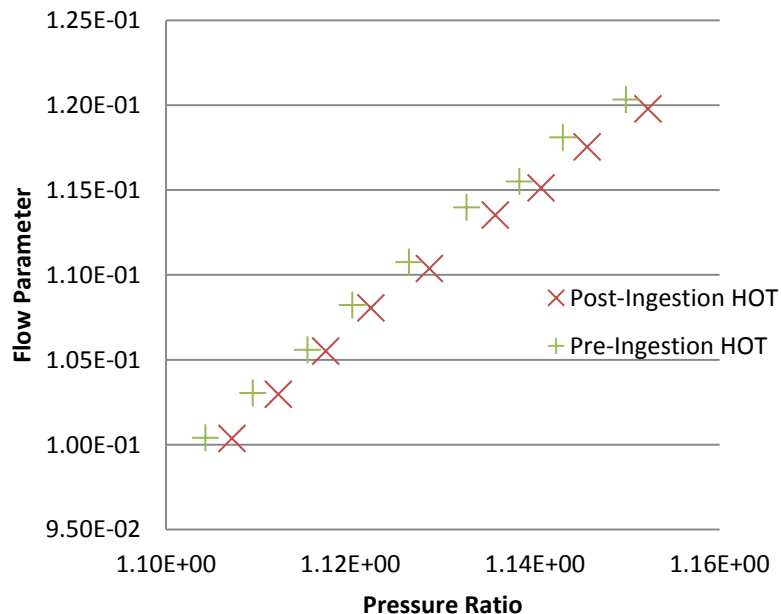
Flow Parameter Cold



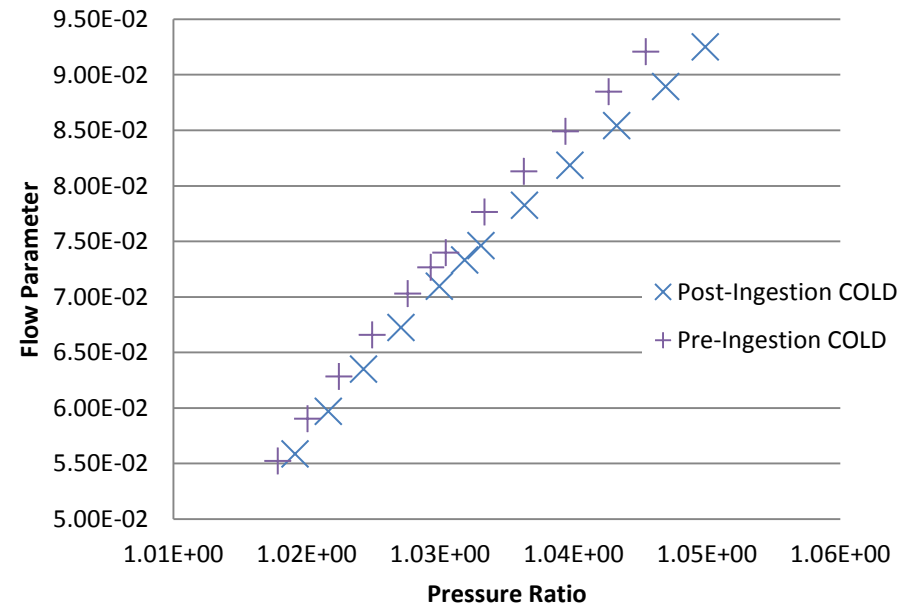
Variation in Metal Temperature

Approx ATT: $T_m=980^\circ\text{C}$

Volcanic Ash Ingestion:
 $T_m=980^\circ\text{C}$, $0 < d < 20$
Flow Parameter Hot

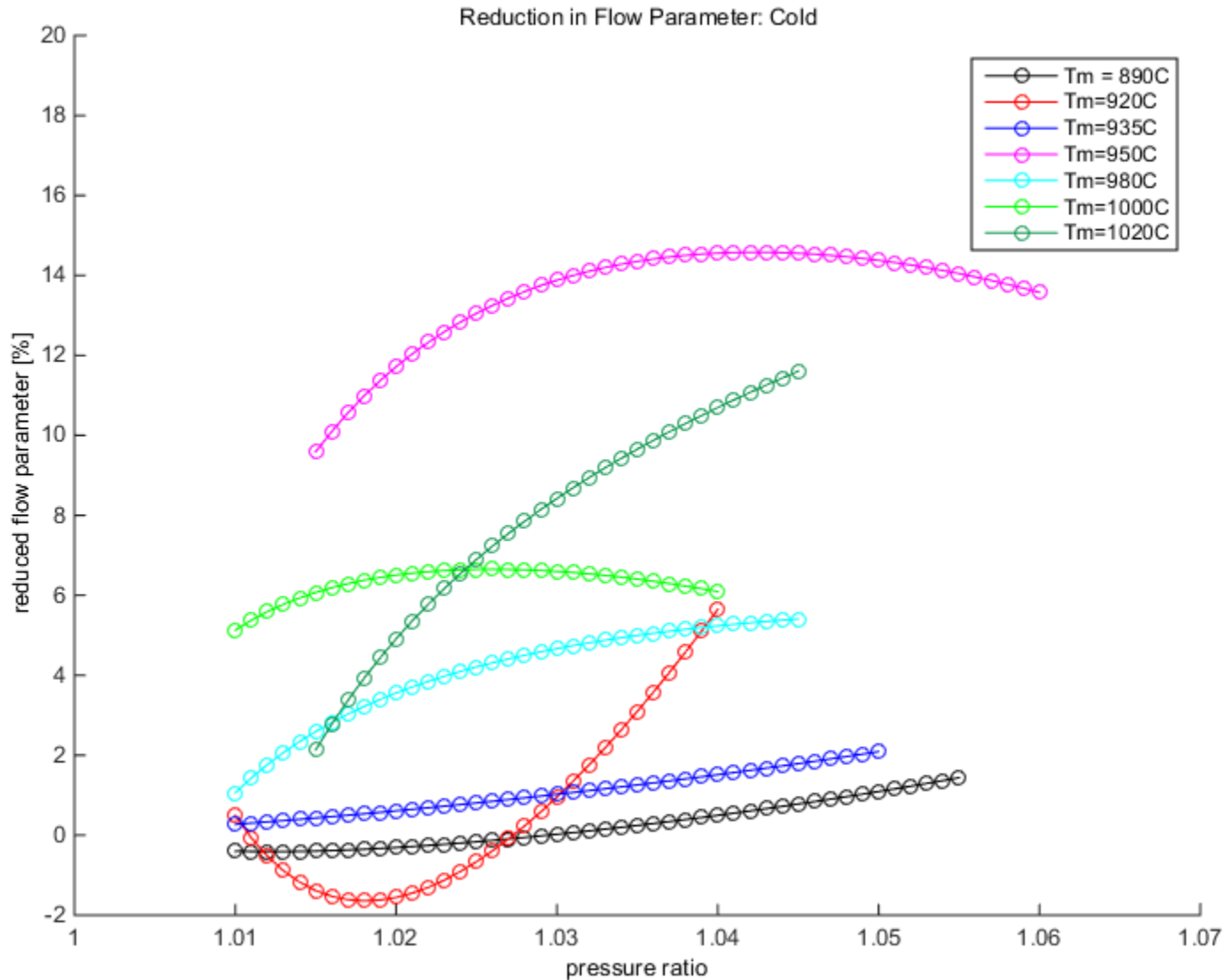


Volcanic Ash Ingestion: $T_m=980^\circ\text{C}$,
 $0 < d < 20$
Flow Parameter Cold



Metal Temperature EJYA2010 Ash

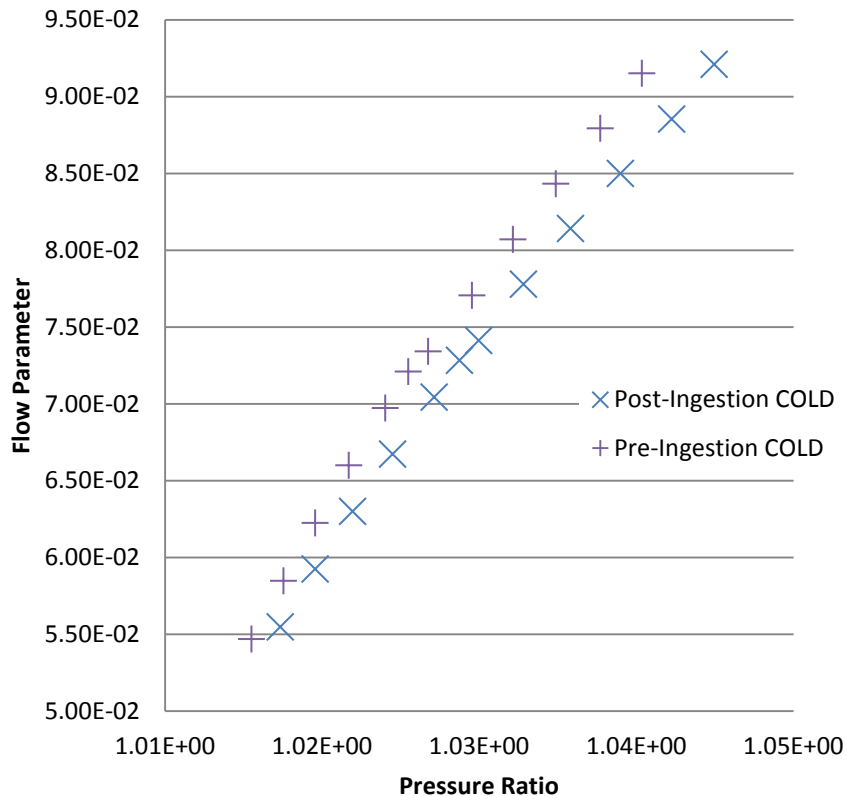
$0 < d < 20$ micron



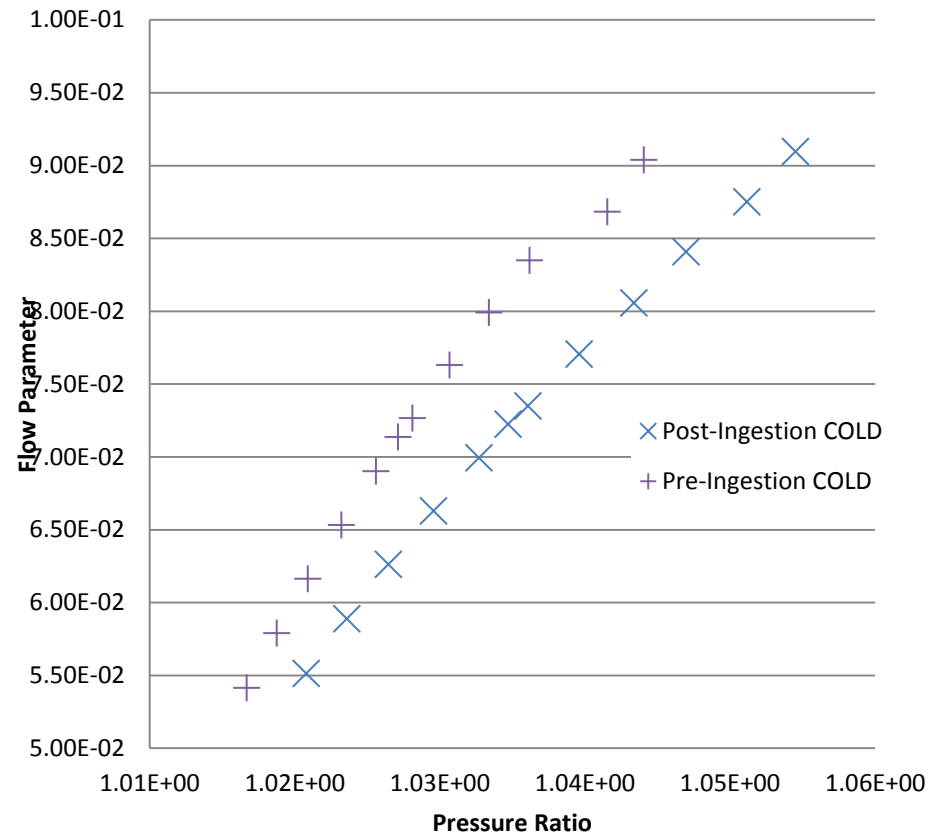
Variation in Ash Diameter

EJYA2010

$T_m=1000^{\circ}\text{C}$, $0 < d < 20$
Flow Parameter Cold

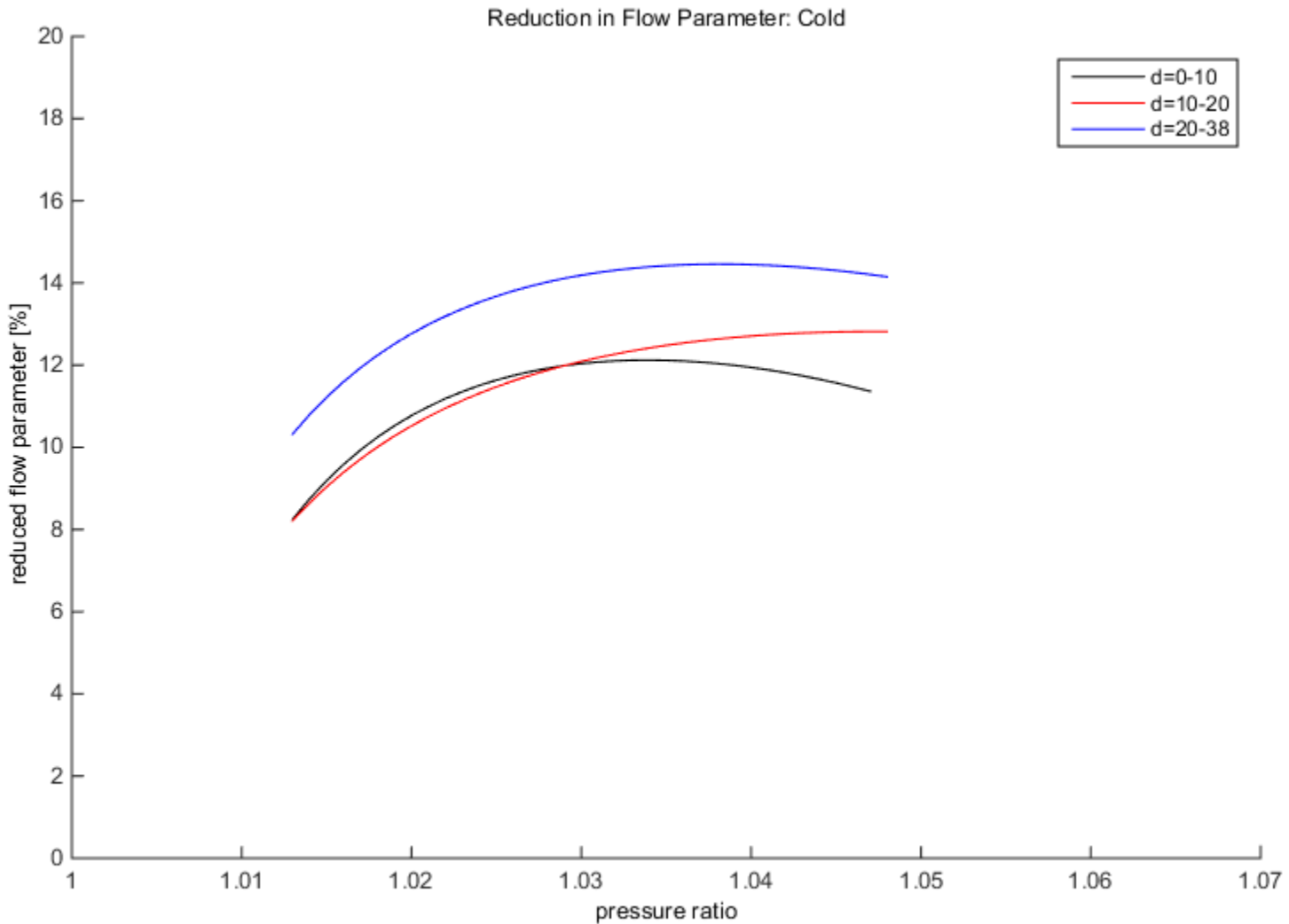


$T_m=1020^{\circ}\text{C}$, $0 < d < 10$
Flow Parameter Cold



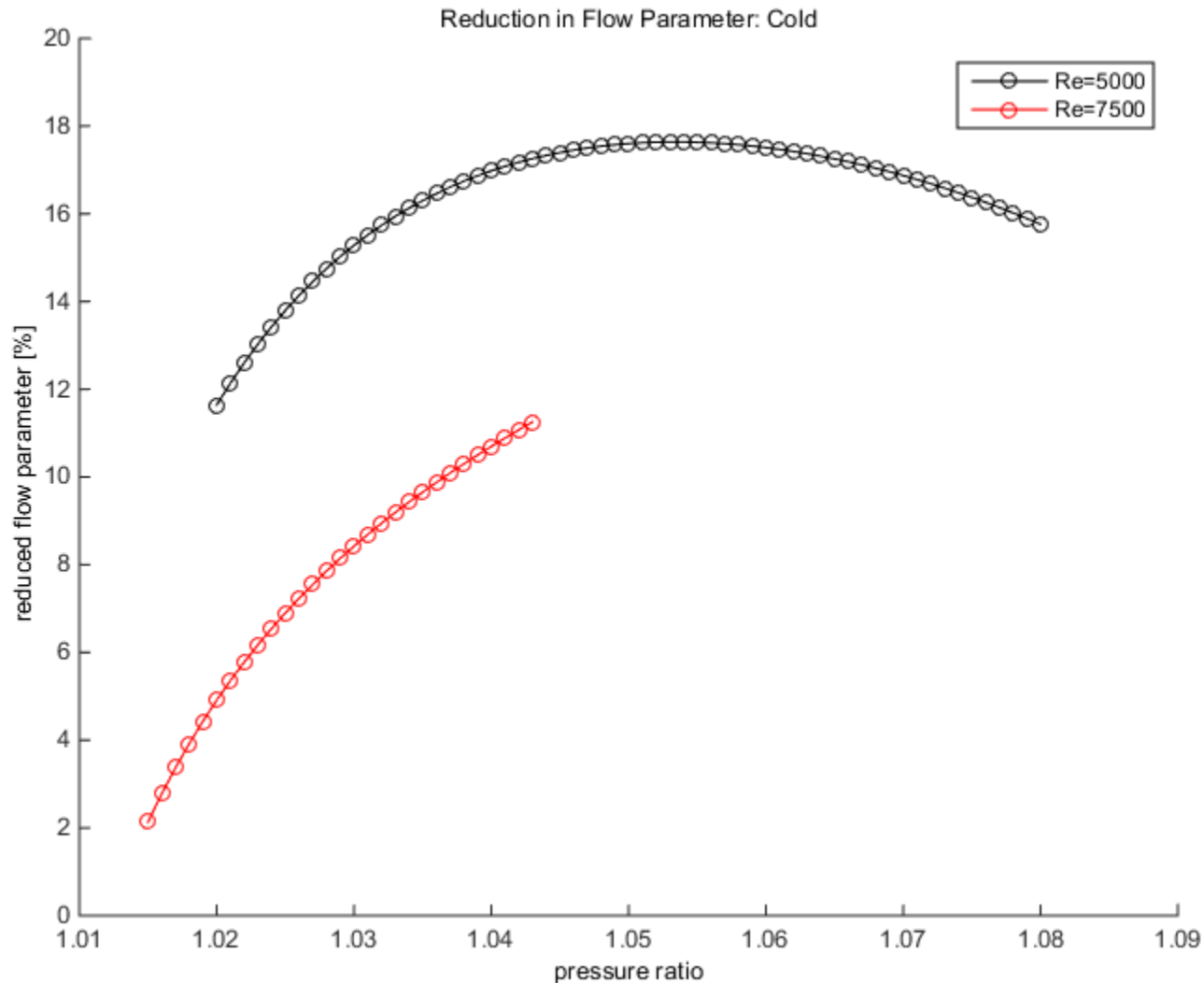
Particle diameter variation EJYA2010 Ash

$T_m = 1020^{\circ}\text{C}$, $T_c = 627^{\circ}\text{C}$



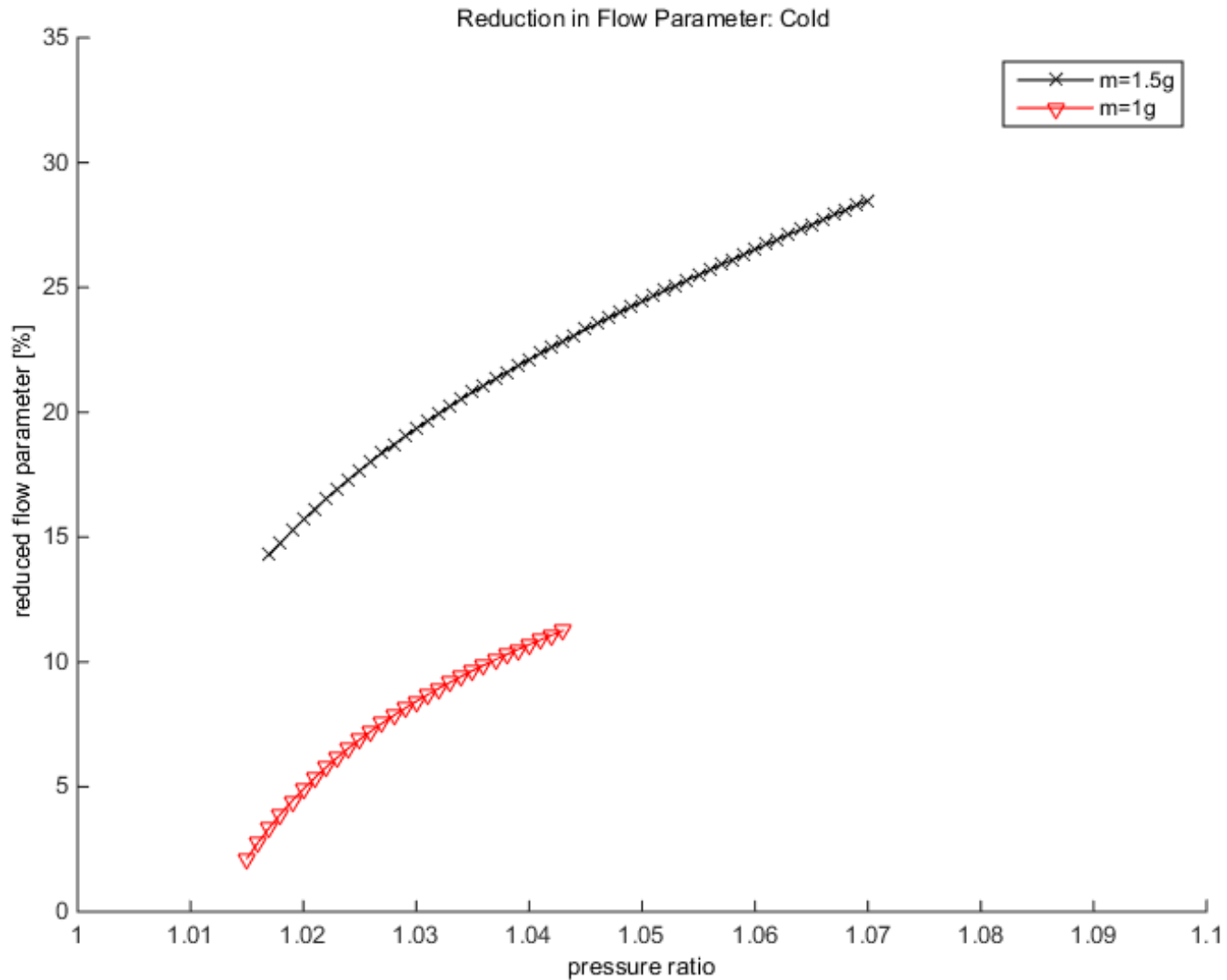
Effect of internal Reynolds number

$T_m = 1020^\circ\text{C}$, $T_c = 627^\circ\text{C}$ EJYA2010 Ash
 $0 < d < 20$ micron,



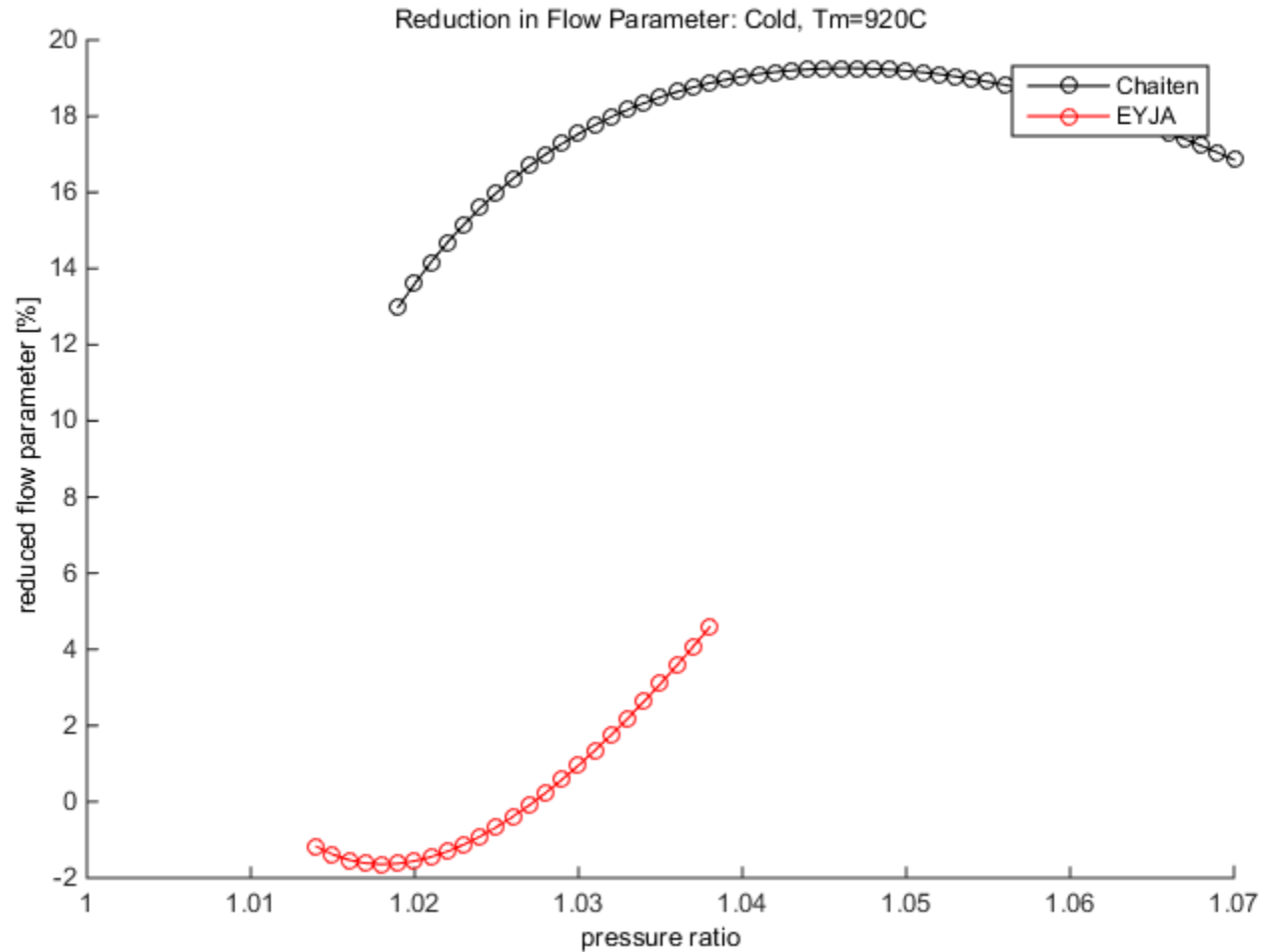
Effect of Dosing Density, EJYA2010 Ash

$T_m = 1020^{\circ}\text{C}$, $T_c = 627^{\circ}\text{C}$, $Re = 5000$



Effect of Ash Type

$T_m = 920^{\circ}\text{C}$, $T_c = 627^{\circ}\text{C}$



Effect of Ash Type

$T_m = 1020^{\circ}\text{C}$, $T_c = 627^{\circ}\text{C}$

