

Zentrum für Konstruktionswerkstoffe

Staatliche Materialprüfungsanstalt Darmstadt (MPA)

Fachgebiet und Institut für Werkstoffkunde (IfW)



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HELSMAC Symposium on Materials and Coatings for High Temperatures

Evolution of the crack driving force and fracture resistance during thermal cycling

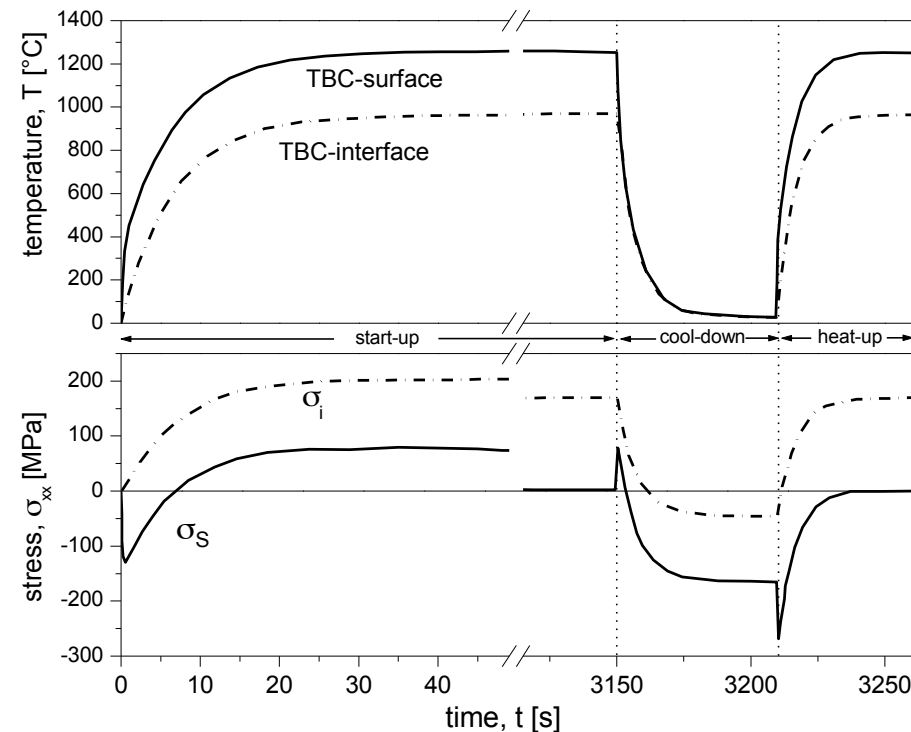
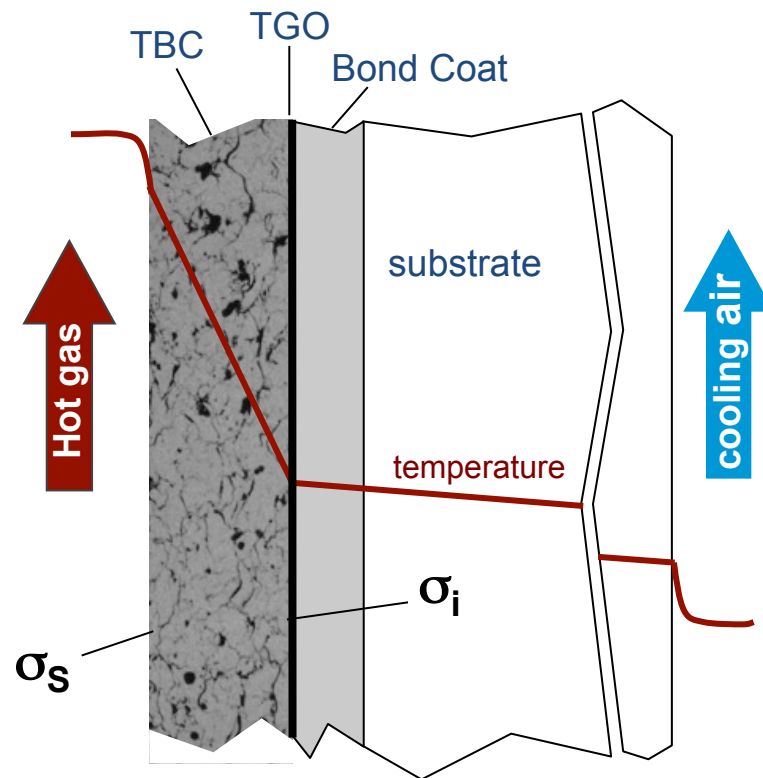
Cambridge, April 7, 2016

Matthias Oechsner, Alfred Scholz, Peter Wittig, Martin Frommherz

Outline

- Impact of thermal cycling on coating stresses and damage progression
- Coating life: crack driving force vs. fracture resistance
- Crack driving force
 - Constrained vs. free standing sintering
 - In-plane vs. out-of-plane stiffness
- Fracture resistance
 - Cohesive vs. adhesive fracture toughness
 - Vertical crack resistance
- Summary & Conclusions

Load situation during operation

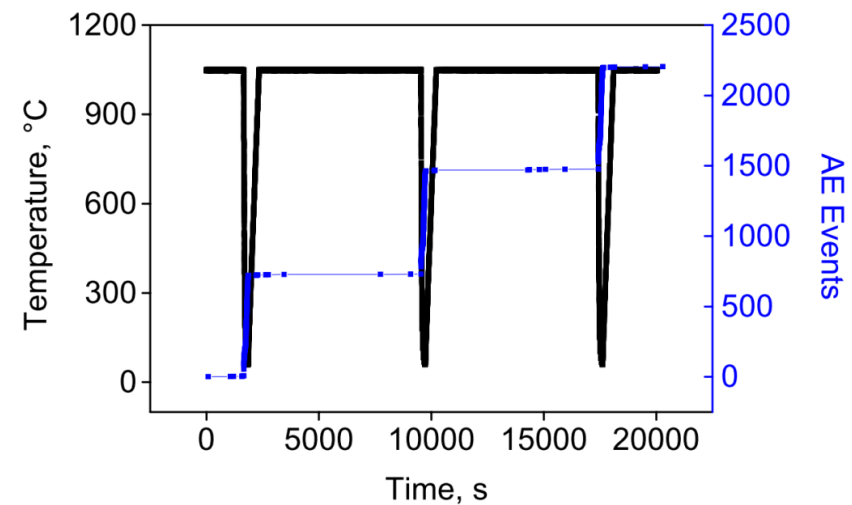
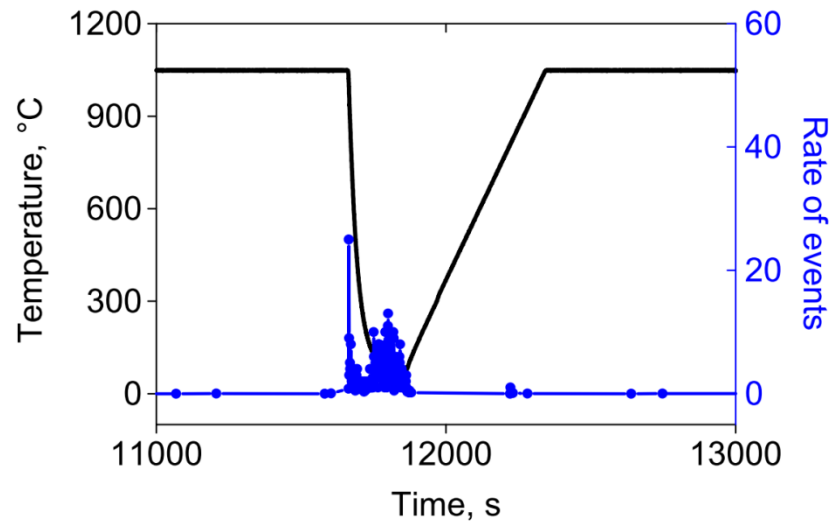


[M. Oechsner, Bd. 18, VDI Fortschrittsberichte Nr. 263. Düsseldorf: 2001]

- Layer stresses due to thermal misfit & thermal gradient
- Stress relaxation during stationary dwell time
- Thermal shock of ceramic surface during heat-up and cool down

Coating Damage progression during cyclic loading

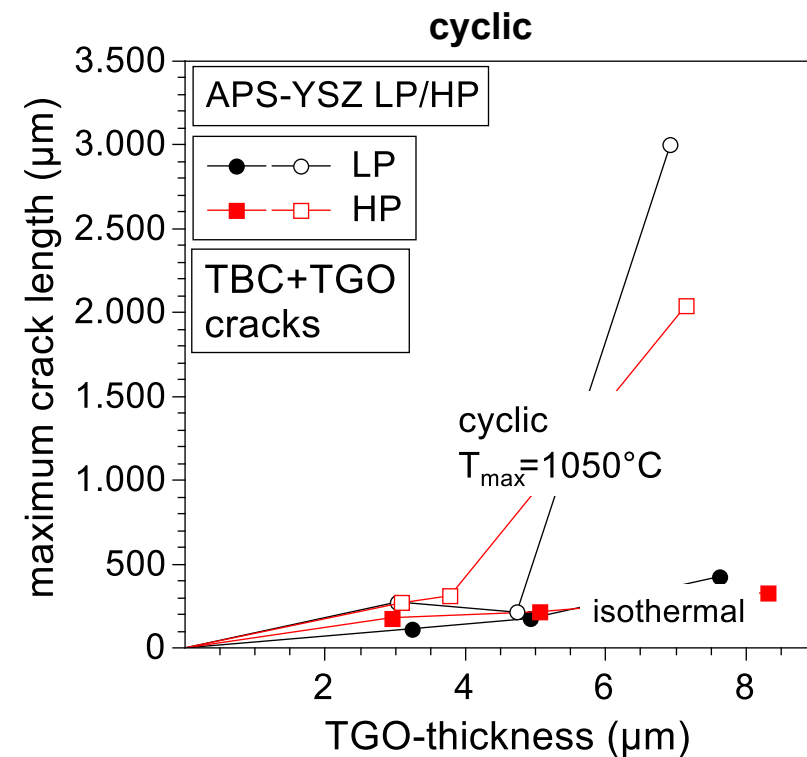
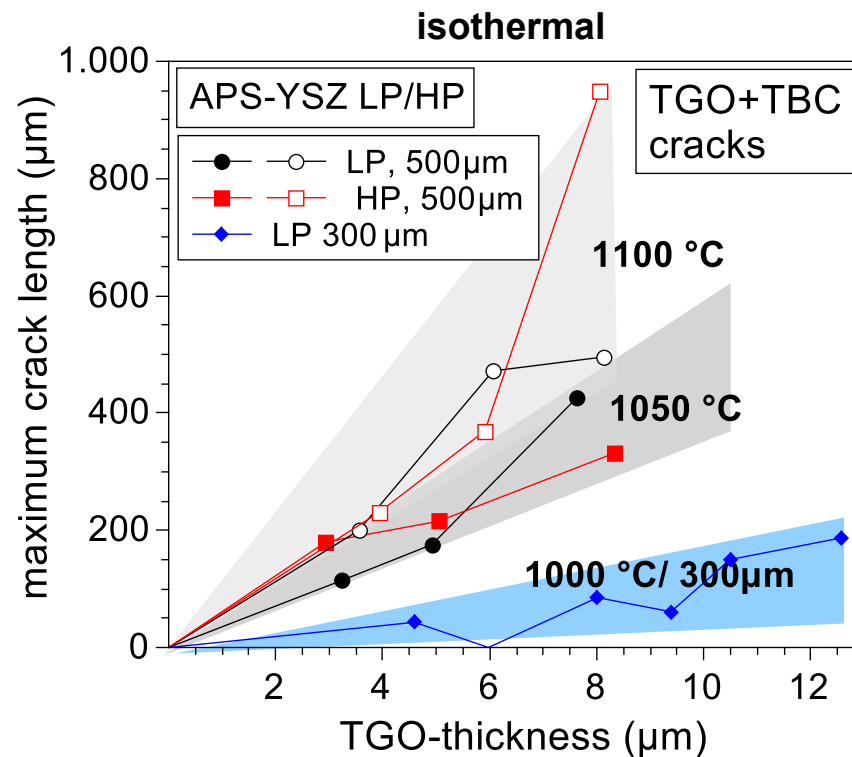
Damage detection using acoustic emission



[O. Trunova, RWTH Aachen, 2006]

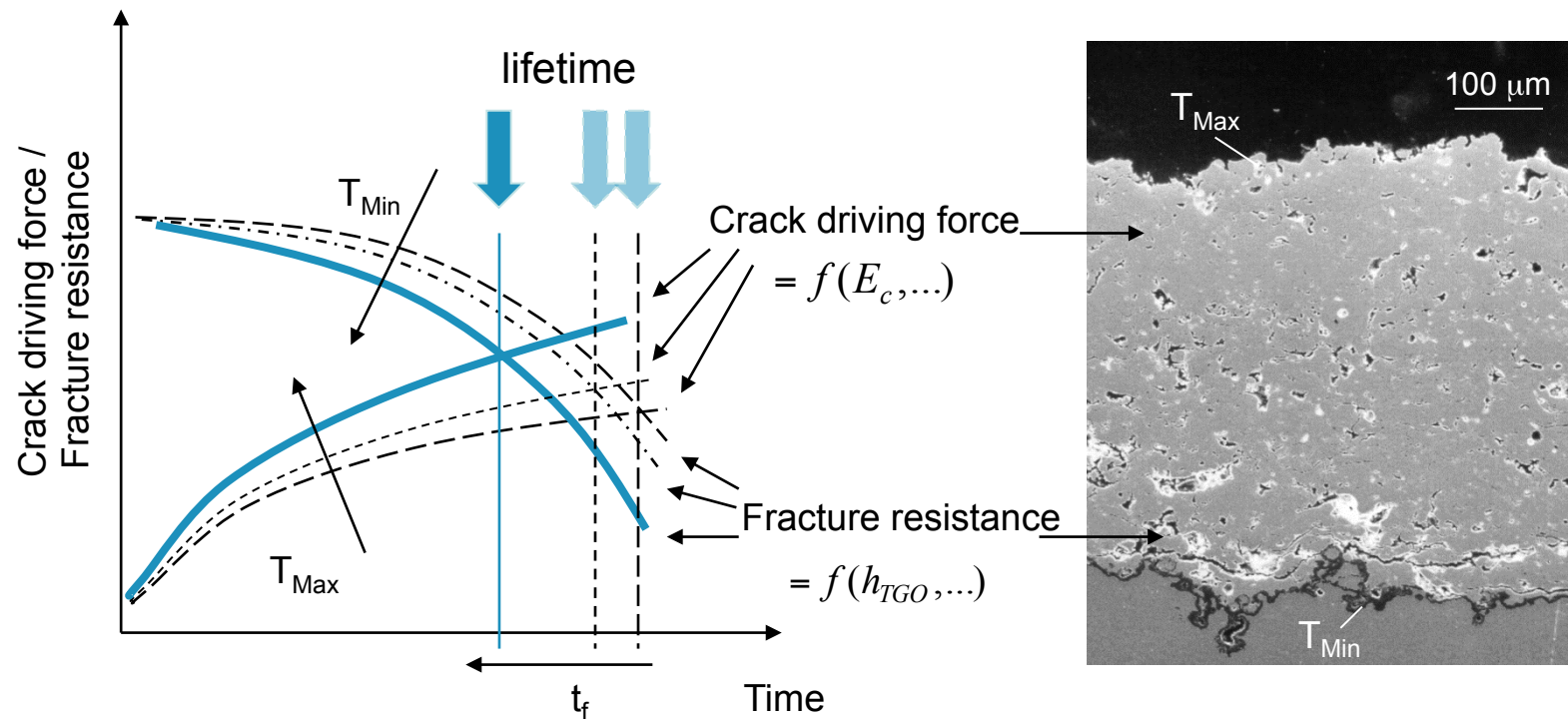
Acoustic emission signals are detected during cool down phase

Accumulated damage during cyclic oxidation



- Macroscopic crack growth after „incubation time“ ($t@T$)
- Cyclic loading results in faster crack growth kinetics

Approach to assess TBC life time



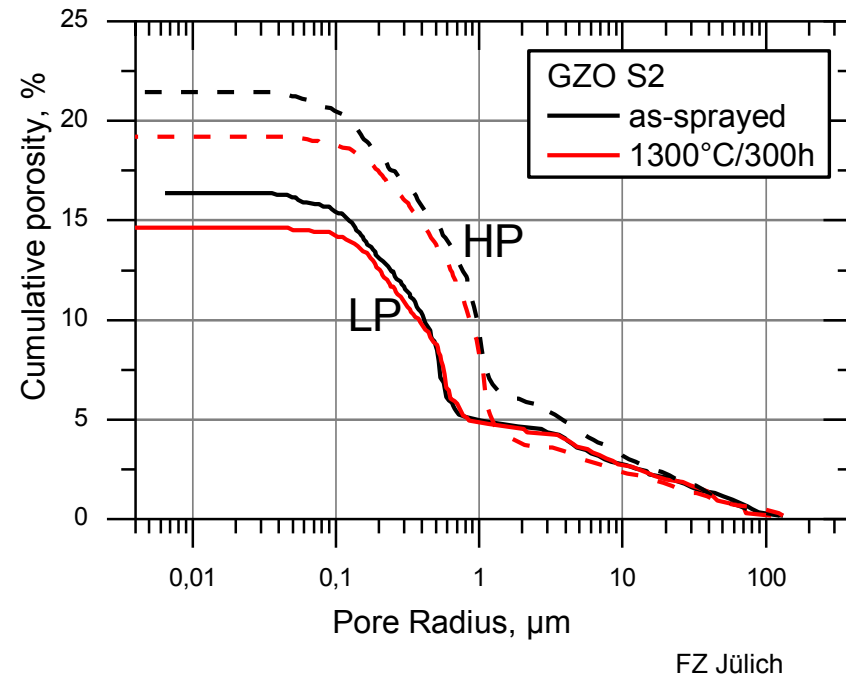
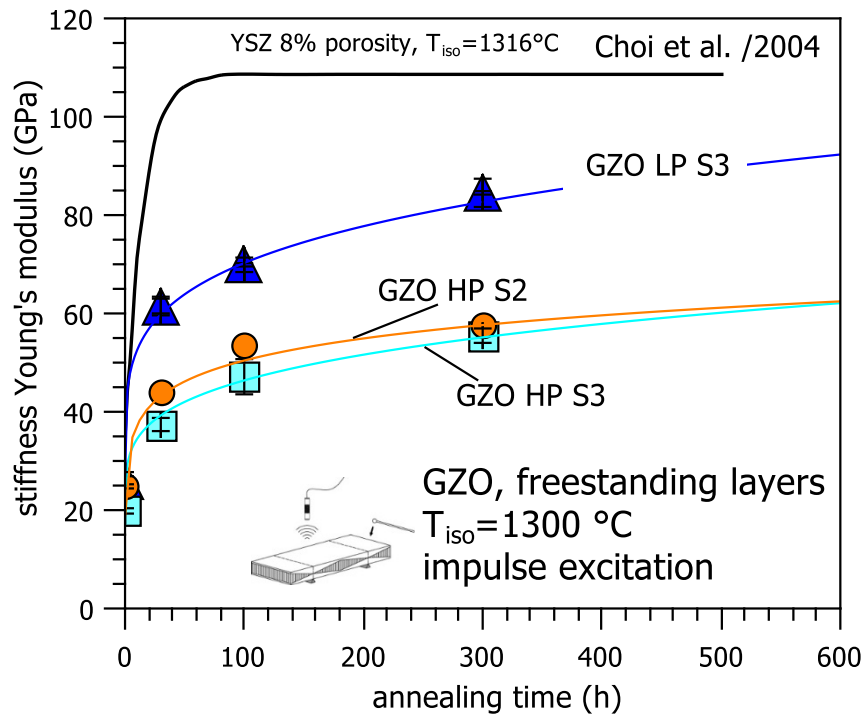
[M. Oechsner, Bd. 18, VDI Fortschrittsberichte Nr. 263. Düsseldorf: 2001]

- Crack driving force and toughness against crack propagation are time dependent
- Kinetics are determined by the surface and interface temperature

Crack Driving Force

Crack Driving Force

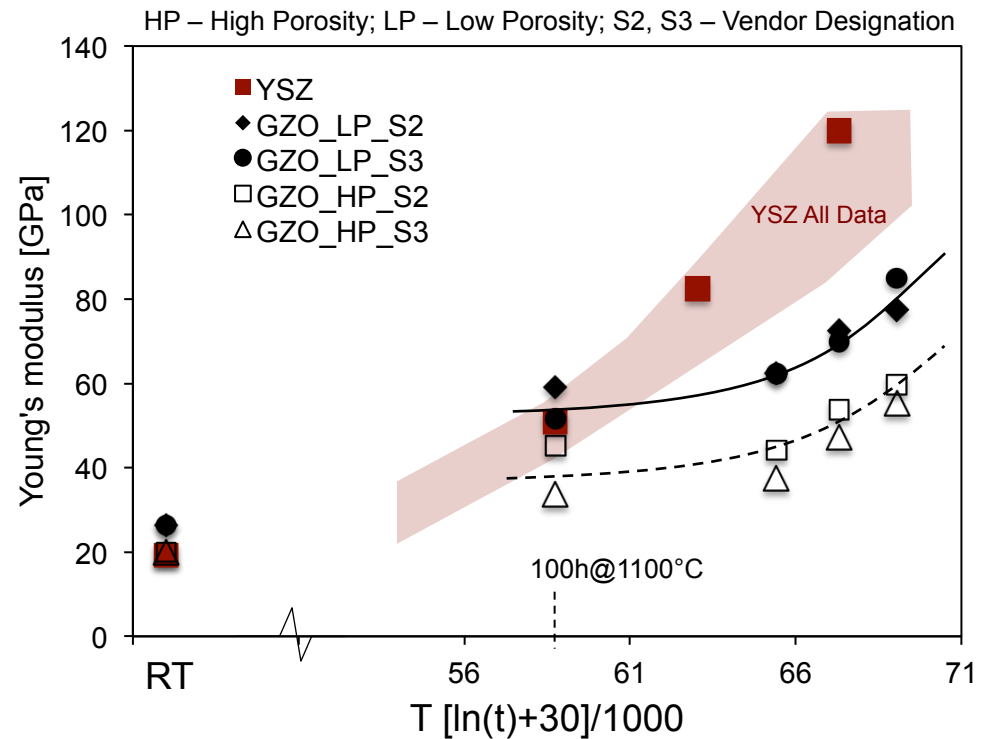
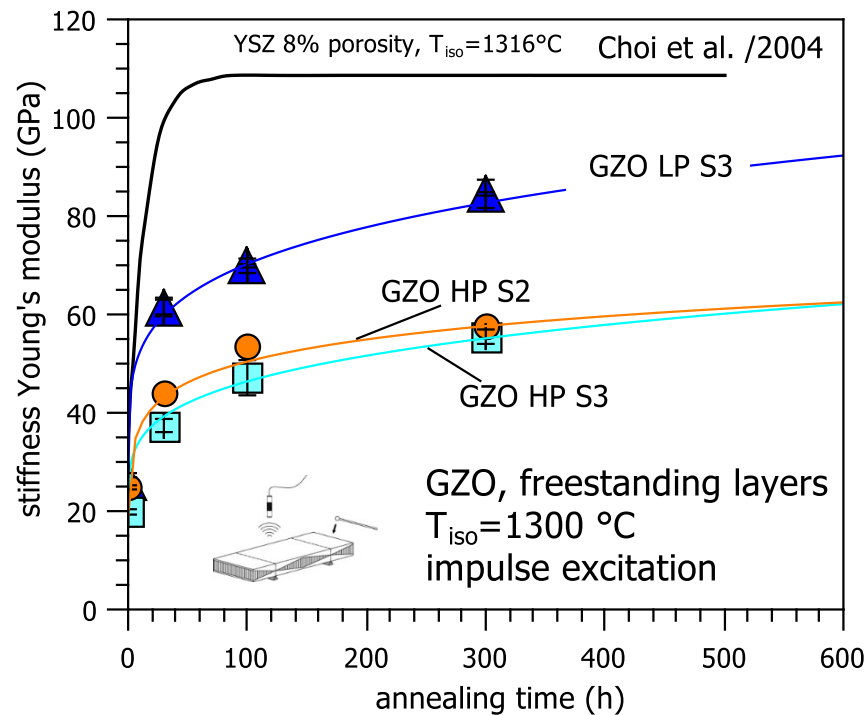
Increase in Coating Stiffness



- Stiffness und thus the Crack Driving Force increase due to sintering
- Increase in stiffness is mainly correlated to healing and sintering of “submicron” defects

Crack Driving Force

Time-Temperature-Parameter

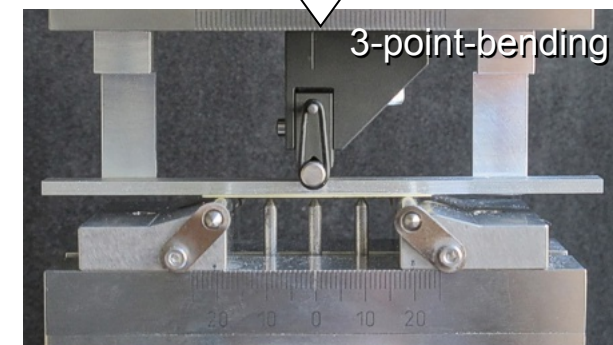
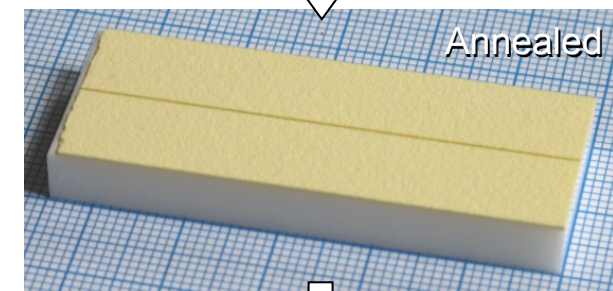
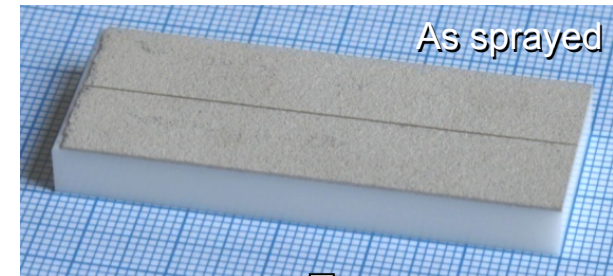
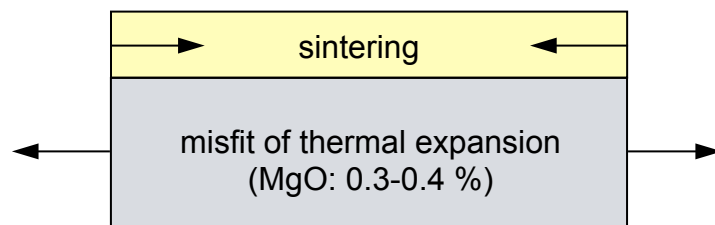


Change in Young's modulus can be described by a time-temperature relation

Crack Driving Force

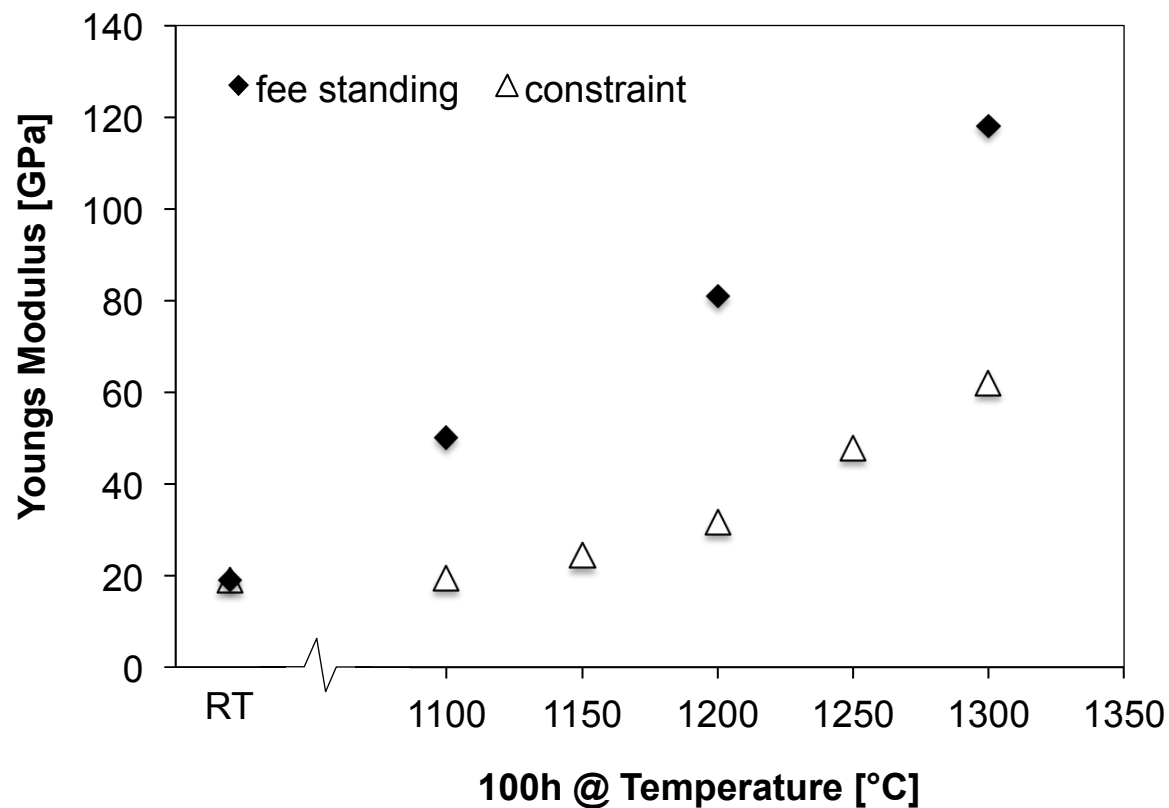
What impact has constraint on sintering?

- YSZ has been sprayed on Magnesia (MgO) specimens in order to allow high temperature exposure while being constraint by a substrate
- Note that the CTE of Magnesia is larger than the CTE of YSZ, mimicking the constraint conditions present at nickel-based superalloys

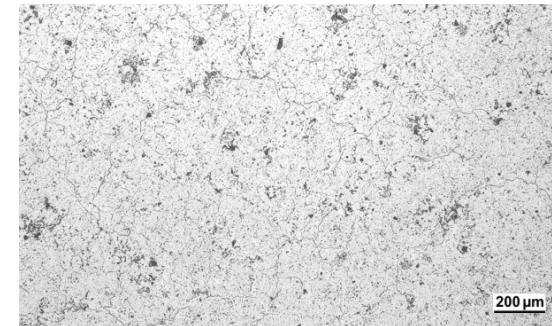


Crack Driving Force

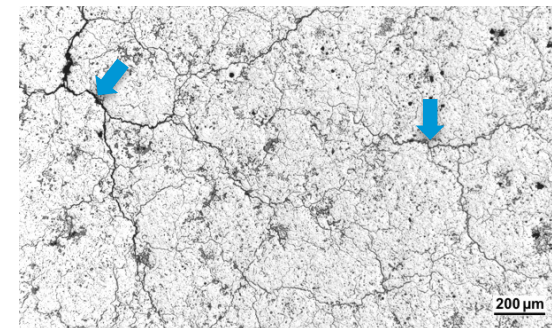
Approximation of local stiffness properties



Free standing



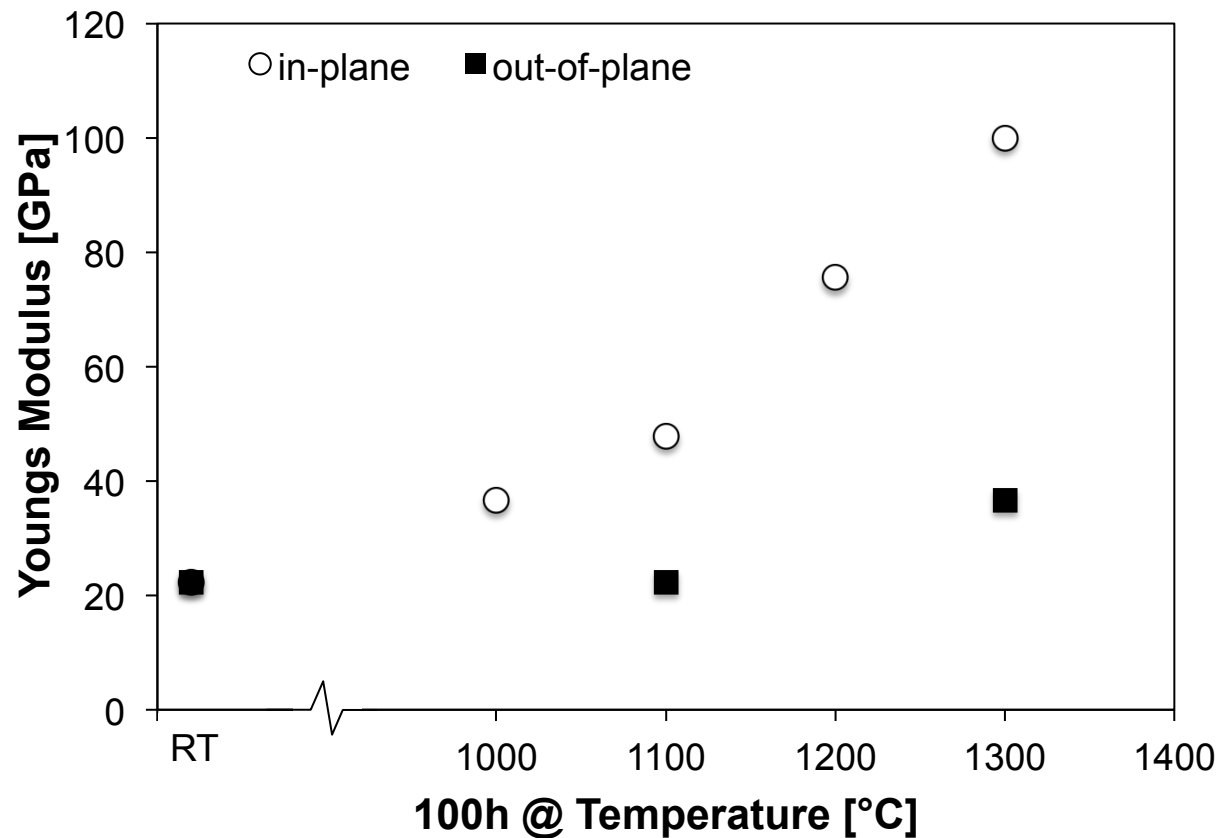
Constraint ($\epsilon \approx 0.4\%$)



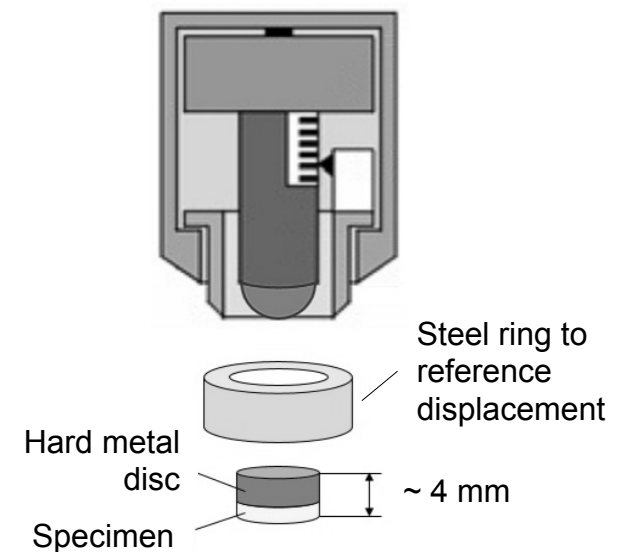
[P. Wittig, unpublished]

- Constraint during sintering reduces increase in stiffness
- Segmentation cracks in coating after constraint sintering visible

Anisotropy of elastic properties



Miniature Compression Test



Significant stiffness difference of free standing sintered samples ($E^{\perp} < 0,6 \cdot E^{\parallel}$)

Validation

Young's Modulus on Combustor Component

removed for copy right reasons

Heat Shield

Siemens SGT-4000F

$T_{\text{Surface}} \approx 1250^{\circ}\text{C}$

$T_{\text{BondCoat}} \approx 870^{\circ}\text{C}$

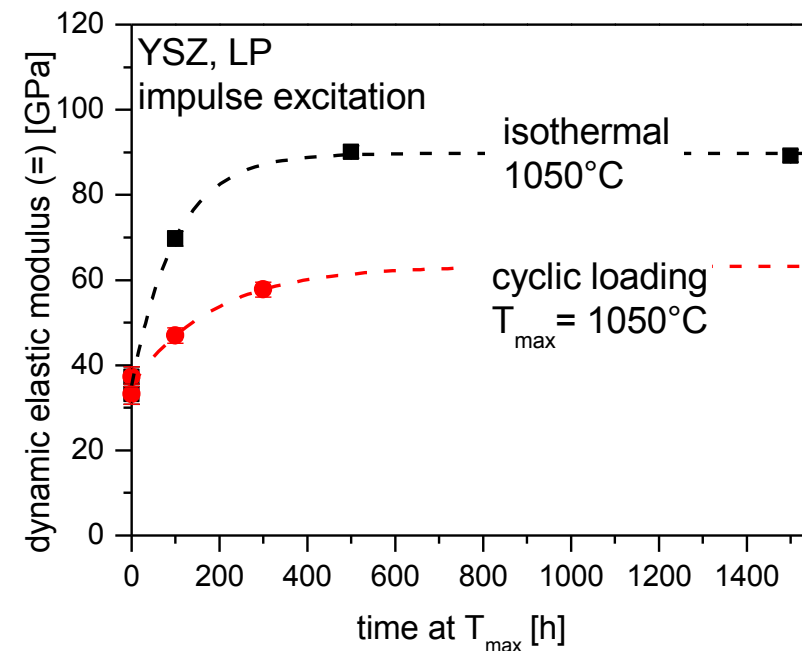
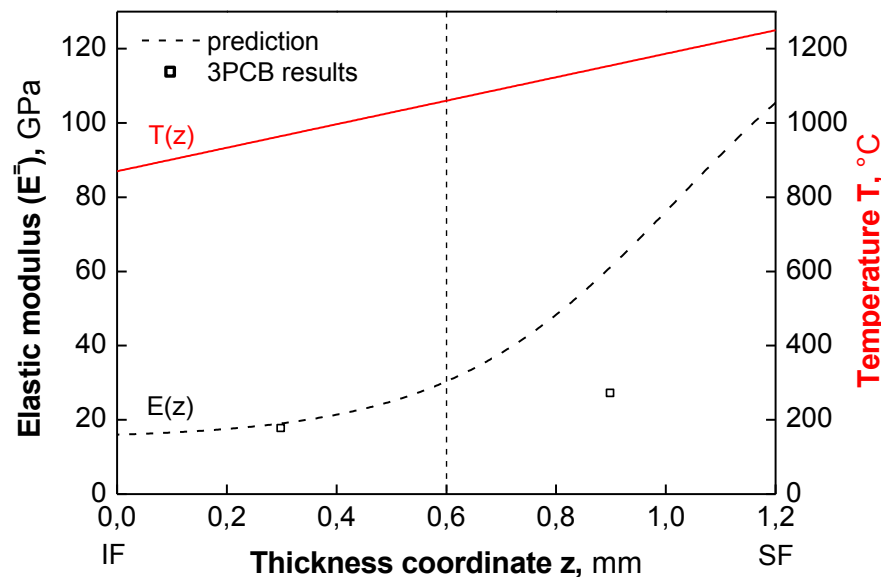
$t_{\text{Operation}} \approx 6.600 \text{ hrs.}$



Validation

High temperature modulus over-estimated by prediction

Effective planar elastic modulus, $E^=$



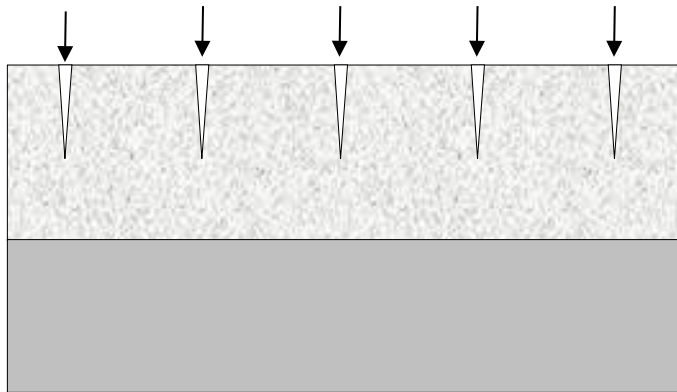
Low temperature modulus is captured well by prediction, however high temperature modulus is predicted too low

→ Potential impact of segmented TBC from cyclic loading?

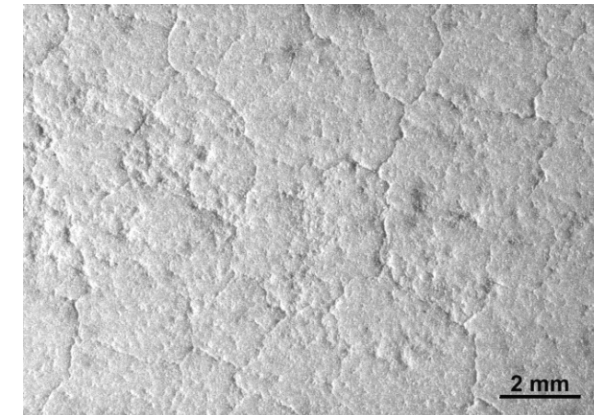
Combustor tiles show segmentation cracks

Explanation for reduced stiffness?

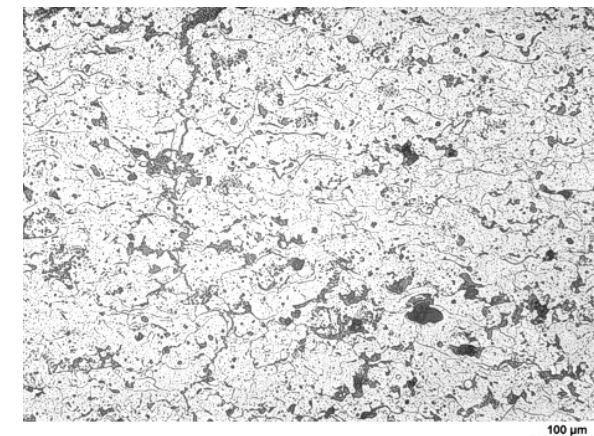
Sintering under constraint + cyclic loading
introduce segmentation cracks, lowering the
in-plane stiffness



Top view



Cross section



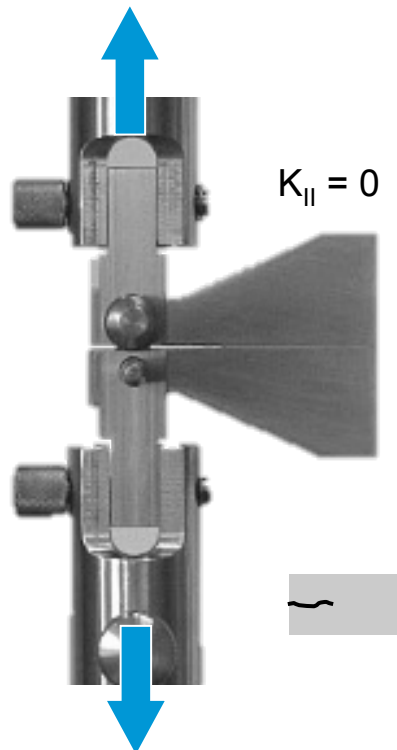
Fracture Resistance

Fracture Resistance

In-plane Fracture Toughness

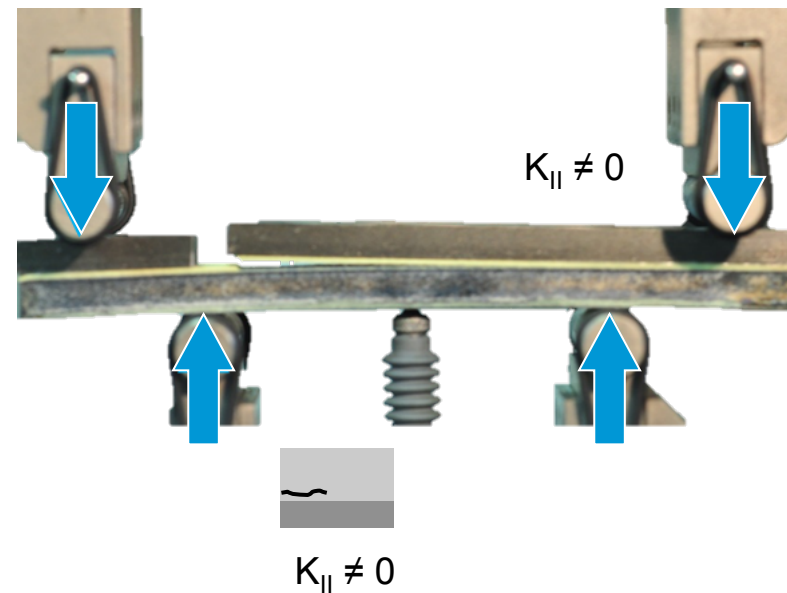
TDCB

Tapered Double Cantilever Beam



→ Cohesive Fracture Resistance

Modified 4-Point Bending Test

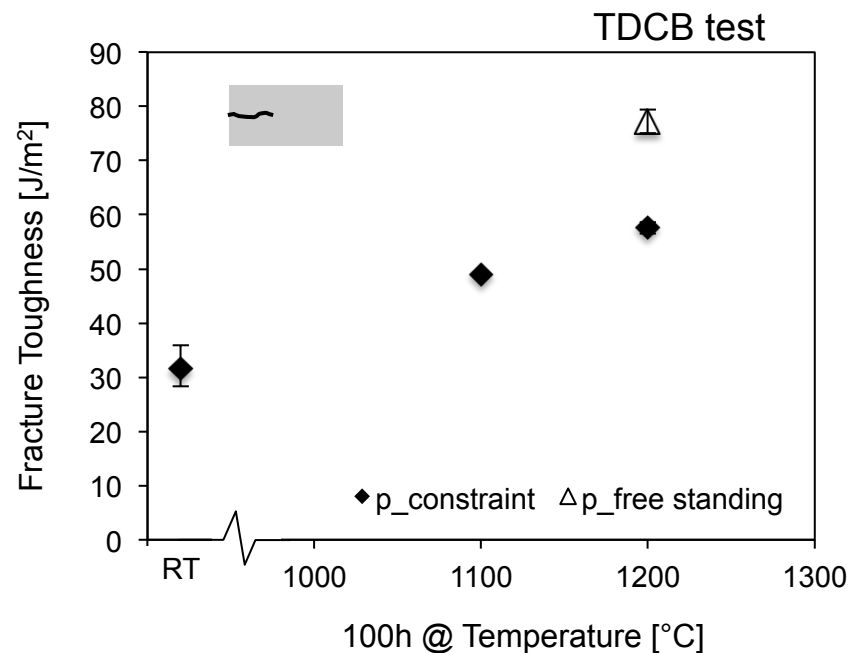


→ Interfacial Fracture Resistance

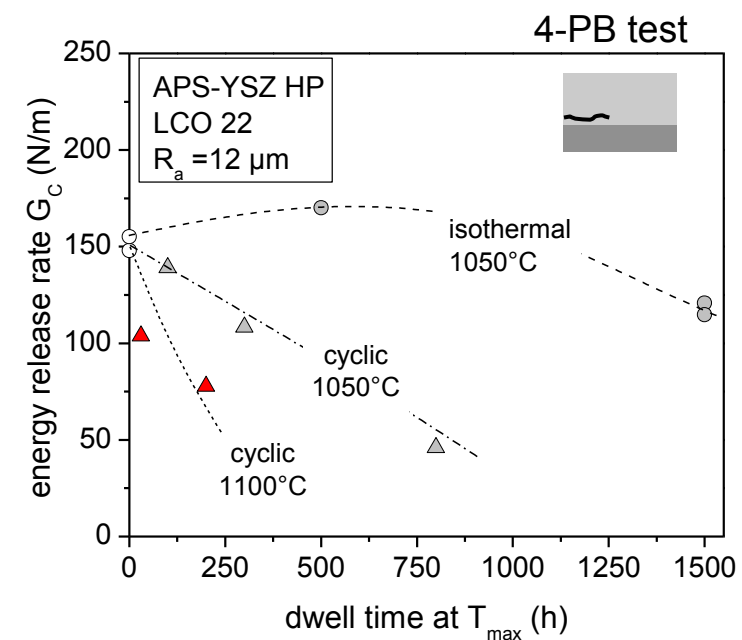
Fracture Resistance

Local Evolution

Cohesive fracture toughness



Interface fracture toughness

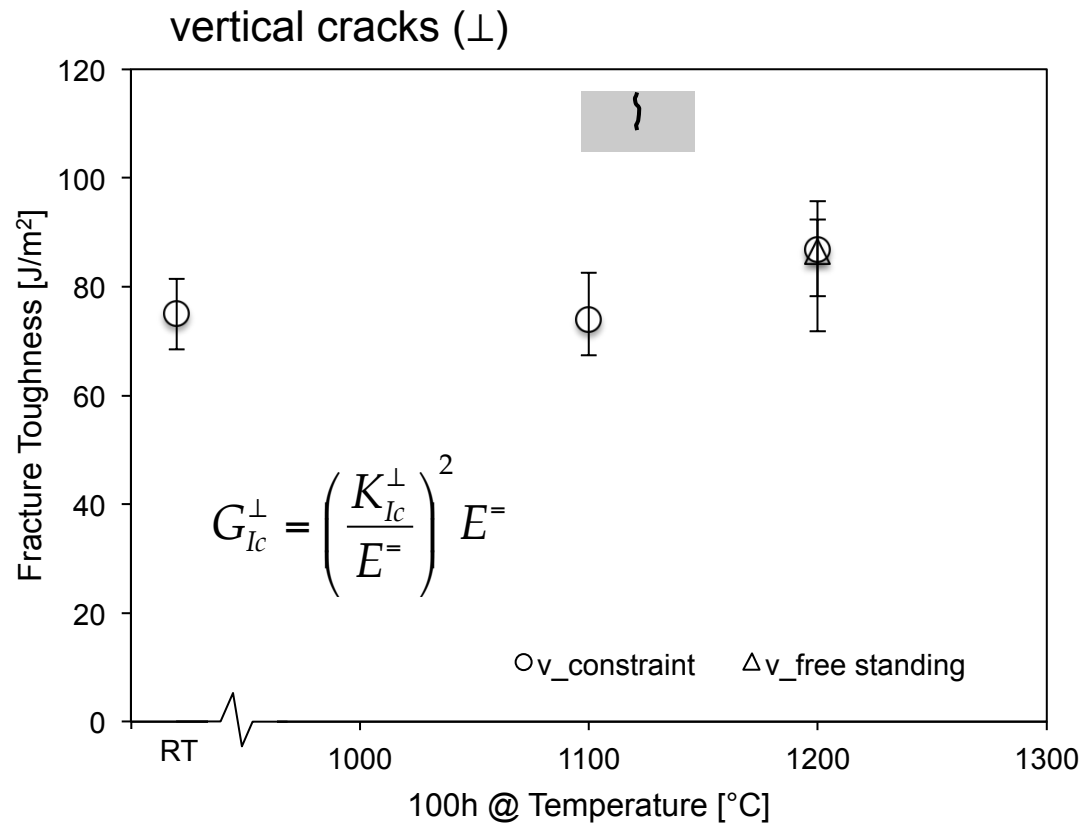


- Sintering results in an increase in toughness
- Influence of segmentation is limited

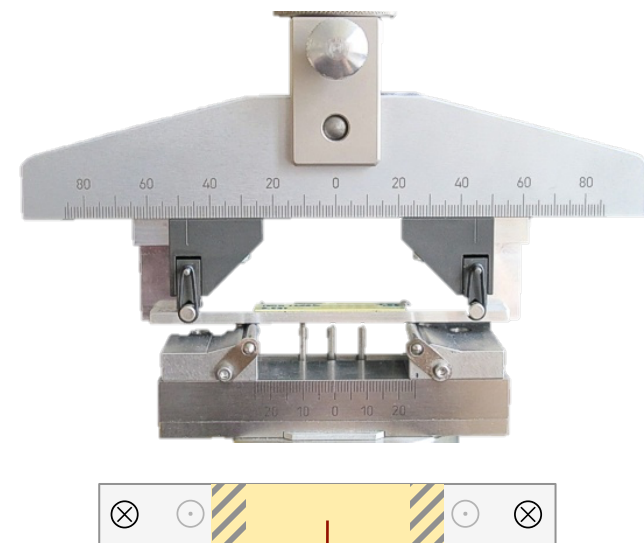
- Damage accumulation due to subcritical crack growth
- TGO growth induces damage

Fracture Resistance

Anisotropy



SENUD
 Single Edge Notched Uniform Displacement

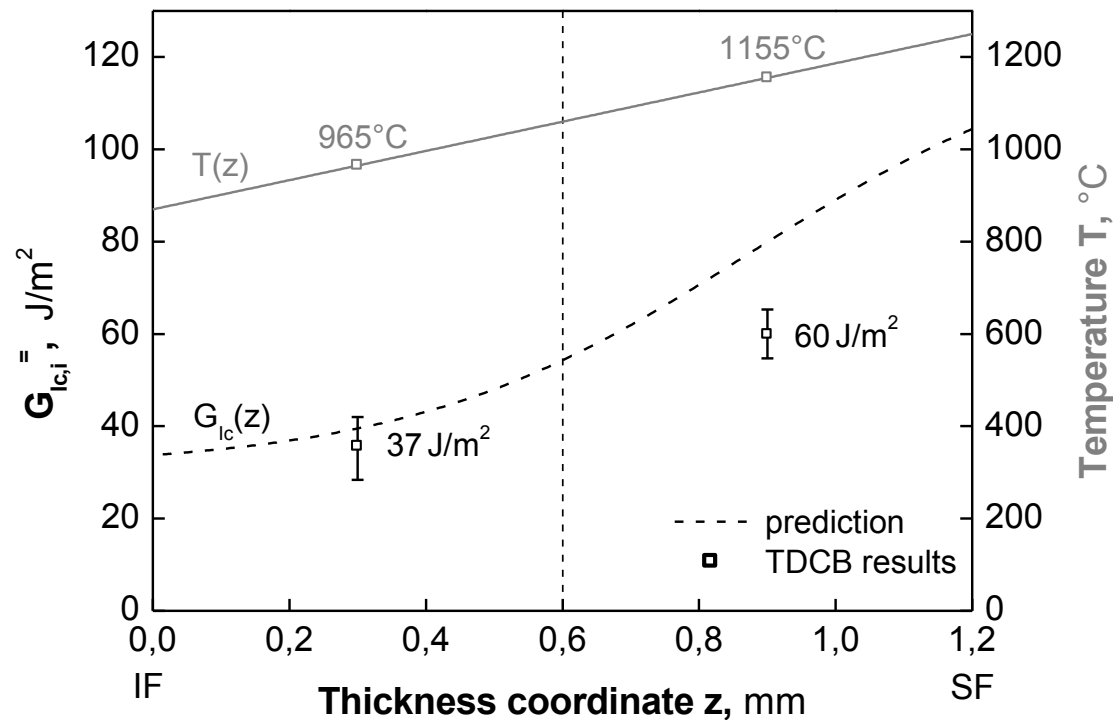


Slight increase in fracture toughness due to sintering

Validation

Prediction vs. Experiment

Critical energy release rate $G_{Ic}^=$ (small cracks)



[data: P. Wittig]

Model prediction over-estimates the observed fracture toughness

Summary & Conclusions

- Thermal cycling accelerates coating degradation
- Crack driving force & fracture resistance change with time, temperature and cyclic loading conditions
- Crack driving force
 - Sintering under constraint conditions reduces increase in coating stiffness
 - Sintering under constraint conditions introduces vertical cracking
 - Cyclic loading introduces coating segmentation
 - Out-of-plane stiffness changes at a slower rate compared to in-plane stiffness
- Fracture resistance
 - Cohesive fracture toughness increases with time@temperature
 - Adhesive fracture toughness decreases with growth of TGO
 - Only slight increase in resistance against vertical cracking due to sintering
- Comparison with service experienced components confirms general trend



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Questions ?

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